MRS/IS Facility Co-Located with a Repository: Preconceptual Design and Life Cycle Cost Estimates

R. I. Smith J. F. Nesbitt

November 1982

Prepared for the U.S. Department of Energy under Contract DE-AC06-76RLO 1830

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Pacific Northwest Laboratory Richland, Washington 99352 • **،** " ₽. -.

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Appendix A was developed by E. T. Merrill of PNL. Appendix B was developed by PNL staff members E. T. Merrill and B. M. Cole, led by J. F. Fletcher. Appendix C was developed by P. M. Daling of PNL. Appendix D is based on material developed by K. D. Hayden of Westinghouse-Hanford Co.

Responsibility for assembling and integrating the information, performing the necessary analyses, and drafting the rest of the report rests with the Project Manager, R. I. Smith of PNL, with the very considerable assistance of J. F. Nesbitt of PNL.

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EXECUTIVE SUMMARY

Changes in recent years in federal policies regarding reprocessing and/or disposal of spent nuclear reactor fuel have produced delays in the development of fuel reprocessing plants and deep geologic disposal facilities. As a result, many nuclear power plants are faced with the possibility of shutdown due to lack of spent fuel storage capacity. In recognition of this problem, legislative initiatives are underway in Congress to provide appropriate storage and disposal facilities.

The Department of Energy (DOE), through its Office of Nuclear Fuel Cycle, has established a program to examine the various alternatives for storage of spent nuclear fuel, solidified high-level wastes (HLW), and transuranic (TRU) wastes until an appropriate deep geologic repository is available for disposal of these wastes. One of these alternatives, a monitored retrievable storage/interim storage (MRS/IS) facility built on the site of a future repository, is the subject of this stugy.

The MRS/IS facility evaluated in this study is composed of a Waste Handling Facility where the incoming waste shipments are received and the individual fuel assemblies/HLW canisters/TRU containers are examined and decontaminated and/or repackaged as appropriate before transfer to the storage areas. The facility is also composed of storage areas where the spent fuel assemblies and HLW canisters are stored in either large metal storage casks standing on support pads or in subsurface drywells with the surrounding soil providing shielding. In the storage areas, remote-handled TRU wastes (RHTRU) are stored in concrete casks standing on support pads, and contact-handled TRU wastes (CHTRU) are stored in a surface warehouse. Transfer of the stored wastes from the storage areas to the repository is accomplished after the repository is opened.

The objectives of this study are: 1) to develop a preconceptual design for an MRS/IS facility that would become the principal surface facility for a deep geologic repository when the repository is opened, 2) to examine various issues such as transportation of wastes, licensing of the facility, and environmental concerns associated with operation of such a facility, and

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3) to estimate the life cycle costs of the facility when operated in response to a set of scenarios which define the quantities and types of waste requiring storage in specific time periods, which generally span the years from 1990 until 2016.

The life cycle costs estimated in this study include: the capital expenditures for structures, casks and/or drywells, storage areas and pads, and transfer equipment; the cost of staff labor, supplies, and services; and the incremental cost of transporting the waste materials from the site of origin to the MRS/IS facility (and in the case of spent fuel, returning the spent fuel to the reprocessing plant).

Three scenarios are examined to develop estimates of life cycle costs of the MRS/IS facility. In the first scenario, HLW canisters are stored, starting in 1990, until the co-located repository is opened in the year 1998. Additional reprocessing plants and repositories are placed in service at various intervals. In the second scenario, spent fuel is stored, starting in 1990, because the reprocessing plants are delayed in starting operations by 10 years, but no HLW is stored because the repositories open on schedule. In the third scenario, HLW is stored, starting in 1990, because the repositories are delayed 10 years, but the reprocessing plants open on schedule.

The undiscounted life cycle costs for the MRS/IS facility estimated in this study range from \$0.5 to \$2.5 billion, depending upon the scenarios. Expenditures for metal storage casks are estimated to range from \$0.30 to \$1.77 billion. Cost reductions resulting from the use of drywells instead of metal casks could range from \$0.21 to \$1.25 billion. Other cost reductions resulting from consolidation of spent fuel assemblies into closely packed arrays and from the use of large storage casks for offsite shipment of spent fuel and HLW could be more than \$1.6 billion.

The principal conclusions derived from this study are the following:

 Co-locating the MRS/IS facility with a repository will reduce overall waste management system costs by eliminating the duplication of facilities that would occur if the storage and repository facilities

vi

were located separately. Since the MRS/IS facility becomes the surface facility for the repository, the useful life of the structure is extended significantly, thus allowing a longer amortization period and a smaller annual amortization charge.

- The stored waste materials would be transferred directly from storage to the repository without leaving the site, thereby minimizing the potential for transportation accidents and the possible exposure of the public resulting from such accidents.
- Because the life cycle cost of an MRS/IS facility is likely to be in the \$0.7 to \$2.5 billion range, all avenues available for reducing costs should be explored. The use of drywells instead of metal casks, consolidation of spent fuel assemblies, and the use of the large storage casks for shipment of wastes all show promise for cost reductions. Water pool storage, an alternative not examined in this study, should also be carefully evaluated for comparison with the dry storage alternatives, to select the most cost-effective approach.

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• •

6

•

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CONTENTS

•

2

ACKN	OWLED	GMENTS	•	•	•	•	•	•	•	•	•	•	•	iii
EXEC	UTIVE	SUMMARY	•	•	•	•	•	•	•	•	•	•	•	v
1.0	INTR	ODUCTION	•	•	•	•	•	•	•	•	•	•	•	1.1
2.0	SUMM	ARY .	•	•	•	•	•	•	•	•	•	•	•	2.1
	2.1	STUDY BA	SES	•	•	•	•	•	•	•	•	•	•	2.1
	2.2	CONCEPTU	JAL FAC	LITY	CHARA	CTER	ISTICS	5	•	•	•	•	•	2.3
	2.3	CONSTRUC	CTION SO	CHEDUL	E AND	cos	T ESTI	(MATE:	S	•	•	•	•	2.4
	2.4	SYSTEM L	IFE CYC	CLE CO	DST	•	•	•	•	•	•	•	•	2.4
	2.5	SENSITIV	ITY OF	COSTS	5 то с	CONCEI	PTS AN	ND AS	SUMPT	IONS	•	•	•	2.7
	2.6	CONCLUS	IONS AND	RECO	OMMEND	DATIO	NS	•	•	•	•	•	•	2.7
3.0	OBJE	CTIVES, S	SCOPE A	ND BAS	SES OF	STU	DY	•	•	•	•	•	•	3.1
	3.1	OBJECTIV	/ES AND	SCOPE		•	•	•	•	•	•	•	•	3.1
	3.2	STUDY BA	ASES ANI) PLAN	INING	ASSU	MPTION	NS .	•	•.	•	•	•	3.2
		3.2.1 F	Regulate	ory Co	onside	erati	ons	•	•	•	•	•	•	3.2
		3.2.2 F	unctio	nal Ca	apabil	litie	s	•	•	•	•	•	•	3.2
		3.2.3	Storage	Syste	ems	•	•	•	•	•	•	•	•	3.2
		3.2.4 E	Economi	c Base	es	•	•	•	•	•	•	•	•	3.3
	3.3	LEGISLAT	TIVE REG	UIREN	IENTS	•	•	•	•	•	•	•	•	3.4
		3.3.1	Interim	(Emer	gency	y) Sto	orage	of S	pent I	uel	•	•	•	3.4
		3.3.2 M	lonitore	ed Ret	rieva	able S	Storaç	ge	•	•	•	•	•	3.5
		3.3.3	Storage	of Tr	ransur	ranic	Waste	es	•	•	•	•	•	3.5
	3.4	FUEL CYC	CLE SCEN	NARIOS	5	•	•	•	•	•	•	•	•	3.6
	3.5	UNIT COS	STS AND	SCENA	RIOS	FOR	TRANSF	PORTA	TION	•	•	•	•	3.8
		3.5.1 l	Jnit Tra	anspor	rtatio	on Co	sts	•	•	•	•	•	•	3.9

		3.5.2	Trans	portati	on Sc	enari	ios	•	•	•	•	•	•	3.9
4.0	MRS/	IS/REP	OSITORY	FACILI	ΤY	•	•	•	•	•	•	•	•	4.1
	4.1	GENER	IC CONS	IDERATI	ONS	•	•	•	•	•	•	•	•	4.1
		4.1.1	Licen	sing	•	•	•	•	•	•	•	•	•	4.1
		4.1.2	Safet	у.	•	•	•	•	•	•	•	•	a	4.2
			4.1.2.1	Norma	1 Fac	ility	/ Open	ration	۱.	•	•	•	•	4.3
			4.1.2.2	Abnor	mal Oj	perat	ing (Condit	ions	•	•	•	•	4.4
			4.1.2.3	Impro	bable	Ever	its	•	•	٠	•	•	•	4.4
		4.1.3	Envir	onmenta	1 Con	sider	atio	ns	•	•	•	•	•	4.5
			4.1.3.1	Envir	onmen	tal I	[mpac	ts Dur	ing	Const	ructi	on	•	4.6
			4.1.3.2	Envir	onmen	tal I	[mpac	ts Dur	ing	Opera	tion	•	•	4.6
			4.1.3.3	Envir	onmen	tal I	[mpac	ts Dur	ing	Decom	missi	oning	•	4.7
		4.1.4	Gener	al Stan	dards	and	Crit	eria	•	•	•	•	•	4.7
		4.1.5	Quali	ty Assu	rance	•	•	•	•	•	•	•	•	4.9
			4.1.5.1	Devel	opmen	t of	QA P	rogram	n.	•	•	•	•	4.9
			4.1.5.2	QA C1	assif	icat	ions	•	•	•	•	•	•	4.10
		4.1.6	Funct	ional C	riter	ia ar	nd Sy	stem R	Requi	remen	ts	•	•	4.11
			4.1.6.1	Funct	ional	Crit	teria	•	•	•	•	•	•	4.11
			4.1.6.2	Syste	m Re q	uirer	nents	•	•	•	•	•	•	4.17
	4.2	SITE	LOCATIO	N AND D	ESCRI	PTIO	۷.	•	•	•	•	•	•	4.19
		4.2.1	Site	Locatio	n and	Arra	angem	ent	•	•	•	•	•	4.19
		4.2.2	Site	Paramet	ers	•	•	•	•	•	•	•	•	4.23
			4.2.2.1	Clima	tolog	у	•	•	•	•	•	•	•	4.23
			4.2.2.2	Hydro	logy	•	•	•	•	•	•	•	•	4.23
			4.2.2.3	Ecolo	gу	•	•	•	•	•	•	•	•	4.24

С.

	4.2	2.2.4	Environme	nt	•	•	•	•	•	•	•	4.25
	4.2	2.2.5	Terrain a	nd Geol	logy	•	•	•	•	•	•	4.25
	4.2	2.2.6	Floodplai	n Manag	gement	t	•	•	•	•	•	4.26
4.3	SYSTEM (DESCRIF	TIONS .	•	•	•	•	•	•	•	•	4.26
	4.3.1	√aste ⊦	landling F	acility	/	•	•	•	•	•	•	4.27
	4.3	3.1.1	Cask Rece	iving a	and SI	nippir	ıg	•	•	•	•	4.35
	4.3	3.1.2	Container	Transf	fer an	nd Pac	kagin	g	•	•	•	4.36
	4.:	3.1.3	Contact M	ateria	l Hano	dling	Syste	m	•	•	•	4.37
	4.3.2	Transfe	er and Stor	rage of	F Cont	tact-H	landle	d Was	tes -			1 20
		IKU22 I	actificy	•	•	•	•	•	•	•	•	4.38
	4.3	3.2.1	Structure	•	•	•	•	٠	•	•	•	4.40
	4.3	3.2.2	Material	Handlir	ng and	d Stor	age	•	•	•	•	4.40
	4.3	3.2.3	Retrieval	•	•	•	•	•	•	•	•	4.41
	4.3	3.2.4	Storage E	nviron	nent	•	•	•	•	•	•	4.42
	4.3	3.2.5	Criticali	ty Prev	ventio	on	•	•	•	•	•	4.42
	4.3	3.2.6	Radiation	Monito	oring	•	•	•	•	•	•	4.43
	4.3	3.2.7	Lighting	•	•	•	•	•	•	•	•	4.43
	4.3	3.2.8	Fire Dete	ction a	and Su	uppres	sion	•	•	•	•	4.43
	4.3	3.2.9	Ventilati	on	•	•	•	•	•	•	•	4.44
	4.3.3	Transfe	er and Sto	rage of	f Remo	ote-Ha	andled	Wast	es –			
	(Casks	• •	•	•	•	•	•	•	•	•	4.44
	4.3	3.3.1	Surface C	ask Sto	orage	•	•	•	•	•	•	4.48
	4.3	3.3.2	System Ar	rangeme	ent	•	•	•	•	•	•	4.50
	4.3	3.3.3	Component	Descr	iptio	n	•	•	•	•	•	4.52
	4.:	3.3.4	Cask Moni	toring	Syste	em	•	•	•	•	•	4.53
	4.3.4	Transfe Drywell	er and Sto Is .	rage of	f Remo	ote-Ha	andled	Wast •	es –	•	•	4.54

	4.	.3.4.1	Transpor	rtation	and P	laceme	ent Sj	ystems	5	•	•	4.54
	4.	.3.4.2	Drywell	Storage	e Fielo	d	•	•	•	•	¢	4.58
	4	.3.4.3	Drywell	Monito	ring	٠	•	•	•	•	•	5.58
	4.3.5	Service	e Facili	ties	•	•	•	•	•	•	•	4.59
	4.	.3.5.1	Administ	tration	Build	ing	•	•	•	•	•	4.59
	4	.3.5.2	Mainten	ance Bu	ilding	•	•	•	•	•	•	4.61
	4.	.3.5.3	Materia	l Wareh	ouse B	uildir	ng	•	•	•	•	4.61
	4	.3.5.4	Gate Ho	uses	•	•	•	•	•	•	•	4.61
	4.3.6	Service	e Utilit	ies .	•	•	•	•	•	•	•	4.61
	4	.3.6.1	Water S	upply	•	•	•	•	•	•	•	4.61
	4	.3.6.2	Electri	cal Pow	er Sys	tems	•	•	•	•	•	4.62
	4	.3.6.3	Sanitar	y Waste	Dispo	sal Sy	ystem	•	•	•	•	4.62
	4	.3.6.4	Communi	cations	and F	ire A	larm	Syster	n	•	•	4.62
	4	.3.6.5	Radiati	on Moni	toring	and S	Surve	illan	ce	•	•	4.63
4.4	COST ES	STIMATE	AND SCH	EDULES	•	•	•	•	•	•	•	4.64
	4.4.1	MRS/IS	Facilit	y Base	Cost a	nd Coi	nstru	ction	Sche	dule	•	4.64
	4.4.2	Cost a	nd Sched	ule: R	eferen	ce Me [.]	tal S	torage	e Cas	ks	•	4.68
	4.4.3	Cost a	nd Sched	ule: M	etal C	ask S	uppor	t Pad	S	•	•	4.68
	4.4.4	Cost a	nd Sched	ule: C	oncret	e Casl	ks	•	•	•	•	4.71
	4.4.5	Cost a	nd Sched	ule: C	oncret	e Cas	k Sup	port	Pads	•	•	4.71
	4.4.6	TRUSS	Building	s.	•	•	•	•	•	•	•	4.71
	4.4.7	Annual	Operati	ng Expe	nse	•	•	•	•	•	•	4.74
	4.4.8	Transp	ortation	Costs	•	•	•	•	•	•	•	4.75
	4.4.9	Drywel	l Storag	e.	•	•	•	•	•	•	•	4.75
	4.4.10	Decomm	issionin	g Costs	•	•	•	•	•	•	•	4.77

Ð

۴-سر

•

æ

xii

	4.5	LIFE CYCLE COSTS	•	•	•	4.77
		4.5.1 Reference Scenario Life Cycle Costs .	•	•	•	4.79
		4.5.2 Delayed Reprocessing Scenario Life Cycle Co	sts	•	•	4.79
		4.5.3 Delayed Disposal Scenario Life Cycle Costs	•	•	•	4.84
5.0	RELA	TION TO OTHER FACILITIES	•	•	•	5.1
	5.1	REACTOR POWER STATIONS	•	•	-	5.1
	5.2	REPROCESSING PLANTS	•	•	•	5.1
	5.3	GEOLOGIC REPOSITORIES	•	•	•	5.2
	5.4	LOCAL SITE SUPPORT SYSTEMS	¢	•	•	5.2
		5.4.1 Transportation Services	•	•	•	5.2
		5.4.2 Essential Services	•	•	•	5.4
		5.4.3 Other Support Services	•	•	•	5.5
6.0	RESU	LTS AND RECOMMENDATIONS	•	•	•	6.1
	6.1	RESULTS OF STUDY ANALYSES	•	•	•	6.1
		6.1.1 Comparison of Metal Storage Casks with Dryw	ells	•	•	6.4
		6.1.2 Possibilities for Cost Reduction	•	•	•	6.5
		6.1.2.1 Consolidation of Spent Fuel Assembile	es	•	•	6.5
		6.1.2.2 Shipment in Large Metal Storage Casks	s	•	•	6.5
		6.1.2.3 Combined Effect of Fuel Consolidation	n and	l		c c
	~ ~	storage Lask Transport	•	•	•	0.0
	6.2	ADVANTAGES AND DISADVANTAGES OF CO-LOCATION .	•	•	•	6.8
	6.3	RECOMMENDATIONS	•	•	•	6.9
7.0	SENS CONC	ITIVITY OF ESTIMATED COSTS TO VARIATIONS IN EPTS AND ASSUMPTIONS	•	•	•	7.1
8.0	TECH	INICAL STATUS/RESEARCH AND DEVELOPMENT REQUIREMENTS	•	•	•	8.1
	8.1	RECEIVING AND HANDLING	•	•	•	8.1

*

- ,4

"

.

a'

1

8.2	ST	ORAGE	•	•	•	•	•	•	•	•	•	•	•	8.1
8.3	RE RE	SEARCH /	AND DI	EVELOP	MENT	REQUI	REMEN	ITS	•	•	•	•	•	8.2
APPENDI)	ХА —	CONSID	ERATIO	ONS FO	OR MRS	5/IS C	OST E	EVALUA	TION	•	•	•	•	A.1
APPENDI)	КВ —	MRS/IS	FUEL	CYCLE	AND	WASTE	SCEN	NARIOS	5	•	•	•	•	B.1
APPENDI)	кс –	TRANSPO	ORTAT	ION IN	IFORMA	TION	•	•	•	•	•	•	•	C.1
APPENDI)	CD -	GENERA	L CRI	TERIA	AND S	STANDA	RDS	•	•	•	•	•	•	D.1

FIGURES

.

.

r:

2.1	Fractions of Total Undiscounted Life Cycle Attributable to Each Component of Cost, fo Each Scenario and Storage Alternative .	e Cost or	•		•	•	2.6
4.1	Flow Diagram for Spent Fuel	•	•	•	•	•	4.13
4.2	Flow Diagram for High-Level Waste	•	•	•	•	•	4.14
4.3	Flow Diagram for Remote Handled TRU Waste	•	•	•	•	•	4.15
4.4	Flow Diagram for Contact-Handled TRU Waste	2.	•	•	•	•	4.16
4.5	Location Map - Hanford Site	•	•	•	•	•	4.20
4.6	MRS/IS Facility Site Arrangement	•	•	•	•	•	4.21
4.7	Expanded MRS/IS Site Arrangement	•	•	•	•	•	4.22
4.8	Waste Handling Facility	•	•	•	•	•	4.28
4.9	Waste Handling Facility - Ground Floor Pla	an.	•	•	•	•	4.29
4.10	Waste Handling Facility - Upper Levels .	•	•	•	•	•	4.31
4.11	Waste Handling Facility - Sections and Ele	evation	s	•	•	•	4.33
4.12	Cask Receiving and Handling	•	•	•	•	•	4.35
4.13	Transuranic Surface Storage Facility .	•	•	•	•	•	4.39
4.14	The Reference Passive Cooling Dry Storage	Cask	•	•	•	•	4.45
4.15	Concrete Cask for RHTRU Waste Storage .	•	•	•	•	•	4.47
4.16	Yard Gantry Crane	•	•	•	•	•	4.49
4.17	Surface Storage Cask Unloading		•	•	•	•	4.51
4.18	Reference Drywell Encasement	•	•	•	•	•	4.55
4.19	Drywell Canister Unloading Sequence .	•	•	•	•	•	4.56
4.20	MRS/IS/Repository Arrangement	•	•	•	•	•	4.60
4.21	Postulated MRS/IS Facility Design and Cons	structi	on Sch	nedule	2	•	4.65
6.1	Fractions of Total Undiscounted Life Cycle to Each Component of Cost, for Each Scenar Alternative	e Cost / rio and	Attrik Stora	outabl age	e		63
		•	•	•	•	•	0.0

TABLES

¥.

۲ بر

.

•

8

4

.

`

2.1	System Life Cycle Cost	•	2.5
2.2	Effects of Changes in Study Bases	•	2.7
3.1	Reference Transportation Systems Selected for this Study .	•	3.10
3.2	Round-Trip Transportation Costs for Truck and Rail Shipments of Spent Fuel and High-Level and Transuranic Wastes	•	3.11
3.3	Reference Canister Sizes and Weights for Offsite Transportation	•	3.12
3.4	Annual Number of Incoming and Outgoing Shipments at the MRS/IS Facility (Reference scenario)	•	3.13
3.5	Annual Number of Incoming and Outgoing Shipments at the MRS/IS Facility (Delayed Reprocessing scenario)	•	3.14
3.6	Annual Number of Incoming and Outgoing Shipments at the MRS/IS Facility (Delayed Disposal scenario)	•	3.15
4.1	Reference Heat Emission Rates	•	4.17
4.2	Reference Gamma Dose Rate and Neutron Emission Rates $$.	•	4.18
4.3	Reference Physical Characteristics of Wastes	•	4.18
4.4	MRS Reference Scenario Storage Requirements	•	4.40
4.5	Reference Metal Storage Cask Design Data	•	4.46
4.6	Typical Surface Radiation Levels of Remote-Handles Material	•	4.48
4.7	Construction Capital Cost Summary	•	4.66
4.8	Cost Estimating Factors	•	4.67
4.9	Construction Costs for Utilities	•	4.68
4.10	Schedule and Costs for Annual Purchases of Metal Storage Casks	•	4.69
4.11	Schedule and Costs for Annual Construction of Storage Pads and Storage Fields for Metal Casks	•	4.70

4.1	L2 Schedule and Costs for Annual Purchases of Concrete Storage Casks	•	4.72
4.1	13 Schedule and Costs for Annual Construction of Storage Pads and Storage Fields for Concrete Casks	•	4.73
4.1	L4 Yearly Operating Costs for the MRS/IS Facility	•	4.74
4.1	L5 Annual Transportation Costs for Each Scenario	•	4.76
4.1	L6 Schedule and Costs for Annual Construction of Drywells and Drywell Fields	•	4.78
4.1	<pre>L7 MRS/IS Facility Co-located With a RepositoryReference Scenario, Life-Cycle Cash Flows: Cask Storage</pre>	•	4.80
4.1	MRS/IS Facility Co-located With a RepositoryReference Scenario, Life-Cycle Cash Flows: Drywell Storage	•	4.81
4.1	19 MRS/IS Facility Co-located With a RepositoryDelayed Reprocessing Scenario, Life-Cycle Cash Flows: Cask Storage	•	4.82
4.2	20 MRS/IS Facility Co-located With a RepositoryDelayed Reprocessing Scenario, Life-Cycle Cash Flows: Drywell Storage	•	4.83
4.2	MRS/IS Facility Co-located With a RepositoryDelayed Reprocessing Scenario, Life-Cycle Cash Flows: Cask Storage	•	4.85
4.2	22 MRS/IS Facility Co-located With a RepositoryDelayed Disposal Scenario, Life-Cycle Cash Flows: Drywell Storage .	•	4.86
5.1	l Items and Functions Shared or Used by Both MRS/IS Facility and the Repository	•	5.3
6.1	Components of Life Cycle Costs, Percentages and Totals .	•	6.2
6.2	2 Undiscounted and Discounted Life Cycle Costs for the Scenarios and Storage Alternatives Studied	•	6.4
6.3	B Effect of Fuel Assembly Consolidation on MRS/IS System Life Cycle Costs	•	6.6
6.4	Effect of Shipment in Metal Storage Casks on Waste Management System Costs	•	6.7
6.5	Combined Effect of Fuel Consolidation and Shipment in Storage Casks on Waste Management System Costs	•	6.7
7.1	Estimated Life Cycle Costs and Possible Variations	•	7.2

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1.0 INTRODUCTION

Until 1975, commercial power reactor owners had planned to store spent fuel at the reactor for a short period prior to shipment to a reprocessing plant. Reactors built in that era generally has storage space for only one or two batch discharges of spent fuel plus a full core discharge capability. However, changes in recent years in federal policies regarding reprocessing and/or disposal of spent nuclear reactor fuel have produced delays in the development of fuel reprocessing plants and deep geologic disposal facilities. As a result, many nuclear power plants are faced with the possibility of shutdown due to lack of spent fuel storage capacity. In recognition of this problem, legislative initiatives are underway in Congress to provide appropriate storage and disposal facilities. In response to these legislative initiatives, the Department of Energy (DOE), through its Office of Nuclear Fuel Cycle, has established a program to examine the various alternatives for storage of spent nuclear fuel, solidified high-level wastes (HLW), and transuranic (TRU) wastes until an appropriate deep geologic repository is available for disposal of these wastes. One of these alternatives, a monitored retrievable storage/interim storage (MRS/IS) facility built on the site of a future repository, is the subject of this study.

The storage facility evaluated in this study employs dry handling and storage methods, utilizing a large hot cell facility, metal casks or drywells, concrete casks, and a surface warehouse.

The study objectives, scope, and study bases are presented in Section 3. A preconceptual design for the facility is given in Section 4, together with estimates of construction, operating, and life cycle costs. The relationship of the MRS/IS facility to other parts of the nuclear fuel cycle and to local site support systems is discussed in Section 5. The results of the cost analyses, the advantages and disadvantages of co-location with a repository, and recommendations for further action are given in Section 6. The sensitivity of the estimated life cycle costs to variations in the study bases is examined in Section 7, and the status of system component development and areas needing further research and development are discussed in Section 8.

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2.0 SUMMARY

The Office of Nuclear Fuel Cycle of the Department of Energy (DOE) has established a program to examine the various alternatives for monitored retrievable storage (MRS) and interim storage (IS) of spent nuclear fuel, solidified high-level waste (HLW), and transuranic (TRU) waste until such time as appropriate geologic repository/repositories are available. The alternatives being examined are: 1) a facility co-located with a reprocessing plant, 2) a facility located separate from any other facilities, and 3) a facility co-located with a geologic repository. The facility examined in this study is located on the site where a geologic repository is to be developed, and it becomes the principal surface facility of the repository when the repository is opened, thus avoiding duplication of the facilities.

The objectives of this study are to develop a preconceptual design for an MRS/IS facility to be co-located on the same site as a geologic repository, to estimate the life cycle costs, and to examine the transportation, licensing, safety, and environmental issues associated with such a facility.

2.1 STUDY BASES

A number of bases and assumptions are made to facilitate the analyses of the MRS/IS/Repository concept. These include:

- Construction, operation, and decommissioning of the facility are major federal actions and are subject to the requirements of the National Environmental Policy Act (NEPA); the facility is subject to licensing by the Nuclear Regulatory Commission.
- 2. The facility utilizes passively cooled dry storage devices (metal casks, drywells) for storing spent fuel and canisters of HLW, concrete casks for storing remote-handled TRU (RHTRU) wastes, and a warehouse for storing contact-handled TRU (CHTRU) wastes.
- 3. Transport of the radioactive wastes is accomplished using existing or currently designed truck and rail shipping containers.
- 4. All costs are based on mid-1982 prices, with future expenditures discounted 2 percent per year from mid-1982.

- 5. The facility is assumed to have the capability to receive, package as necessary, store, retrieve, and ship radioactive waste materials either offsite or to the co-located repository.
- The highly radioactive materials (spent fuel, HLW, and RHTRU) are assumed to be from reactor fuel that has cooled for at least 10 years since discharge from a reactor.

The types and quantities of radioactive wastes to be handled by the facility are defined by three principal scenarios: reference, delayed reprocessing, and delayed disposal. In all scenarios, the MRS/IS facilities do not receive any material for storage until 1990. Prior to 1990, spent fuel is assumed to be stored at reactor sites.

In the Reference scenario, reprocessing plants with capacities of 1500, 1500, 3000, and 3000 metric tons of heavy metal (MTHM) per year are placed in operation in the years 1989, 2000, 2005, and 2010, respectively. Geologic repositories with capacities of 1800 MTHM per year in each of the first 5 years of operation and 3000 MTHM per year in each of the succeeding 21 years of operation are postulated to be placed in operation in the years 1998, 2002, and 2015.

In the Delayed Reprocessing scenario, the initial operation of the reprocessing plants is delayed 10 years.

In the Delayed Disposal scenario, the initial operation of the repositories is delayed 10 years. All spent fuel is postulated to be reprocessed, with only solidified HLW and TRU wastes placed in the repositories.

Transportation of the radioactive materials is accomplished using presently available or designed shipping containers, with the volume of material divided evenly between truck and rail transport systems. Large numbers of shipments are required. The maximum numbers of truck and rail shipments made annually to and/or from the facility are: in the Reference scenario, 864 and 142; in the Delayed Reprocessing scenario, 3473 and 454; and in the Delayed Disposal scenario, 2445 and 579. The costs of transportation

considered in this study are just those incremental costs attributable to utilizing the MRS/IS facility, not the total transport costs associated with the waste management system.

2.2 CONCEPTUAL FACILITY CHARACTERISTICS

The facility considered in this analysis is postulated to be located on the Hanford Site, and has reasonable access to highways and rail-track, electrical service, process water supplies, heavy equipment and transportation services, and security services available on the Site.

The site for the MRS/IS facility is postulated to be located west of the 200 West area, and occupies about 400 acres of land. In comparison, an area of about 550 acres is projected to be required for the surface support facilities for the geologic repository.

The reference MRS/IS facility consists of three principal sections: the Waste Handling Facility (WHF), the storage areas, and the support facilities, with appropriate interfaces. The WHF encompasses the receiving and shipping stations for transport casks, the shielded cells for inspection, encapsulation (if needed), container decontamination, and delivery to the onsite transport system of the received radioactive materials. All materials are received dry and are maintained dry throughout the handling and storage operations.

The storage areas include large fenced areas containing support pads for metal storage casks or drywells, depending upon which concept is used for storage of spent fuel and HLW, storage areas containing support pads for concrete storage casks used in storing RHTRU wastes, and large concrete warehouse(s) for storage of CHTRU wastes. Each of the storage systems has provisions for monitoring each of the system's containment barriers for detection of release of radioactive material. A reference metal storage cask (REA 2023) and a reference drywell are postulated for this analysis.

Onsite transporter systems are employed to transfer the spent fuel, HLW, and RHTRU from the WHF to the storage areas. For the metal and concrete casks, a tractor-trailer unit is used to move the loaded casks from the WHF to the storage areas, where a large gantry crane places the casks onto the

storage pads. For the drywell, a shielded transporter is used which couples with the top of the drywell for insertion of the sealed canister containing spent fuel or HLW.

CHTRU wastes are received at the TRU Surface Storage (TRUSS) facility and stored using normal warehousing equipment. The TRUSS building is constructed of precast concrete and has appropriate ventilation and monitoring systems to minimize the potential for release of radioactive materials to the environment. The TRU wastes stored in the TRUSS facility are assumed to have been concreted within their shipping and storage containers to reduce the potential for dispersion of TRU materials in the event of an accident that breaches the containers.

The conventional support facilities include an administration building, maintenance building, material warehouse, gate houses, sanitary disposal system, water and electrical supply systems, and communication and fire alarm systems.

2.3 CONSTRUCTION SCHEDULE AND COST ESTIMATES

Design of the MRS/IS facility is estimated to require about 30 months, with construction initiated about 15 months after the start of the design work. Construction is estimated to require about 48 months. Elapsed time from authorization to initial operation is postulated to be about 66 months.

The total cost of the basic facility, including the initial storage areas and warehouse, is estimated to be \$178 million in mid-1982 dollars. Direct construction costs are about \$105 million, with engineering, indirect, and other costs and contingencies comprising an additional \$73 million.

2.4 SYSTEM LIFE CYCLE COST

The life cycle cost of an MRS/IS facility co-located with a repository is comprised of the capital construction cost, capital and operating costs during operation, and decommissioning costs. The direct construction costs are estimated to be \$178 million. Operating costs are estimated to be about \$11 million per year, plus canister materials when using drywells.

Purchases of metal storage casks during the lifetime of the facility are estimated to cost from \$306 million to \$1.768 billion, depending upon the scenarios. Purchases of drywells in lieu of metal casks are estimated to cost from \$90 million to over \$509 million. Purchases of concrete storage casks are estimated to cost from about \$42 million to over \$243 million.

Decommissioning of the MRS/IS facility is limited to the decontamination and disposal of the storage casks and/or drywells and removal of the storage pads. The rest of the facility becomes part of the repository system and would be decommissioned when the repository is closed. It is anticipated that, at least when metal casks are used, the salvage value of the casks will exceed the other costs of decommissioning. Hence, no net cost is assigned to decommissioning in this study.

The life cycle cost of the MRS/IS system is summarized in Table 2.1 for the three principal scenarios, both undiscounted and discounted at the rate of 2 percent per year.

The fractions of total undiscounted life cycle cost attributable to each component of cost are illustrated in Figure 2.1 for each of the three principal scenarios and storage alternatives.

TABLE 2.1. System Life Cycle Cost^(a)

	Reference	Delayed	Delayed
	Scenario	Reprocessing	Disposal
Undiscounted:			
Metal Casks	0.731	2.257	2.487
Drywells	0.518	1.973	1.235
Discounted:			
Metal Casks	0.578	1.592	1.661
Drywells	0.412	1.376	0.868

(a) Billions of dollars.



FIGURE 2.1. Fractions of Total Undiscounted Life Cycle Cost Attributable to Each Component of Cost, for Each Scenario and Storage Alternative

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2.5 SENSITIVITY OF COSTS TO CONCEPTS AND ASSUMPTIONS

As shown in Figure 2.1, two components of cost, transportation (in the Delayed Reprocessing scenario) and metal casks or drywells, contribute most of the cost and are logical candidates for examination for cost reduction.

If drywells are utilized instead of metal casks, the life cycle cost is reduced by 29.1, 12.2 and 50.3 percent for the Reference, Delayed Reprocessing, and Delayed Disposal scenarios, respectively.

If spent fuel assemblies are disassembled and consolidated into closely packed containers at the reactor sites prior to shipment, the number of shipments is cut in half, as is the number of casks needed to store spent fuel.

The use of larger shipping casks (i.e., the reference metal storage cask) also greatly reduces the number of shipments required. The effects of these changes in the study bases are summarized in Table 2.2, for the base case of using the reference metal cask.

TABLE 2.2. Effects of Changes in Study Bases

	Reference <u>Scenario</u>	Delayed Reprocessing	Delayed Disposal
Undiscounted Life Cycle Cost (\$ Billions)	0.731	2.294	2.487
Fuel Consolidation at Reactor Sites (% change)		-41.4	
Ship in Storage Casks (% change)	-36.2	-50.2	-45.3
Fuel Consolidation and Shipment in Storage Casks (% change)	-36.2	-66.5	-45.3

2.6 CONCLUSIONS AND RECOMMENDATIONS

Several conclusions can be drawn from the results of this study. First, co-locating the MRS/IS facility with a repository has several advantages. Overall waste management costs can be reduced by eliminating the duplication

of facilities that would occur if the MRS/IS facility and the repository were located separately. Amortization of the capital expenditures on facilities would take place over a longer period of time, perhaps 40 years rather than the 15- to 20-year life of the MRS/IS facility, thereby reducing total system costs. In addition, the stored materials would be transferred directly from storage to the repository, without leaving the site, thereby minimizing the potential for transportation accidents and the possible exposure of the public resulting from such accidents.

Second, the likely cost of an MRS/IS system is large, \$0.5 to \$2.5 billion. Thus, all avenues available for reducing costs should be explored. Based on the unit costs assumed for the reference metal cask and for the reference drywell, the drywell is less expensive by from 12 to 50 percent. Use of fuel consolidation and larger shipping casks has the potential to reduce system costs by from 36 to 66 percent.

Third, the basic technology needed to construct and operate an MRS/IS facility is generally well-developed. Additional information on allowable fuel element cladding temperatures in dry storage would be very helpful, as would the development of validated heat transfer calculational codes for predicting cladding temperatures. Also, information to assist in the licensing of large storage casks for use in shipment as well as in storage would be very useful.

Fourth, a review of the scenarios examined in this study and the associated transportation costs suggests that the waste management system might be considerably more cost-effective if there were two MRS/IS facilities, one located at the reprocessing plant to hold spent fuel for reprocessing, and one located at the repository to store HLW and TRU wastes until the repository is placed in operation. This situation is not examined in this study, but should be evaluated before establishing a site-specific program.

Finally, in view of the massive quantities of radioactive material to be stored and the time duration of the storage, the use of a water pool for storage of spent fuel, HLW, and RHTRU might be cost-effective. A detailed analysis of a water pool facility comparable with the analysis presented in this study for dry storage facilities should be made before embarking on the construction of a cask or drywell storage facility.

3.0 OBJECTIVES, SCOPE, AND BASES OF STUDY

The monitored retrievable storage/interim storage (MRS/IS) facility is conceived as a government-owned, contractor-operated facility for providing temporary storage for spent fuel and/or reprocessing wastes. The MRS/IS program would provide federal contingency capability for storing spent nuclear fuel until reprocessing facilities can eliminate the need for such storage, and would provide federal capability for storing solidified high-level wastes (HLW) and transuranic (TRU) wastes until appropriate waste disposal repositories become available. It is assumed that the actual repository will not exist when the MRS/IS facility is built. Therefore, consideration of facility capabilities that could initially serve the needs of the MRS/IS facility and subsequently serve the needs of the repository is an important aspect of this study, in terms of projecting life cycle costs. Similarly, support services, in the form of existing roads, railroads, and other utility services, and extensions of those services, as they apply to the MRS/IS/Repository, are also important considerations.

3.1 OBJECTIVES AND SCOPE

The objectives of this study are to: 1) develop a preconceptual design for an MRS/IS facility to be co-located on the same site as a geologic repository, 2) to estimate the life cycle costs, and 3) to examine the transportation, licensing, safety and environmental issues associated with such a facility.

The scope of this study is limited to consideration of an MRS/IS facility that is located on a site with a geologic repository. The functional requirements of the facility include the ability to receive, handle, transfer, store, and ship spent reactor fuel, solidified HLW, and transuranic wastes, both contact-handled (CHTRU) and remote-handled (RHTRU). Storage concepts considered are: 1) dry storage casks, 2) drywells, and 3) warehouse storage for CHTRU. The MRS/IS facility is to be constructed on a modular basis, with additional storage space developed annually to accommodate the quantities of waste projected to need storage each year. All wastes are to be stored in a retrievable manner.

3.2 STUDY BASES AND PLANNING ASSUMPTIONS

To facilitate comparison of the study results, a number of generic assumptions have been made to provide a common basis for the individual site studies. These are: 1) the facility is located and constructed so it can also serve as the basic surface facility for a permanent geologic repository, and 2) facility capabilities and capacities are based on the assumption that no additional pool expansions or dry storage at reactors are available or used. Basic assumptions are identified in the following subsections.

3.2.1 Regulatory Considerations

Building and operating an MRS/IS facility is a major action by the federal government and is subject to the requirements of the National Environmental Policy Act (NEPA). The facility is also subject to licensing by the Nuclear Regulatory Commission (NRC).

The interim storage facility will be decommissioned after its contents are transferred to permanent repositories.

3.2.2 Functional Capabilities

The facility has the capability to receive materials from reactors and reprocessing plants and to ship material to reprocessing plants as well as to repositories. The facility also has the capability to repackage any material received from offsite as well as to repackage any onsite material as required for offsite transport. In addition, it has the capability to receive and to ship materials by both rail and highway vehicles.

Casks used for shipment of material to and from the MRS/IS facility are either those currently licensed for the shipment of irradiated commercial fuel assemblies and TRU wastes or are newly developed ones similar in design and handling requirements. One or more of the casks has the capability of transporting either spent fuel or solidified commercial high-level waste.

3.2.3 Storage Systems

The facility will accept both assembled and disassembled commercial pressurized water (PWR) and boiling water (BWR) reactor fuel that can be identified and is known to comply with certain specified requirements.

The facility will accept identifiable solidified high-level waste forms that are known to comply with specified heat, containment and physical condition requirements.

The facility will accept identifiable transuranic wastes that comply with specified contents, packaging and physical condition requirements.

Storage is provided for spent fuel, solidified commercial high-level wastes, and transuranic wastes only until disposal in the repository is available.

3.2.4 Economic Bases

All costs developed in this study are presented in terms of constant, unescalated mid-1982 dollars, including expenditures that are made in future years. Interest rates and inflation or escalation rates are difficult to predict, but the difference between interest and inflation rates tends to be around 2 percent, essentially independent of the actual values of the individual interest and inflation rates. Therefore, in developing the present values of future expenditures in this study, a discount rate of 2 percent is used.

Costs are developed in terms of expenditures per year, covering the construction, operation and decommissioning of the MRS/IS facility. The costs of transporting the radioactive materials from their points of origin to the MRS/IS facility are developed separately, but are included in the total life cycle cost of the system. Each total annual expenditure is discounted to mid-1982. The discounted annual expenditures are summed to obtain the present values of the lifetime expenditures for the facility, thus permitting comparisons between design concepts that may have different expenditure patterns.

A detailed discussion of the methods used in this study to develop the estimates of capital, operating, and decommissioning costs is presented in Appendix A of this report.

3.3 LEGISLATIVE REQUIREMENTS

A number of bills are presently under consideration by Congress which deal with the topics of interim (emergency) storage of commercial spent nuclear fuel, monitored retrievable storage of spent fuel, solidified high-level wastes, transuranic wastes, and permanent disposal of these nuclear wastes in deep geologic repositories.

Each of the bills under serious consideration (S.1662, H.R.3809, H.R.6589) has provisions for the establishment of repositories, mechanisms to assure full recovery of the costs of storage and disposal operations from the waste generators, and procedures to assure that interested states and Indian tribes can be involved in the siting process. Several of the proposed bills differ regarding who has title to the radioactive material while in storage prior to final disposal in a repository. The federal government takes title in one bill (S.1662), and the waste generators retain title in the other two bills (H.R.3809, H.R.6589).

Specific provisions unique to interim storage, monitored retrievable storage, and transuranic waste storage are discussed in the following subsections.

3.3.1 Interim (Emergency) Storage of Spent Fuel

The bills contain language that would make licensing of additional storage capacity at existing reactor sites easier, by eliminating some of the issues that would otherwise have to be considered (availability or desireability of alternatives, the need for power from the reactor, any issues relating to reactor operation, etc.).

The capacity of the interim (emergency) storage facilities would be limited [1700 (H.R.3809) or 2800 (S.1662) metric tons], would be exempt from licensing if located at an existing federal site (H.R.3809), and would not be a major federal action as defined in the NEPA (H.R.3809). The operation of an interim (emergency) storage facility is limited to 5 to 7 years (President's letter), or 8 to 12 years (S.1662).

The interim (emergency) storage provisions are intended to provide a way to avoid shutdown of operating power reactors in case full core discharge capability is lost as the quantities of fuel in storage pools approach the pool's capacity. This type of storage is intended as a very limited effort, of relatively short duration. Longer-term storage of radioactive materials such as spent fuel, solidified high-level waste, and transuranic waste would be provided for by monitored retrievable storage facilities, which are discussed in the next subsection.

3.3.2 Monitored Retrievable Storage

The DOE is directed to submit to Congress within 1 year of passage of the enabling legislation a proposal to develop one or more MRS facilities. This proposal is to include site-specific designs, specifications and cost estimates, and a plan for integrating the MRS facilities with the deep geologic disposal repositories also mandated by the legislation.

In all cases, an environmental assessment (EA) is required at the time the proposal is submitted, with an environmental impact statement (EIS) to be issued before construction is initiated. The MRS must be licensed by the NRC. During the NEPA and licensing processes, issues normally considered, such as the need for the facility, alternate sites, and alternate designs, need not be considered.

No specific instructions are given in the various House bills regarding the capacity of an MRS facility. However, in the Senate bill (S.1662), until a second repository is in operation, a limit of 70,000 metric tons of spent fuel is placed on the combined capacity of an MRS facility and the first repository when located within 50 miles of each other.

Similarly, no clearly defined limitation is proposed for the duration of MRS operations. Instead, the MRS facilities are to remain in service until geologic repositories are available.

3.3.3 Storage of Transuranic Wastes

The storage of transuranic wastes is addressed specifically in the House bills, with the intent of storing these materials until a geologic repository is available. If located on a federal site, the storage facility would not be subject to licensing or the NEPA. Several time constraints are proposed in the pending legislation: 1) the NRC shall issue regulations governing TRU storage within two years of passage; 2) DOE shall cease accepting TRU wastes for storage when an appropriate repository is available, or 6 years after NRC has issued their regulations, whichever occurs first. Thus, TRU wastes would be accepted for storage for a maximum of 8 years following passage of the enabling legislation.

3.4 FUEL CYCLE SCENARIOS

Three principal scenarios and two alternative scenarios (developed in Appendix B) are examined for their impact on the life cycle cost of the MRS/IS facility co-located with a repository. The storage facility is postulated to begin operation in 1990, with spent fuel requiring storage prior to that time being stored at reactor sites.

In the Reference scenario, reprocessing plants are postulated to come on-line in the years 1989, 2000, 2005, and 2010, with capacities of 1500, 1500, 3000, and 3000 metric tons of heavy metal (MTHM) per year, respectively. Geologic repositories are postulated to be placed in operation in the years 1998, 2002, and 2015, with capacities of 1800 MTHM per year in each of the first 5 years of operation and 3000 MTHM per year in the succeeding 21 years of operation.

In the Delayed Reprocessing scenario, startup of each of the reprocessing plants is delayed 10 years, to the year 1999, 2010, 2015, and 2020, with the repository schedule remaining the same as that of the Reference scenario.

In the Delayed Disposal scenario, reprocessing starts in 1989, as in the Reference scenario, but opening of the repositories is delayed 10 years to the years 2008, 2012, 2015, and 2025.

The alternative scenarios, Early Disposal and Delayed Disposal with No Reprocessing, represent the lower- and upper-bound situations for storage of material in the MRS/IS facility, and are not analyzed in this study.

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In the three principal scenarios it is assumed that all spent fuel is eventually reprocessed. It is also assumed that there is only a single MRS/IS facility serving the U.S. nuclear power industry. Thus, in the Delayed
Reprocessing scenario, many spent fuel assemblies (~30,000) are stored for an extended period of time (~30 years), but little or no reprocessing waste must be handled. Conversely, in the Delayed Disposal scenario, no spent fuel is stored, but massive quantities of reprocessing wastes are stored for an extended time period.

For the Reference scenario, the maximum number of incoming HLW canisters that must be handled annually is 700 in the years 1992 through 1997. The maximum numbers of incoming remote-handled transuranic (RHTRU) canisters, RHTRU drums, contact-handled transuranic (CHTRU) drums, and CHTRU boxes that must be handled annually are 549, 698, 4868, and 41, respectively, in the years 1992 through 1997. The maximum inventory of HLW and TRU wastes occurs in the year 1997, just prior to the opening of the repository, with 4900 HLW canisters, 3845 RHTRU canisters, 4299 RHTRU drums, 34,076 CHTRU drums, and 286 CHTRU boxes.

For the Delayed Reprocessing scenario, the maximum number of spent fuel assemblies that must be handled annually is 9590, in the year 2016, when the fuel is being shipped to the reprocessing plants. The maximum inventory of spent fuel assemblies stored in the MRS/IS facility is 26,981, in the year 1997. The bulk of these assemblies remain in storage until the year 2012 when reprocessing plant capacity exceeds the output from the operating reactors. Since the repositories will be in operation before any HLW or TRU wastes are created, all of these materials will go directly to the repository.

For the Delayed Disposal scenario, the maximum number of incoming HLW canisters that must be handled annually is 2,334 in the year 2007. The maximum numbers of incoming RHTRU canisters, RHTRU drums, CHTRU drums, and CHTRU boxes that must be handled annually are 1,830, 2,327, 16,227, and 135, respectively, in the year 2007. The maximum inventory of HLW and TRU wastes occurs in the year 2016, just following the opening of the third repository, with 29,598 HLW canisters, 22,157 RHTRU canisters, 28,169 RHTRU drums, 192,923 CHTRU drums, and 1,643 CHTRU boxes.

The repository co-located with this MRS/IS facility is assumed to come on-line in 1998 for both the Reference and the Delayed Reprocessing scenarios. Since all of the original MRS/IS facility except the interim

storage areas would then be serving and supporting the underground repository, there would be no further activities related to interim storage. The removal of the wastes stored in the various interim storage areas and their transfer to the repository are assumed to be parts of the repository operation. As indicated in Appendix B, this transfer would be accomplished over a period of several years.

Although the repository co-located with this MRS/IS facility would come on-line in 2008 in the Delayed Disposal scenario, the storage facility would still be required to receive wastes until after the second and third repositories open in 2012 and 2015, respectively. Assuming the first repository would be co-located with this MRS/IS facility, then the activities of this facility would be shared with the repository from 2008 to 2016. At that time, all activities would be transferred to the repository.

3.5 UNIT COSTS AND SCENARIOS FOR TRANSPORTATION

A significant portion of the cost of operating a waste management system is attributable to the cost of transporting the spent fuel and reprocessing wastes. These costs are also quite sensitive to the scenario for system operation that is selected for analysis. The base unit costs associated with transport of the radioactive materials are presented in this subsection, together with a summary of the transportation links postulated for the MRS/IS facility co-located with a repository for the three principal fuel cycle scenarios. Additional details concerning transportation costs and transport scenarios are given in Appendix C.

3.5.1 Unit Transportation Costs

Unit transportation costs are presented for four fuel-cycle materials: spent fuel, HLW, RHTRU wastes, and CHTRU wastes. RHTRU wastes are further subdivided into three categories: wastes that are packaged in special cylindrical canisters (including compacted cladding hulls), wastes that are packaged in "standard" 210-liter (55-gal) drums with surface dose rates less than 5 R/hr, and drummed wastes with surface dose rates greater than 5 R/hr. Transportation costs are calculated for shipments by truck and by rail.

Transportation links of 500 miles and 2500 miles one way are evaluated. Transportation costs are evaluated only between the boundary fences of the sending and receiving facilities. All handling costs and truck/cask demurrage charges accrued within the MRS/IS facility boundary are attributed to operating costs. Rail car/cask demurrage charges are included in the unit shipping costs.

The reference transportation systems evaluated for this study are listed in Table 3.1. These systems are selected based on availability, licensability, and compatibility with the reference waste packages.

Transportation costs are based on the assumption that private industry will provide the transportation services as a commercial venture, although the services could be owned and provided by the government. Therefore, total transportation costs are the sum of the shipping charges, special equipment and security costs (where applicable) and shipping container rental fees. The unit transportation costs for truck and rail shipments of the six different cargoes are summarized in Table 3.2.

Special equipment charges and security costs are currently required for shipments of spent fuel and may be required for shipments of high-level wastes in the future. The costs for HLW shipments shown in Table 3.2 include these additional costs.

3.5.2 Transportation Scenarios

The transportation requirements are derived from the fuel cycle scenarios developed in Section 3.4 and Appendix B. The primary assumptions used to calculate the number of shipments for each scenario include:

- All waste volumes are transported from the source site(s) to the MRS/IS facility by rail and truck. Fifty percent of the waste volume is assumed to be delivered by rail and 50 percent of the waste volume is assumed to be delivered by truck.
- The transportation containers and their load capacities for each of the waste forms are as listed in Table 3.1.

Material	Shipping Mode	Shipping Container	Waste Packages Per Shipment	Leasing Fee <u>(\$/Day)</u>
Spent Fuel	Truck	NAC-1	1 PWR or 2 BWR	2000(a)
	Rail	IF-300	7 PWR or 18 BWR	5750
High-Level Wastes	Truck	NAC-1	l canister	2000
	Rail	IF-300	5 canisters	5750
RHTRU Special Canister	Truck	H∟₩—T	11 canisters	1750
	Rail	HLW-R	5 canisters	4375
RHTRU Drums <5 R/hr	Truck	CNS 14-170	14 drums	175
	Rail(b)	CNS 14-170	42 drums	525
RHTRU Drums >5 R/hr	Truck	CNS 7-100	7 drums	175
	Rail(b)	CNS 7-100	21 drums	525
CHTRU wastes	Truck	TRU-PACT	36 drums or 3 boxes	700
	Rail(c)	TRU-PACT	72 drums or 6 boxes	1400

TABLE 3.1. Reference Transportation Systems Selected for this Study

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(a) Leasing fee for the NAC-1 is calculated from a schedule.

(b) It is assumed that three of these shipping containers can be transported per rail car.

(c) Assumes two truck TRU-PACT versions are transported per rail car.

		Round-Trip	o Unit Transpor	tation Costs
	Shipping	One-Way	/ Miles (%/Shim	ment) ^(b,c)
Material	Mode	500	2000	2500
Spent Fuel(d)	Truck	12,170	29,010	34,710
	Rail	91,140	216,920	262,240
High-Level(d)	Truck	12,200		34,210
wastes	Rail	91,210		262,410
RHTRU Wastes;	Truck	9,280		23,030
Special canisters	Rail	69,670		193,770
RHTRU Wastes: Drums <5 R/br	Truck	3,450		10,825
	Rail	21,090		57,530
RHTRU Wastes; Drums >5 R/br	Truck	3,380		10,645
	Rail	20,770		55,680
CHTRU Wastes	Truck	5,310		14,380
	Rail	25,600		70,600

TABLE 3.2. Round-Trip Transportation Costs for Truck and Rail Shipments of Spent Fuel and High-Level and Transuranic Wastes(a)

(a) Transportation costs include shipping charges, special equipment and security costs (where applicable) and shipping system rental fees.

(b) Rounded to the nearest 10 dollars.

(c) These costs do not include demurrage fees for truck shipments which are, on average, \$29.30 for each hour of turnaround time at the terminal facilities. Rail demurrage fees are included in shipping system rental fees.

(d) Costs include charges for special equipment and escort services.

- The size, weight and capacity of the containers considered for use are shown in Table 3.3.
- The MRS/IS facility goes into service in 1990. Prior to that time, spent fuel requiring storage is held either at the reactor sites or in a temporary storage facility located on a government site.
- Only those incremental offsite transportation costs associated with the MRS/IS facility that are in addition to the transportation costs normally required in the waste management system without an MRS/IS facility are included in the MRS/IS facility life cycle costs.

Other background, bases, and assumptions used for the transportation aspect of this study are given in detail in Appendix C.

The annual number of incoming or outgoing shipments for the Reference scenario is listed in Table 3.4. The maximum number of shipments received at the facility occurs in the years 1992 through 1997. During each of those years, 651 truck shipments and 135 rail shipments will require remote handling, and 75 truck shipments and 38 rail shipments of CHTRU will also be processed by the MRS/IS facility.

Fuel Cycle Material	Dimensions, m	Net ^(a) Capacity, m ³ (ft ³)	Average Weight Loaded, kg (1b)
Spent fuel PWR assembly BWR assembly	NA NA	NA NA	658 (1448) 284 (625)
Solidifed high-level waste canister	0.31 D x 3.1	0.17 (6.0)	1050 (2310)
RHTRU wastes Hulls canister 210 L (55 gal) drum	0.62 D x 3.1 0.62 D x 0.92	0.75 (2.6) 0.17 (6.0)	3500 (7700)
CHTRU wastes 210 L (55-gal) drum Metal box	0.62 D x 0.92 1.2 x 1.9 x 1.9	0.19 (6.7) 3.5 (123.6)	300 (660) 4000 (8800)

TABLE 3.3. Reference Canister Sizes and Weights for Offsite Transportation

NA = Not Applicable

(a) Based on maximum of 80 percent full.

	ł	ILW	RHT	FRU	СНТ	RU
Year	Rail	Truck	Rail	Truck	Rail	Truck
90	24	117	23	99	13	26
91	47	234	44	201	25	50
92	70	350	65	301	38	75
93	70	350	65	301	38	75
94	70	350	65	301	38	75
95	70	350	65	301	38	75
96	70	350	65	301	38	75
97	70	350	65	301	38	75
98-00	0	0	0	0	0	0
01	10	47	0	0	0	0
02-10	0	0	0	0	0	0
11	47	234	5	1	3	5
12	24	117	0	0	0	0
13	42	210	26	120	16	30
14	70	350	26	120	16	30
15	0	0	0	0	0	0

TABLE 3.4. Annual Number of Incoming Shipments at the MRS/IS Facility (Reference scenario)

For the Delayed Reprocessing scenario, the MRS/IS facility is used to store spent fuel exclusively, since the repository is opened in 1998. The annual number of incoming shipments for the Delayed Reprocessing scenario is listed in Table 3.5. The maximum annual number of incoming shipments of spent fuel occurs in the years 1996 and 1997 when over 2100 shipments are received each year. The maximum number of shipments away from the MRS/IS facility occurs in the year 2016 when nearly 4000 shipments are made.

The annual number of shipments for the Delayed Disposal scenario is listed in Table 3.6. The maximum number of incoming shipments occurs in the year 2011 when over 3000 shipments of waste are received at the MRS/IS facility. During that year, it is estimated that 2201 truck shipments and 456 rail shipments will arrive which will require remote handling. In addition, 244 truck shipments and 123 rail car shipments of incoming CHTRU wastes will be received at the MRS/IS facility.

TABLE 3.5. Annual Number of Incoming and Outgoing Shipments at the MRS/IS Facility (Delayed Reprocessing scenario)

	Spent	Spent Fuel		
Year	Rail	Truck		
90	76	583		
91	84	696		
92	107	819		
93	110	832		
94	165	1268		
95	208	1560		
96	247	1888		
97	246	1903		
98 ^(a)				
99–11	0	0		
12	_105 ^(b)	-770		
13	-84	-598		
14	-145	-1100		
15	-295	-2258		
16	-452	-3453		
17	-164	-1320		
18	0	0		

(a) Reprocessing initiated.
(b) (-) indicates shipment from inventory to an offsite destination.

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	ł	₩	RHT	ſRU	CH	FRU
Year	<u>Rail</u>	Truck	Rail	Truck	Rail	Truck
90	24	117	23	99	13	26
91	47	234	44	201	25	50
92-00	70	350	65	301	38	75
01	94	463	87	398	50	99
02	117	582	108	503	63	123
03–05	140	700	129	603	67	131
06	187	932	173	800	101	196
07	234	1164	215	1006	125	246
08–10	196	980	170	787	9 8	195
11	243	1212	213	989	123	244
12	136	674	101	476	60	115
13	76	376	85	399	50	97
14	126	630	85	399	50	97
15	17	83				
16	26	122				

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TABLE 3.6. Annual Number of Incoming and Outgoing Shipments at the MRS/IS Facility (Delayed Disposal scenario)

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4.0 MRS/IS/REPOSITORY FACILITY

The various considerations related to the MRS/IS/Repository facility whose preconceptual design is developed in this report are presented in this section. These considerations include licensing aspects, safety and environmental concerns, functional criteria and facility requirements, site location and description, system descriptions, schedule and cost distributions, and life cycle costs. These considerations are divided into generic considerations and design-specific considerations and are discussed in succeeding subsections.

4.1 GENERIC CONSIDERATIONS

Subjects such as licensing, safety, environmental protection, general standards and criteria, and quality assurance are relatively independent of the details of the facility design, and are discussed generically in the following subsections.

4.1.1 Licensing

The various bills before Congress all require that the MRS/IS facility be licensed by the Nuclear Regulatory Commission under the appropriate parts of Title 10, Code of Federal Regulations (10 CFR). Principal among these is Part 72, which deals specifically with storage of spent nuclear reactor fuel and other radioactive materials in facilities independent of the reactor. Other parts of 10 CFR that are relevant to the design, construction, and operation of an MRS/IS facility include:

- 10 CFR 20 Standards for Protection Against Radiation
- 10 CFR 50 Appendix B (Quality Assurance) and Appendix E (Emergency Planning)
- 10 CFR 51 Licensing and Regulatory Policy and Procedures for Environmental Protection
- 10 CFR 60 Disposal of High-Level Radioactive Wastes in Geologic Repositories

- 10 CFR 71 Packaging of Radioactive Materials for Transport
- 10 CFR 73 Physical Protection of Plants and Materials
- 10 CFR 100 Appendix A, Seismic and Geologic Siting Criteria
- 10 CFR 170 Fees for Facilities and Materials Licenses and Other Regulatory Services.

Since the surface handling facilities developed for the MRS/IS facility co-located with a repository will be used by the repository when it is opened, it is expected that additional guidance in the form of Regulatory Guides related to Part 60 will become available in time to be of assistance in the development of the final design of the surface handling facilities.

Depending upon the location of the facility, there may be permits and/or licenses required by state and local agencies. All required licenses and permits will be identified and a schedule established to ensure the availability of necessary information and the timely submission of applications for the necessary licenses/permits.

4.1.2 Safety

This program will include measures necessary to assure compliance with applicable safety, fire, and health requirements. Operation of a MRS/IS facility involves the receiving, handling, and storage of radioactive solids in the form of spent fuel, solidified HLW, and packaged TRU wastes. Otherwise, the operations do not involve any significant use of toxic materials. Principal potential safety hazards at the facility are:

- release of radioactive materials
- criticality incidents
- radiation exposure
- fire
- operational hazards personnel exposure to excessive noise, dust from construction, etc.
- natural phenomena flooding, tornado, earthquake.

Systems and operational procedures will be used in the MRS/IS facility to protect facility personnel and the public from nuclear radiation and contamination and to provide industrial safety. Safety will be considered for three circumstances--normal operating conditions; abnormal operating conditions and conditions resulting from improbable events.

The principal concerns of the facility in regard to safety deal with the handling of the nuclear waste or spent fuel. Considerations for facility safety include layout, design, construction, and, in particular, proper design for nuclear materials handling, such as the use of work zones to limit personnel exposure to radiation, the use of an adequate facility security system, and the use of high safety factors and significant redundance for all systems that receive, handle, and store the nuclear waste.

Containment and filtering is provided to minimize the potential for release of radioactive materials. Criticality incidents and radiation exposure are prevented by careful attention to design concepts and configuration. Comprehensive fire detection and protection equipment are used throughout the entire facility. Potential noise excesses are controlled by equipment isolation, sound-absorbent material, and personnel protection where required. Dust during construction operations is controlled by water sprinkling. Personnel exposure to high temperatures is reduced by ventilation, air-conditioning and worker protection where required. All facilities are designed to withstand the effects of natural phenomena as appropriate for the safety classification of the individual facility.

4.1.2.1 Normal Facility Operation

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Containers of wastes are received, handled, stored and eventually retrieved on a routine basis. If additional storage space is being constructed simultaneously to the receipt of material, the two operations will be separate. Protection from radioactivity is provided by the integrity of the waste form, its container and cask, or by the isolation provided for in the waste handling building and in the storage modes.

During normal operations, insignificant quantities of airborne radioactivity could be released into the atmosphere. However, exposure of the public shall not be greater than that allowed by 10 CFR 20 and Appendix I to 10 CFR 50. Engineered confinement systems will prevent major release of radioactivity from the waste handling building or from the storage areas.

The waste handling facility will be treated as a "controlled area" in which building ventilation pressure(s) is maintained below ambient atmospheric or adjacent area pressure, thus assuring that possible leakage through the walls will be into, not outward from, any potential source of contamination. Additionally, all exhaust air from the building will be filtered through filter systems that include high-efficiency particulate air (HEPA) filters and then released through a stack. The stack provides for dispersal in the atmosphere of the small amount of radioactivity that may pass through the filters. The stack height is established according to atmospheric conditions at the site; dispersion provides enough dilution that radioactivity reaching ground level is at or below permissible concentrations.

Finally, the occurrence of release of radioactivity from either the waste handling facility or the storage areas depend upon simultaneous leakage from both the waste form and its failed containers, and consequently is expected only rarely.

4.1.2.2 Abnormal Operating Conditions

Anticipated occurrences that could result from equipment failures, operator errors, or unplanned process variations during the operating life of the facilities are considered in terms of possible effect of the failure, how detected, safeguards and recovery procedures. These considerations are incorporated into the design of the facility confinement systems.

4.1.2.3 Improbable Events

Although they have a very low probability of occurring, some upper limit accidents or improbable events justify the incorporation of additional design features to further reduce the probability of their occurrence or to mitigate

their effects. Improbable events considered include earthquakes, high winds and tornadoes, and floods. Risks due to these natural phenomena are assessed and adequate design provisions made to them, as follows:

- Seismic design of structures, systems and components considers the seismic events of Safety Function Earthquake (SFE), Operating Basis Earthquake (OBE) and Uniform Building Code Earthquake (UBC) and is in accordance with the earthquake level assignment and applicable NRC regulations.
- The Design Basis Wind (DBW) is the same as the Operating Basis Wind (OBW) for the Hanford Site. American National Standard Institute (ANSI) requirements will govern the design.
- There will be no design basis for flood (DBF) because of the elevation of the reference site above the Columbia River.
- An MRS/IS facility need not be protected from tornado missiles but shall be designed to prevent massive collapse of building structures or the dropping of heavy objects on the waste forms as a result of building structure failures.

4.1.3 Environmental Considerations

Construction, operation, and decommissioning of an MRS/IS facility by the federal government will require compliance with the National Environmental Policy Act (NEPA). These activities will almost certainly be viewed as major federal actions requiring the preparation of an environmental impact statement (EIS). Two EISs will probably be required, one covering construction and operation of the facility and the other covering decommissioning. The EISs will be prepared in accordance with the regulations of the Council on Environmental Quality (CEQ). In addition, since the facility is to be licensed by the U.S. Nuclear Regulatory Commission (NRC), a safety analysis report (SAR) will be prepared covering operation of the facility. Together, these documents will describe the facility and alternatives to the facility; the environmental impacts of constructing, operating, and decommissioning the facility; the measures taken to assure safety, and the measures taken to monitor safety. The proposed MRS/IS facilities are described in Subsection 4.3. The potential environmental impacts associated with these facilities that will require consideration in the EISs are discussed briefly in the following subsections.

4.1.3.1 Environmental Impacts During Construction

During construction of the MRS/IS facility, the environmental impacts will be similar to those of any major construction project, except that construction work force at any time is likely to be less than 200 or 300 people. Therefore, socioeconomic impacts and the impacts from the presence of extra temporary workers or from many people concentrated in a small geographic area will be small. Some of the environmental impacts from construction will be:

- removal of the land from production or other uses
- possible removal of timber from the land
- irreversible use of some construction materials
- irreversible use of fuels and electricity
- occasional minor traffic congestion
- dust from construction activities
- noise from construction activities
- minor socioeconomic impacts.

4.1.3.2 Environmental Impacts During Operation

Radioactive materials, including spent fuel, will be handled during operation of the MRS/IS facility. Appropriate measures will be taken at all times to avoid criticality and the possibility of any other accident, as well as to minimize occupational or public radiation dose from routine radioactive waste handling activities. Probably the most significant impact from operation of the facility will be the large number of shipments of radioactive material to and from the facility.

The impacts from operation will include:

- routine occupational radiation doses to workers at the facility
- substantial freight traffic to and from the facility hauling radioactive shipments

- routine public radiation doses due to transportation activities
- potential (small) for accidental offsite releases of radioactivity.

4.1.3.3 Environmental Impacts During Decommissioning

Only the storage areas will need to be decommissioned when the MRS/IS facility ceases operation because the waste handling facility will become part of the repository. Before decommissioning of the storage areas begins, all packaged radioactive wastes will be placed in the repository, leaving only incidental amounts of radioactivity to be removed. Significant quantities of construction materials (e.g., iron) could be reclaimed. The decommissioning work force will be small, so socioeconomic impacts will be small. Some of the impacts from decommissioning will be:

- routine occupational radiation doses from decommissioning activities
- routine public radiation doses from the transportation of radioactive wastes to low-level waste burial grounds
- some noise
- little socioeconomic impact
- traffic to and from land fills.

Because the storage facilities are expected to be essentially uncontaminated, or readily decontaminated at the time of decommissioning, only the last of the listed impacts is expected to be significant.

4.1.4 General Standards and Criteria

The design and construction of the MRS/IS facilities are governed by a vast variety of codes and standards. These are summarized briefly in this subsection with a comprehensive listing given in Appendix D.

The pertinent codes and standards are listed by title, starting with federal codes.

U.S. Government Codes, Standards, and Guides

- National Environmental Policy Act (NEPA)
- Occupational Safety and Health Administration (OSHA)

- Code of Federal Regulations, including NRC and DOT requirements and guides
- U.S. Department of Energy Manual Chapters

State of Washington Codes, Standards, and Guides

- Washington Administrative Code, including construction standards and safety standards for handling explosives
- Washington Highway Manual
- Washington Grid System

Industrial and Professional Society Publications

- American Conference of Governmental Industrial Hygienists
- American Concrete Institute
- American National Standards Institute
- American Nuclear Society
- American Society of Civil Engineers
- American Society of Heating Refrigeration and Air Conditioning Engineers
- American Society of Mechanical Engineers
- American Society for Testing and Materials
- American Water Works Association
- Factory Mutual Resource Corporation Manual
- Government-Industry Data Exchange program
- Institute of Electrical and Electronic Engineers
- Insulated Power Cable Engineers Association
- National Fire Code
- National Fire Protection Association
- Underwriter's Laboratories, Inc.
- Uniform Building Code

4.1.5 Quality Assurance

A quality assurance (QA) program based on the criteria of 10 CFR 50, Appendix B, will be established, implemented, and applied to the structures, systems and components of the MRS/IS facility that are important to safety. The QA program will extend throughout design, development, manufacturing, construction and operation. Primary focus will be on items essential to the integrity of confinement, to radiological safety, and to prevent criticality events. However, it will also encompass other items and activities at varying levels of assurance.

The QA program shall include:

- designation of organizational responsibilities
- preparation of QA plan, procedures, and instructions including quality levels
- program for training personnel
- implementation and documentation
- documented audit program.

The QA program shall cover the following activities:

- design and development
- procurement
- manufacturing, fabrication, and assembly
- construction and installation
- operation, maintenance, and modification.

4.1.5.1 Development of QA Program

A QA program to ensure the MRS/IS facility does not adversely affect the health and safety of the public will be developed in steps of increasing specificity. An overall QA program document, including general QA procedures and instructions for siting, design, construction, testing, and operation of structures, systems, and components of the facility, will be prepared. The overall program will outline the hierarchy of responsibilities and organizational interfaces, and the procedures for internal controls and auditing.

Major participating organizations will prepare and submit for review and approval separate detailed QA plans that meet the requirements set forth by the overall program document. Upon approval, these separate QA plans become part of the overall program. Detailed QA plans will also be required of all lower-tier contractors; these will also be subject to approval and will form part of the overall program upon their approval.

4.1.5.2 QA Classifications

Structures, systems, and components of the MRS/IS facility are to be classified into three levels as related to their importance to nuclear safety.

- <u>Quality Assurance Level I</u> Level I structures, systems, and components, or portions thereof, will be subjected to the requirements of a quality assurance program established in accordance with guidelines provided in 10 CFR 50, Appendix B. Structures, systems, and components will be considered important to nuclear safety and designated Level I if they are necessary to ensure
 - maintenance of the confinement system for the Level I building
 - prevention or mitigation of the consequences of accidents which would result in potential offsite exposures as large as
 10 percent of 10 CFR 100 limits
 - prevention of offsite doses arising from the failure of a system or component containing radioactive material that would result in doses at the site boundary >500 mR to the whole body or its equivalent to any part of the body.
- Quality Assurance Level II Structures, systems and components, or portions thereof, that are not Level I but are either essential to normal operation of the MRS/IS facility, essential to preventing a non-nuclear hazard to repository operating personnel, or are required for physical protection against radiological sabotage, will be classified as Level II. Level II structures, systems, and components are not essential for the nuclear safety of the MRS/IS

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facility and their failure could not result in an accident or accident consequences that would release hazardous materials to the offsite environs consisting of:

- radioactivity that would result in doses or concentrations of radioactive material in excess of the limits of 10 CFR 20, or
- hazardous or toxic materials in concentrations that would cause undue risk to the health and safety of the general public.
- Quality Assurance Level III Structures, systems, and components, or portions thereof, that are not Level I or Level II and the failure of which could not result in any release of radioactive, hazardous, or toxic materials to the environs, will be classified as Level III.

A component may be classified at a lower level than its parent system, provided that the consequences of its failure satisfy the criteria for the lower classification. No component will be classified at a higher level than its parent system. If no specific level is established for a component, it will be considered to be at the classification level of its parent system. This classification will consider safety analyses, programmatic loss potential, and industrial experience.

4.1.6 Functional Criteria and System Requirements

The MRS/IS system is intended to receive, store, and ship out spent reactor fuel, solidified HLW, and packaged TRU wastes during the time period before availability of a geologic repository and for a reasonable period of time thereafter. The general functional capabilities required of the MRS/IS facility are discussed in Subsection 4.1.6.1.

To be acceptable into the facility, the radioactive materials and the handling and storage system must satisfy a number of specifications. These charcteristics are discussed in Subsection 4.1.6.2.

4.1.6.1 Functional Criteria

The MRS/IS facility which is co-located with a repository will have the capability to receive, store and ship the volumes of spent fuel, solidified HLW, and packaged TRU wastes, as described in Appendix B, for the Reference scenario, the Delayed Reprocessing scenario, and the Delayed Disposal

scenario. The radioactive materials are assumed to be delivered to the MRS/IS site by both rail and highway transport, with the volume of materials evenly distributed between the two transport modes.

The facility will have the capability to unload the materials, inspect as appropriate, repackage when necessary, transfer to the storage locations, retrieve from the storage locations, and ship to another location (reprocessing plant, geologic repository). Process flow diagrams for spent fuel, HLW, RHTRU and CHTRU materials are shown in Figures 4.1, 4.2, 4.3 and 4.4, respectively.

Shielding at the facility will be sufficient to permit handling, inspection and storage of spent reactor fuel that has cooled at least 10 years, or solidified HLW and TRU wastes whose source fuel assemblies were discharged from reactors at least 10 years prior to receipt at the facility, while maintaining occupational radiation exposure within allowable limits.

The storage facilities at the facility will have the capability to transfer sufficient heat from the stored material to the environment to prevent overheating and possible damage to the stored material. The transfer of heat will be accomplished using passive techniques to avoid the need for active operating systems in the storage areas.

The ability to periodically sample the environment within the storage containers and the environment surrounding the storage containers will be provided to assure detection of any unexpected dispersion of the radioactive materials while in storage.

Accountability for all waste packages received by the facility will be maintained until the material is removed from the facility.

The facility will be designed to preclude accidental criticality.

The facility will be constructed in such as way as to facilitate its physical protection and to facilitate safeguarding the stored material.

The facility will have the capability to process and package for disposal radioactive wastes resulting from facility operation.

The facility will have the capability to provide surge storage for 20 waste packages.



FIGURE 4.1. Flow Diagram for Spent Fuel







FIGURE 4.3. Flow Diagram for Remote Handled TRU Waste

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FIGURE 4.4. Flow Diagram for Contact-Handled TRU Waste

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4.1.6.2 System Requirements

Requirements and characteristics of the radioactive materials that are acceptable for storage in the MRS/IS facility and the processing capabilities required at the facility are discussed in this subsection.

<u>Heat Emission</u>. The reference heat emission rates from spent fuel and solidified HLW are given in Table 4.1. It is anticipated most of the materials received by the facility will have lower heat emission rates than the reference case.

<u>Radiation Emission</u>. The gamma surface dose rates and neutron emission rates emanating from unshielded containers of reference waste material are given in Table 4.2.

<u>Physical Characteristics</u>. The dimensions and weights of waste packages anticipated to be processed at the MRS/IS facility are listed in Table 4.3.

<u>Receiving Capability</u>. The facility has the ability to receive and process or place in surge storage 1 rail car shipment and/or 5 truck shipments per day. Each rail shipment of spent fuel is assumed to consist of 7 PWR or 18 BWR assemblies. Each truck shipment is assumed to consist of 1 PWR or 2 BWR assemblies. HLW canisters are also received in cask shipments, 1 canister per truck cask, 5 canisters per rail cask. The TRU wastes in 55-gallon drums are received in the TRU-PACT container (72 drums, 6 boxes/rail; 36 drums, 3 boxes/truck).

TABLE 4.1. Reference Heat Emission Rates

Package	Watts, 10 Years After Discharge
PWR element (a)	550
BWR element ^(D)	175
HLW canister (c)	2300

(a) 462 kg initial U, 35,000 MWD/MTU exposure.

(b) 186 kg initial U, 25,000 MWD/MTU exposure.

(c) 2.14 MT initial U processed, 60 percent PWR, 40 percent BWR.

Package	Gamma Surface Dose Rate, R/hr	Neutron Emission
HLW canister ^(a)	1×10^{5}	5×10^8
Hulls canister ^(D)	1×10^{3}	5×10^{6}
Hardware canister ^(C)	3×10^4	

TABLE 4.2. Reference Gamma Dose Rate and Neutron Emission Rates

- (a) 2.14 MT initial U processed, 60 percent PWR, 40 percent BWR, 10 years from discharge.
- (b) Hulls from processing 4.4 MT initial U, 0.5 percent loss, 5 years from discharge.
- (c) Hardware from processing 10.7 MT initial U. Dose rate is proportional to calculated cobalt in hardware five years after discharge.

TABLE 4.3. Reference Physical Characteristics of Wastes

Waste Type	Nominal Dimensions, ft	Nominal <u>Weight, lb</u>
PWR fuel	16.7 x 0.71 x 0.71	1,500
BWR fuel	15 x 0.46 x 0.46	6 00
HLW glass canister	1 O.D. x 10	1,700
Compacted hull canister	2 O.D. x 10	1,700
Fuel hardware canister	2 O.D. x 10	1,700
Remote-handled TRU canister	2 O.D. x 10	1,700(a)
Remote-handled TRU container	55-gal drum	900(a)
Contact-handled TRU container	55-gal drum	900(a)
Contact-handled TRU container	4 x 6 x 6 box	14,000(a)

(a) TRU wastes mixed with concrete for stabilization within the container.

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<u>Processing Capability</u>. The facility has the ability to repackage for storage as required and to store spent fuel assemblies at a maximum rate of 1500 assemblies per year (750 PWR, 750 BWR) or HLW at a maximum rate of 700 canisters per year (equivalent to ~1500 metric tons of spent fuel), RHTRU at a rate of ~550 canisters and ~700 55-gallon drums per year, and CHTRU at a rate of ~3300 55-gallon drums and twenty-five 4- x 4- x 6-foot boxes per year. These rates are equivalent to throughputs for the hot cell/transfer/repackaging station of about 6 spent fuel assemblies (3 PWR, 3 BWR), 3 HLW canisters, 2 RHTRU canisters and 3 RHTRU drums per day. The facility is assumed to operate on the following schedule:

Receiving - 300 days/yr, three 8 hr shifts/day, 7 days/wk Packaging/transfer - 250 days/yr, three 8 hr shifts/day, 5 days/wk.

4.2 SITE LOCATION AND DESCRIPTION

The assumed location for this MRS/IS facility co-located with a geologic repository is within the boundaries of the Hanford Site. Hanford occupies $\sim 570 \text{ mi}^2$ (1500 km²) in the semiarid region of Southeastern Washington (see Figure 4.5).

4.2.1 Site Location and Arrangement

A hypothetical site for the MRS/IS facility is postulated to be located west of the 200 West area within the Hanford Site above the Cold Creek Syncline. The facility site arrangement, shown in Figures 4.6 and 4.7, is compatible with the constraints of the hypothetical site and should also satisfy the requirement of the follow-on repository and its operation. Approximately 250 acres will be required for the initial facility. To cover the interim storage requirements for the various scenarios, up to 400 total acres may be required. In comparison, about 550 acres are projected to be required at the surface to supply and to support an underground respository that may cover or have a surface projection of up to 2000 acres.

The initial area will be developed by the required site preparation, roads, fences, walkways, and rail systems with due consideration and provisions for the additional areas and facilities that may be required later.



FIGURE 4.5. Location Map - Hanford Site

FACILITY INDEX

B to be described as

FACILITY INDEX 1. WASTE HANDLING FACITY 3. GATE HOUSE #1 4. RAL CAR REPECTION FACITY 3. GATE HOUSE #2 4. RAL CAR REPECTION FACITY 5. GATE HOUSE #2 6. PATROL REPOOLATIONS 7. ADMENTIATION RLOG 8. MANFLOWE FACITY 9. ELECTRICAL SUBSTATION 10. STANDOV GORERATOR 11. WASTENDINGE TAXIN 2. POLY HOUSE 13. WARFHOUSE 14. TRANSMIRKIC SUBFACE STORAGE FACILITY 15. CASH STORAGE YAND 16. WATCH TREATENT FANT 17. SEWING LEADY FELO 10. SUBFACE TAXING 20. SAL CAR WARFHOUSE 21. PANONE LOOP 22. EGOLATION TOME 23. PATROL ROAD



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FIGURE 4.6. MRS/IS Facility Site Arrangement

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MRS/15 FACILITIES





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4.2.2 Site Parameters

Conditions of this hypothetical site are assumed to be in accordance with typical conditions found at Hanford. These assumed conditions, which include climatology, ecology, hydrology, environment, terrain and geologic formations, and flood plain management, are discussed in subsequent subsections.

Real-time wind speed, direction, and stability data are available from the Hanford Meteorological Station, which has been in continuous operation since the middle 1940s.

4.2.2.1 Climatology

The Hanford climate is generally mild and dry with occasional periods of high winds. Summers are generally hot and dry with relatively mild winters, considering the latitude. For the months of January and July, the average maximum temperatures are $36.7^{\circ}F$ ($2.6^{\circ}C$) and $91.8^{\circ}F$ ($33.2^{\circ}C$), respectively, and average minimum temperatures are $22.1^{\circ}F$ ($-5.5^{\circ}C$) and $61.0^{\circ}F$ ($16.1^{\circ}C$), respectively. Average annual precipitation is 6.25 inches (15.9 cm) with 42 percent occuring November through January. Average monthly wind speeds fluctuate from 5 mph (2.3 m/s) during winter months to 9 mph (4.1 m/s) during summer months, with the prevailing wind direction from the northwest, although the strongest winds are from the southwest.

Tornadoes are infrequent in the region; they tend to be small and cause little damage when they do occur. A single, small tornado has been observed onsite, but no damage was reported. Fourteen tornadoes have been confirmed within 100 miles (160 km) of the Hanford Site between 1916 and the present. Data have been analyzed to determine the probability of a tornado hitting a particular Hanford facility. During any year, it is estimated that the probability is six chances in a million or less than once in 100,000 years.

The number of thunderstorm days at Hanford gives an estimated annual lightening-strike frequency of 0.022 for a building 30 feet (9 m) high. This frequency corresponds to about one strike per 45 years.

4.2.2.2 Hydrology

The hydrology of the Hanford Site consists of both surface and subsurface flow systems. The Columbia and Yakima Rivers form the principal surface water drainage of the area. On an average, these rivers discharge 100,000 and $10,000 \text{ ft}^3/\text{sec}$ (2,830 and 283 m³/sec), respectively. Two ephemeral streams occur along the extreme western boundary of the Hanford Site, but their water discharges are very low, even during the rainy season. Various ditches and ponds in and near the 200 Areas contain cooling and process waters, which either evaporate or recharge the underlying unconfined aquifer.

The groundwater flow systems consist of unconfined and numerous confined aquifers. Hydrologic knowledge of aquifer properties is quite extensive for the unconfined system; however, it is less complete for the confined systems, particularly those small systems within the deeper basalts. An extensive field testing program is under way to acquire a solid understanding of all confined aquifers that may be important in designing and siting an underground repository.

Groundwater beneath the Hanford Site occurs in either an unconfined aquifer or in one of several deeper confined aquifers. The unconfined aquifer consists of both galciofluvial sand and gravel deposit and the Ringold silts and gravels. The Yakima River recharges the unconfined aquifer. The unconfined aquifer overlies a series of confined aquifers, including portions of the lower Ringold Formation and interbeds of the Columbia River Basalt Group.

4.2.2.3 Ecology

The Hanford Site is described as a "shrub-steppe" zone characterized by low precipitation and wide daily and annual temperature ranges.

The vegetation consists primarily of eight major kinds of shrub-steppe communities identified by the most conspicuous or abundant plant species:

- sagebrush/bluebunch wheatgrass
- sagebrush/cheatgrass or sagebrush/Sandberg bluegrass
- sagebrush-bitterbrush/cheatgrass
- greasewood/cheatgrass/saltgrass
- winterfat/Sandberg bluegrass
- Thyme buckwheat/Sandberg bluegrass
- cheatgrass-tumble mustard
- willow.

The sagebrush/bluebunch wheatgrass and sagebrush-bitterbrush/cheatgrass vegetation types cover extensive acreage. Bluebunch is the most important livestock forage. Cheatgrass provides forage for mule deer, especially in the fall and winter.

Scarcity of grass allows the invasion of tumbleweed, especially in burn-over areas. Both cheatgrass and tumbleweed are well adapted to invading disturbed habitats. They will become more prevalent on the Hanford Site as soil is disturbed by construction.

4.2.2.4 Environment

The MRS/IS facility site is to be incorporated into an environment already slightly altered from its original state due to 1) livestock grazing and 2) the activities associated with Hanford projects since the early 1940s. Land within a 50-mile (80 km) radius is used primarily for grazing, growing wheat, and irrigated farm crops. The nearest military facility is the U.S. Army Yakima Firing Range located ~30 miles (48 km) to the northwest. There are no recreational facilities within a 5-mile radius of the proposed site. The closest public highways are State Highways 12, 240 and 24.

4.2.2.5 Terrain and Geology

The Hanford Site lies on the low-lying, partly dissected, and modified alluvial plain of the Columbia River within the central part of the Pasco Basin. Most of the Hanford site is underlain by generally coarse-grained sediments deposited by several glacial floods. Sediments at or near the ground surface range from coarse boulder and cobble gravel in the extreme northern reaches, to sandy cobble and granular gravels in the central part of the site, to coarse sands in the southern part. The entire site is blanketed by a veneer of wind-blown (eolian) sediments that range from very fine sands and silts to coarse sand.

The MRS/IS facility site is underlain by 1000 feet (300 m) of sands, silts, and clays laying on a basalt lava accumulation estimated to be 10,000 feet (3000 m) thick. The soil type which makes up the site consists of Rupert Sand, which is mostly composed of granitic, quartzitic, and basaltic sand. The Hanford Site lies in a region characterized by few earthquakes of damaging intensity, with no clear-cut relationships of epicenters to specific surface faulting or specific geologic structures. To date, no intensities greater than four on the Modified Mercalli Scale (MM-IV) with a gravitational ground acceleration of 0.01 g have occurred in the immediate Hanford Site area, although intensities as high as MM-V or MM-VI have been observed in surrounding areas.

4.2.2.6 Floodplain Management

Because of recurring damages due to flooding, proper floodplain management has become an item of national concern. The proposed facility site is not located in a floodplain as defined by 10 CFR 122. By definition, a floodplain is any low land or relatively flat area adjoining inland or coastal waters, that are flood-prone and subject to a 1 percent or greater chance of flooding in any given year (the 100-year flood). The estimated 100-year maximum Columbia River flood of 444,000 cfs would result in a river elevation of 356 ±2 feet mean sea level (MSL) based on U.S. Corps of Engineers projections.

The probable maximum flood (PMF), as evaluated by the U.S. Corps of Engineers, would result in a Columbia River elevation of 382 ± 4 feet with an occurrence rate of once every several thousand years. The hypothetical site for the MRS/IS facility is at an elevation of ~600 feet MSL; therefore, it is concluded that the site would not be subject to inundation by any flood having a volume equal to or less than the PMF.

4.3 SYSTEM DESCRIPTIONS

The MRS/IS facility consists of the major systems or components described in the following subsections. Security, accountability, monitoring, surveillance, and control functions are provided in the appropriate areas within the facility.
4.3.1 Waste Handling Facility

The waste handling facility (WHF), illustrated in Figure 4.8, is to receive, examine, and prepare for storage both remotely-handled and contact-handled waste. It provides space and systems so the process functions can be accomplished effectively and safely as well as providing the necessary support activities and functions. Its requirements are basically independent of the storage concept used (i.e., surface casks or below-grade drywells). However, requirements and/or size or capacity will vary with the various fuel cycle and transportation scenarios. Also if the drywell storage concept is adopted, additional provisions and capabilities will be required to overpack all fuel element bundles on a production basis in the WHF. The building is the sealed-confinement type with ventilation systems adequate to prevent exposure of the public to radiation doses in excess of allowable limits.

The core of the WHF (Figures 4.9, 4.10 and 4.11) is designed for the handling and transfer of waste packages that require remote handling. This is done in a series of hot cells located on an upper level and flanked by operating and service galleries. On the ground floor, beneath this group, the shipping cask unloading area provides a space in which the incoming cask is upended and connected to the shielding sleeve from the primary hot cell, thus providing a confined route for transfer of fuel, canisters or drums from the cask to the primary hot cell. Below the secondary cell is another transfer corridor for loading the casks to be transferred to interim storage.

The second waste handling area in the facility is for waste packages that can be contact handled. After preliminary inspection and washdown, the drums or containers are removed from the carriers, inspected for damage, radiation and surface contamination, decontaminated or modified if necessary, and placed on pallets as appropriate for transfer to storage.

The building support areas include radwaste treatment facilities, ventilation and filter rooms, mechanical and electrical rooms, service areas, and administrative areas.





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Two separate ventilating systems are furnished in the building: the confinement system for the waste handling areas, and a standard ventilating system for support and administrative areas. The confinement system supplies fresh air to the negative pressure zones of the waste handling areas and exhausts it through a filter system (which includes HEPA filters) and to the stack.

4.3.1.1 Cask Receiving and Shipping

This area of the facility can accommodate at least two rail cars or trucks at any given time. Shipping casks transported either by rail or by truck are inspected, cooled, protected and, as required, they and their contents are transported to the transfer or packaging portion of the facility. This portion of the facility consists of two basic areas: 1) cask carrier preparation and 2) cask and material transfers or unloading. The preparation activities are located in enclosed spaces that also serve as air locks for truck and rail car entry into the transfer area. Basically this portion of the facility has the following process functions (Figure 4.12):



FIGURE 4.12. Cask Receiving and Handling

- receiving and shipping receives loaded casks and returns empty casks
- cask surge or holding for the temporary storage of cask(s) and carrier(s)
- cask maintenance for minor repair and maintenance of cask(s) and carrier(s)
- preparation peripheral equipment is removed from the cask and/or carrier and stored
- cask loading and offloading casks can be removed from or loaded on a carrier
- cooling and washdown casks can be given exterior washdown or interior venting, flushing and cooling
- 7. decontamination casks can be decontaminated as required
- material unloading casks can be isolated or mated with the transfer/packaging portion of the facility

4.3.1.2 Container Transfer and Packaging

If the cask is shipped in a horizontal position it will be raised to vertical position on the transporter or set in a vertical position on a special car. Then it will be moved beneath the primary hot cell and mated with a shielded collar lowered from the cell. After removal of the shielding plugs from the hot cell and the cask, each canister or fuel bundle is raised up into the hot cell. There it is checked as necessary, and it can be stored temporarily in a lag storage location or it can be placed in one of the process tank areas or cells. These areas have the capability of enclosing fuel bundles or canisters in an overpack; inspecting spent fuel or completed waste packages (both helium-leak and ultrasonically tested for structural soundness), and decontaminating if necessary. Clean canisters and packages are transferred from the primary process cells to the secondary (and clean) hot cell. From there the completed waste package is lowered through shielding collars into a storage cask, which can be sealed and made ready for transfer to the storage area. The transfer and packaging area of the facility is to be designed to:

- use dry handling of the waste throughout the system
- minimize the number of handling operations in the interest of safety and economy
- receive remotely handled spent fuel bundles, HLW canisters and RHTRU packages
- inspect external surfaces of canisters and waste packages for physical damage and contamination
- overpack canisters and fuel (if leaking or damaged or if required for the storage concept) to form acceptable waste packages and inspect the packages following overpacking
- repair canister and waste package closure welds when necessary
- decontaminate canisters and waste packages when necessary
- retain traceability of all waste packages.

Remotely operated cranes, manipulators or devices are used to perform the following functions in the transfer and packaging hot cells:

- remove and replace shielding plugs for cell ports
- unlock/lock and remove/replace cask shield plugs
- extract material packages from shipping cask, move them to and through the hot cells, place them in transfer or storage casks; also the reverse of the above sequence
- mechanically interlock the grapple jaws with the payload while the payload is suspended from the crane.

4.3.1.3 Contact Material Handling System

Another portion of the WHF comprises two bays equipped to receive and handle either truck or rail cars, and a system to receive and remove waste containers from the TRU-PACT or similar shipping system; and to process and prepare the drums and boxes for storage.

After inspection, the entering vehicle is moved to the washdown area for removal of road dirt. Then it goes to the CHTRU waste receiving bay. There a crane offloads the carrier to an air pallet transfer machine which moves the carrier through an air lock into a processing area. In the processing area the drums or boxes are removed from their container by a lift truck and are subsequently inspected for surface contamination and radiation level. Drums that show evidence of damage are overpacked into larger drums or containers and are handled separately. Containers having excessive surface contamination are decontaminated by manual methods. Acceptable containers are placed on pallets and made ready for transfer to the transuranic surface storage (TRUSS) facility.

4.3.2 Transfer and Storage of Contact-Handled Wastes - TRUSS Facility

The TRUSS facility, shown in Figure 4.13, is an above-ground, warehousetype building designed to optimize CHTRU drum and steel box storage life cycle costs within safety, security, and storage environment requirements. The facility will provide indoor container storage in clean, dry conditions. State-of-the-art handling and storage methods will permit efficient operation with forklifts and a minimum of operating personnel. Containers on pallets can be transported to the TRUSS facility by forklift, truck or rail. The necessary segregation of TRU waste types can be accomplished within the facility by zoning with interior walls and aisles, or by covering arrays of similar containers with fire retardant protective covers. The internal floor space measures 280 x 200 feet (56,000 ft^2) of which ~35,000 ft^2 will accommodate a 10-year waste stream volume of 55-gal drums, based on the anticipated waste stream estimates given in Table 4.4. Access aisles will require a total of ~9000 ft² of floor space. leaving 7000 ft² for storing TRU boxes. The facility is sized to accommodate primarily the drummed CHTRU waste generated between the start-up of the MRS/IS facility and start-up of the co-located repository, a period anticipated to be ~10 years. After repository start-up, it is expected that the drummed TRU waste stream will be diverted directly to the repository, and not require interim storage. At the same time, the inventory of waste stored in the TRUSS facility will be sequentially retrieved and transported to the repository.



	MTHM	Containers	Casks Required	Comments
Fue1	530		54	REA-2023 cask, 24 PWR or 52 BWR fuel assemblies per cask
HLW-1 ft x 10 ft	11,000	4,900	350	REA-2023 cask, 14 canisters per cask
RHTRU-2 ft x 10 ft		3,845	1,282	Concrete cask, average 3 containers per cask
RHTRU-55 gal		4,486	408	Concrete cask, 12 drums per cask
CHRTU-55 gal ^(a) CHTRU-4 ft x 6 ft x 6 ft ^(b)		34,076 286		

TABLE 4.4. MRS Reference Scenario Storage Requirements

(a) Stacked four high, \sim 35,000 ft² required. (b) Stacked two high, \sim 3,500 ft² required.

4.3.2.1 Structure

A precast concrete building is used for the TRUSS facility to meet requirements of containment and protection. The basic function of the building is to shelter waste-storage containers; however, it should also confine and reduce the spread of radioactive material in the event of a container failure inside the facility. A fairly light building with an inward-directed air flow will provide reasonable assurance of meeting this objective. This type structure will also provide ample protection from plausible natural events. Floor and loading bay areas are designed to accommodate the handling equipment and containers.

4.3.2.2 Material Handling and Storage

The TRUSS facility will receive and store TRU waste packages for ultimate shipment to a federal repository for disposal. These packages will range from 55-gallon drums and similar containers to 4- x 4- x 6-foot rectangular steel

boxes. Packages will be certified to meet contact-handled waste acceptance criteria for permanent disposal, and will be stored in designated areas in the facility.

Deliveries to the TRUSS facility will normally be made by truck from the WHF and will be received in an enclosed loading bay which will fully contain the delivery trucks or trailers. The 20 ft x 40 ft bay will have roll-up doors leading into the facility and to the outside. During waste deliveries the outer door can be closed to provide weather protection and containment. The loading dock in these bays will match the height of truck or trailer beds to permit forklift unloading and storage operations. Fifty-five-gallon drums will be handled by forklifts equipped with drum handling tongs, and stacked in rectangular modules in designated areas in the building. Drums may be stacked no more than 5 layers high, but the storage arrays may be any convenient length or width. The maximum weight of a drum is ~900 pounds. Forklifts configured with regular times will handle TRU boxes and preassembled 6- or 12-packs of 55-gallon drums. Such packages may have a maximum size of up to 12 x 8 x 8.5 ft and may weigh up to 25,000 pounds. This will require that at least one forklift in the facility have a capacity in excess of 25,000 pounds.

There will be a load-out area on the rear of the facility for loading certified waste packages into TRU-PACTs on trailer beds or rail cars for transfer to the repository. This dock will be completely enclosed to permit forklifts to drive from the interior of the facility onto a trailer or a railcar and load waste packages. The bay will measure ~75 x 25 feet, and will contain one trailer or rail car at a time. It will have doors on both ends to permit forward movement of trailers or rail cars after loading, thus allowing the next carrier to follow directly behind.

4.3.2.3 <u>Retrieval</u>

Drums and boxes from the TRUSS facility will be retrieved with forklifts. There is no preliminary work required to make the containers accessible. They can be moved out of the facility and onto trucks at the loading bays, which is essentially the reverse of the delivery and emplacement

operations. The favorable storage environment will insure that containers will be in good condition at retrieval and not require repackaging, an extra operational step that would add to the cost of TRU retrieval. In short, the TRUSS facility can provide inexpensive TRU retrieval because of:

- immediate access to the waste containers
- avoidance of the need to repackage or contain the original waste containers
- small retrieval crew, using efficient eqipment and techniques.

4.3.2.4 Storage Environment

The TRUSS facility provides a favorable storage environment. The walls and roof will be precast concrete panels with insulation sandwiched inside. Insulation R values of about 11 to 13 for the walls and 19 for the roof will be used. Artificial temperature control requirements are minimized by the inherent thermal stability provided by the structure and concrete slab floor, and by the wide storage temperature range allowed for the waste. The ventilation exhaust system will also help lower the temperature if required for personnel access. No firmly established low temperature limit will be set but the temperature will be high enough to avoid formation of frost on the storage containers. This will be accomplished in the TRUSS facility by using the interior lights to heat the storage space as necessary.

The relative humidity inside the TRUSS facility will be below critical levels for the vast majority of the storage periods, even without mechanical dehumidification equiment or heating. Studies show that the mean ambient relative humidity at Hanford is at, or below, 55 percent for 7 months of the year, and ranges between 60 and 80 percent for the other 5 months. By maintaining the internal TRUSS storage temperature 10° F above the outside temperature in the winter time, the resulting relative humidity will not exceed 55 percent.

4.3.2.5 Criticality Prevention

Storage of fissile material in the TRUSS facility will be done in arrays that make efficient use of the facility and will not permit criticality to

take place. Because of the quantity and form of fissile material that will be placed in the facility and its form and arrangement, the facility will be classified as a Limited Control Facility. As such, criticality monitors are not mandatory, but may be incorporated along with other fissile facility requirements as deemed prudent.

4.3.2.6 Radiation Monitoring

Radiation monitoring and alarm systems will be provided in the TRUSS building, in the ventilation stack, and exterior to the building, to detect any inadvertant releases.

4.3.2.7 Lighting

Skylights may be installed to augment the installed energy-efficient fluorescent lighting. The number and location of skylights will be determined during conceptual design. The skylights will minimize the electrical power requirements during normal working hours only. During non-normal hours or inclement weather the fluorescent lighting must be able to provide 100 percent of the lighting needed, plus heating requirements.

4.3.2.8 Fire Detection and Suppression

Fire alarm control boxes will be provided near the loading bay areas to permit manual activation by operating personnel. The general storage area inside the facility will be equipped with a smoke detection system and an automatic sprinkler system, both of which will signal the fire department upon activation.

A dry-pipe, water sprinkler system will provide fire suppression capability throughout the facility. A dry-pipe system is required because the facility is unheated. A fire main will be required to bring the fire fighting and sprinkler system water to the facility. If the sprinklers are activated the drain system will collect the runoff water and route it to a holding tank. Hand-held fire extinguishers should be provided in accessible areas, but consideration should be given to selecting these locations to permit routine monthly inspection and maintenance when the facility is locked.

4.3.2.9 Ventilation

The facility will be equipped with a ventilation exhaust system to provide negative pressure ventilation within the building. The system will be sized to ensure that the normal air flow through the facility doors and openings is directed toward the inside. It will have a single exhaust stack, equipped with a motor-driven damper interlocked with the exhaust fans. The stack will have an isokinetic sample probe leading to a record and alarm monitoring system. The monitoring system will automatically shut down the ventilation system if air particulate levels reach preset limits. Alarms for the stack monitoring system will be displayed locally on an annunciator panel outside of the facility, and remotely in the WHF.

Because of the inherent thermal stability of this type of structure, ventilating with outside air will be sufficient to provide an acceptable working environment inside the facility during the summer. Material handling will not be a full-time operation, the main function being storage. Cooling for personnel comfort will be limited to keeping the peak globe temperature (WBGT) below 89°F, which can easily be accomplished without air conditioning. Sufficient heat will be generated from the lighting to provide a moderate temperature during the winter to prevent freezing.

4.3.3 Transfer and Storage of Remote-Handled Wastes - Casks

The interim storage provisions for the material received at the MRS/IS facility encompass an enclosed building (TRUSS) and either below-ground drywells or casks located on the surface. This section describes the cask storage concepts.

Two different types of storage casks are used. The REA-2023 cask, shown in Figure 4.14, is the reference cask for fuel and HLW storage, and has been designed, but not yet built. The unit consists of a double containment design with a welded final closure. The various components include a rugged, smooth stainless steel outer skin, a lead gamma shield, a water neutron shield and a basket featuring boral neutron-absorbing plates. The primary containment vessel is also stainless steel, designed according to ASME Boiler and Pressure Vessel Codes. This cask is compatible with loading and unloading procedures





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FIGURE 4.14. The Reference Passive Cooling Dry Storage Cask

which are common to utilities. Handling is accomplished by a redundant lifting yoke and two sets of lifting trunnions. An additional set of pivoting trunnions is also used. The cask can be handled and stored in either a horizontal or vertical attitude. Design permits continuous monitoring of both primary and secondary containment as discussed in Section 4.3.3.4. Cask design data are shown in Table 4.5. This cask is 8 feet in diameter by 16 feet long and weighs about 100 tons.

For storage of RHTRU, reference concrete casks, as shown in Figure 4.15, are used. The concrete casks are up to 9 feet in diameter by 16 feet long and weigh up to 90 tons. Different bore sizes and shielding thicknesses are used to accommodate different cask payloads, which vary from 1- to 2-foot diameter by 10-foot long RHTRU canisters to twelve 55-gallon drums.

The same handling, unloading and storage system is used for all casks. This system uses above-ground storage on reinforced concrete pads. A typical storage yard is 200 feet by 1850 feet and can accommodate about 1000 casks on a nominal 20-foot spacing. A tractor-trailer with pneumatic tires is used to haul the casks from the WHF to the storage yard. A gantry crane or a truck-mounted crane are located in the storage yard for unloading the casks from the trailer onto the storage pad.

Typical radiation levels of the material to be stored are shown in Table 4.6.

TABLE 4.5. Reference Metal Storage Cask Design Data

Designer/manufacturer	REA						
Mode1	REA-2023						
Capacity - PWR assemblies	24						
- BWR assemblies	52						
Weight, loaded, tons	87.5 - 97.5						
Size	8 ft OD x up to 16 ft						
Age of fuel, years	5						
Thermal load, kW	30(a)						

(a) Can be increased to 47 kW by addition of special fins.



	R/hr							
	0.2-5	5-50	50-500	500- 1,000	1,000- 50,000	50,000- 100,000		
Fuel Assemblies					A11			
HLW Canisters						A11		
Hulls, compacted				A11				
Hardware					A11			
RHTRU 1-ft dia x 10-ft can	58%	10%	6%	26%				
RHTRU 55-gallon drums	88%	11A%	1%					

TABLE 4.6. Typical Surface Radiation Levels of Remote-Handled Material

4.3.3.1 Surface Cask Storage

After a cask storage unit is filled in the WHF, it is loaded onto a pneumatic-tired transport trailer and towed into the cask storage area by a wheel tractor. The storage area is served by a mobile yard gantry crane, which spans two rows of storage units with an aisle between the rows for transport trailer access. This allows the gantry crane to unload a storage unit on either side of the transport trailer, as shown in Figure 4.16. In the storage area, the transport trailer meets the yard gantry crane at the placement site, where the gantry crane attaches to the storage unit by means of a cab-controlled power-operated load grab, lifts the cask unit clear of the trailer bed and places the unit in final position on its preconstructed concrete foundation pad. While performing the unloading operation, the gantry crane stands on power-operated stabilizing jacks and operates as a fixed gantry. The storage unit is handled intact and is lifted no more than 4 feet above the ground to minimize the potential for cask damage in the event of a dropped load.

The empty transport trailer is returned by tractor to the WHF for reloading. Since the trailer is of the four-wheel trailer type, it can be separated from the tractor, parked, and retrieved later or taken directly through the system, whichever pattern of operating practice is most advantageous.

The overall average transport travel speed is 4 to 5 mph. Slower speeds will be used when traveling between storage units in the storage area and



higher speeds can be used when traveling empty on main roads. The normal time required for a complete round trip of a transport tractor-trailer for delivery, including placement of a storage unit into the storage area by the crane, is estimated to be 2 hours or less, based on the longest distance to be traveled in the ultimate facility. For early years, a round trip time of 1 hour or less can be expected.

The yard gantry crane is sufficiently mobile, traveling on pneumatic tires at about 2 mph average, to serve the storage area and also to assist in the unloading of inbound shipments.

The transport and yard gantry crane system can retrieve any storage unit from any position in the storage area by reversing the procedure of the normal delivery. The storage area aisles provide unlimited access to any single storage unit, and retrieval cycle time will be comparable to the delivery-placement cycle time. To protect the storage unit against upset due to credible seismic or wind forces during transport and placement, the trailer is designed for stability, and both trailer and gantry crane are provided with antidrop skids to limit trailer or gantry drop in case of tire failure. Because the surface radiation levels on the casks may be as high as 20 mr/hr, some local or limited shielding may be required to allow safe approach by personnel and equipment for recovery from equipment malfunction or failure during the placement operations.

4.3.3.2 System Arrangement

For the waste casks, the storage area is subdivided into lots of ~1000 storage units. The array spacing within each lot, to provide 400 ft² for each storage unit in conformance with design limitations for handling operations is as follows (center-to-center of storage units):

- parallel to travel of transport trailer and yard gantry crane spacing alternately 21 ft to 27 ft.
 - transverse to travel of transport trailer and yard gantry crane spacing nominally 16 ft 8 in.

This spacing provides alternating wide aisles, 15 feet minimum width, for transport tractor-trailer movement and narrow aisles, 9 feet minimum width, for yard gantry crane movement. These widths will also serve possible future larger storage units with storage unit foundation pads 12 feet in diameter. The aisle widths provide for free movement of maintenance and surveillance vehicles and personnel. The gantry crane, trailer and cask arrangement during unloading are shown in Figure 4.17.

The above arrangement and spacing are based on the reference 8 to 9 foot diameter casks, but they can be modified to accommodate casks with different sizes (within reasonable limits). Different cask sizes would only change the internal array arrangement and not the land usage of the storage system.

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Between storage area lots, aisles of 90-foot width are provided to facilitate large-radius turning of the transport tractor-trailer and straight alignment of the transport trailer with the aisles in the lots. The wide aisle also provides ample space for turning and travel of the yard gantry crane. This arrangement provides for drive-through operation of the transport tractor-trailer, avoiding complex maneuvers or backing. The storage area layout in relation to the WHF is shown in Figures 4.6 and 4.7.

The initial storage area fence will enclose an area capable of storing waste through the year 1995. The initial construction will consist of about 50 foundation pads, which is the number required for the first 5 years of facility operation for the Reference scenario.

4.3.3.3 Component Description

Foundation pads for support of the waste storage units are poured in place. The pads are octagonal, circular or three smaller square reinforced concrete slab on grade, approximately 18 inches thick. After construction of the initial 50 pads, they will be built in quantities dictated by the placement schedule.

The area between storage pads, and the lightly traveled portions of the wide aisles between lots, are treated with defoliant, graded, and surfaced with 8 inches of crushed rock. This surface is considered adequate for travel by the transport equipment and yard gantry crane equipped with wide base earthmover-type pneumatic tires, and for use by surveillance and maintenance vehicles. The main roadway portions of aisles, where repeated and heavy traffic is expected, and feeder and collector roadways traveled by the transport equipment are 10 inches of compacted aggregate over a prepared and compacted subgrade.

The transport trailer is a 110-ton capacity, low bed, four-wheel trailer, running on wide base earthmover-type pneumatic tires. Skid rails are provided along each side, ~6 inches clear of the ground, to support the trailer in case of flat tires. Shielding is built into the trailer bed frame to supplement the limited shielding in the bottom of the storage casks. Initial equipment complement is one trailer. The tractor for the transport trailer is a four wheel, pneumatic-tired, diesel-engined unit tractor which has electric power and lighting to support night operation in the storage area. Initial equipment complement is one tractor.

The mobile yard gantry crane is a self-contained, self-propelled, straddle-type lifting system, with rated lifting capacity of 110 tons when stationary on stabilizing jacks.

The gantry main structure comprises two portal frames, each with under-running hoist trolley and hoist. Normal load pickup is by means of power-operated cab-controlled load grab. The load grab is carried by a longitudinal spreader which has a hoist load block built into each end and which incorporates a power-operated load-shift device to provide ~2 feet longitudinal load movement for spotting loads when the gantry is standing on the stabilizing jacks. Operator's cab and engine power unit are mounted on the side frame between the wheels. The four wheels have single wide-base, earthmover-type pneumatic tires. Other features include power-operated stabilizing jacks; skid rails to limit drop to 6 inches in case of flat tires; electric power and lighting to support night operation in the waste storage area. Initial equipment complement is one mobile yard gantry crane.

4.3.3.4 Cask Monitoring System

A monitoring and surveillance program will be implemented and maintained throughout the life of the storage area. The REA cask, described earlier, consists of a double containment design with a welded final enclosure. REA cask design permits continuous monitoring of both primary and secondary containment. Utilization of a pressure sensor permits continuous signal transmission and automatic sensing and recording by a multipoint interrogation system for the secondary containment system. Each cask will be sampled on an established basis for pressure and airborne activity through a sample valve. In order to detect any abnormal thermal conditions, the temperature of the exterior of the casks will also be monitored on an established basis.

Monitoring and service trucks with portable thermocouple and pressure readout and recording instrumentation, pressure gauge and gas sampling manifolds, and sample bottles will be used to periodically measure the environment within each cask. Cask air samples will be withdrawn into an evacuated sample bottle and analyzed in the WHF laboratory for evidence of leakage from the stored fuel or HLW packages.

Measurement of the cask exterior surface temperature will provide an indirect measurement of the fuel element temperature and will simplify the cask design and fabrication by avoiding a thermocouple penetration through the cask pressure boundary.

Because the partial pressure of the air in the cask will increase during the first few months after packaging (due to an increase in temperature), the pressure will be monitored at frequent intervals during this period. Excessive pressure, if any, will be relieved through a sampling manifold into an evacuated waste-gas cylinder.

4.3.4 Transfer and Storage of Remote-Handled Wastes - Drywells

Below-grade drywells could be utilized as a means and method for the interim storage of waste requiring major shielding and isolation. If RHTRU waste packages of a configuration not compatible with drywell dimensional limits are received, they could be stored in concrete casks as previously discussed.

Drywell passive storage would consist of 30- and 18-inch-diameter steel pipe extending about 24 feet below the ground, as shown in Figure 4.18. The ground provides shielding from radiation and permits dry heat dispersion by conduction through the surrounding soil to the atmosphere. The bottom of the pipe is sealed by welding and the top of the drywell is sealed by gasketing or welding. A small sealed tube is provided for sampling the drywell interior on a periodic basis for airborne activity.

4.3.4.1 Transportation and Placement Systems

After a drywell package, which would typically contain three BWR fuel elements, one PWR fuel element or one HLW canister, has been either prepared or checked out in the WHF, it and sand shielding material will be transported



FIGURE 4.18. Reference Drywell Encasement

to the storage area in a shielded cask transporter vehicle. The sequence of the canister placement operations, as illustrated in Figure 4.19, will be in three major steps: drywell preparation, package placement, and completion of placement. These placement activities may be described as follows:

 A cask-positioning fixture will be installed over the drywell to facilitate alignment of the transporter cask on the drywell centerline.





FIGURE 4.19. Drywell Canister Unloading Sequence

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 The transporter vehicle will be driven into position over the drywell for placement of the package. The bottom gate of the transporter cask will be opened and a radiation shield sleeve, located inside the cask, will be lowered into the drywell. The package or canister, attached to a grapple, will be lowered by a hoist mechanism built into the transporter cask.

14

- After the package has been placed in the drywell, ~30 ft³ of sand will be discharged from the transporter sand hopper into the space above the canister to fill the upper compartment of the drywell. As the sand fills the compartment, the radiation shield will be retracted into the shield cask.
- Upon completion of these tasks, the transporter cask will be lifted into the transport position and the cask bottom gate closed. The transporter will then return to the WHF loadout station for another package.
- The cask positioning fixture will be removed and relocated to the next drywell scheduled for package placement. The closure plate will be bolted or welded to the top of the drywell encasement.

The transporter will be supported by and will travel on large earthmover-type pneumatic tires. The transporter speed will be limited to a maximum 10 miles/hour.

The fuel and HLW canisters will be shielded by a vertical, cylindrical bottom-loading cask mounted on the transporter. The cask will be complete with a hoisting mechanism and a grapple device to permit vertical loading and retrieval of the canister.

The transporter will be equipped with positioning mechanisms for vertical, horizontal, and angular adjustment of the cask for alignment with the drywell centerline. The transporter will be capable of handling a package with maximum dimensions of 18 ft 5-1/2 inches in length and 16 inches in diameter. The heaviest package weight will be ~3850 pounds.

4.3.4.2 Drywell Storage Field

Each drywell consists of a cylindrical carbon-steel package encasement vessel that projects ~6 inches above and extends ~24 feet below the ground surface, as shown in Figure 4.18. The encasement vessels will be shop-fabricated of 18-inch- and 30-inch-diameter pipe joined by a pipe reducer. The encasement will be closed at the bottom by a pipe cap welded onto the 18-inch-diameter lower section of the encasement. The closure plate on top of the encasement vessel will be either field welded to the encasement or bolted to provide secondary containment after placement of a package.

The drywells in the storage area will consist of vertical steel encasements buried in the ground in a rectangular array, with a uniform 17-foot center-to-center spacing for spent fuel assemblies and a 44-foot spacing for HLW canisters. The initial storage field for fuel will contain about 1110 drywells, with primary and secondary road systems for package transport, support equipment, and security vehicles.

The storage area will be expandable by modular construction of drywells to ensure a minimum availability of 1 year of storage capacity in advance of ongoing storage operations. It is assumed that the conductivity of the soil will effectively transfer 1 kW/hr of thermal decay heat from the spent fuel packages to the atmosphere on a 17-foot spacing. However, to facilitate the transfer of the 2.3 kW/hr decay heat from the HLW packages, an 11- to 12-inch blanket of a more highly conductive material (e.g., concrete) will be placed around the drywell encasements that are on 44-foot spacings.

4.3.4.3 Drywell Monitoring

A monitoring and surveillance program will be implemented and maintained throughout the life of the drywell field. Design permits continuous monitoring of the interior of each drywell. Utilization of a pressure sensor permits continuous signal transmission and automatic sensing and recording by a multipoint integration system. The interior of each drywell will also be sampled on an established basis for airborne activity through a sample valve located on top of the drywell closure. In order to detect any abnormal thermal conditions, a thermocouple will be provided on the exterior of selected drywell encasements for periodic measurements of the temperature within the drywell.

Monitoring and service trucks with portable thermocouple and pressure readout and recording instrumentation, pressure gauge and gas sampling manifolds, and sample bottles will be used to periodically measure the environment within each drywell. Encasement air samples will be withdrawn into a sample bottle and analyzed in the WHF laboratory for evidence of inert gas leakage from the stored packages.

Measure of the drywell encasement exterior surface temperature will provide an indirect measurement of the fuel element temperature and will simplify the encasement design and fabrication by avoiding a thermocouple penetration through the encasement shell.

The pressure in each drywell will also be measured on a scheduled basis to detect any abnormal changes in pressure. Because the partial pressure of the air in the encasement will increase during the first few months after package placement (due to an increase in temperature), the pressure will be monitored at frequent intervals. Excessive pressure will be relieved through a sampling manifold into an evacuated waste-gas cylinder.

4.3.5 Service Facilities

In addition to the WHF and the storage areas, other support and servicing buildings and facilities as shown in Figures 4.6, 4.7, and 4.20 will be provided for the efficient and safe operation of the MRS/IS facility, first in its role as interim storage and later as the basic surface facility for the co-located repository. Because of the existence and close proximity to various services such as fire and emergency vehicles, no site-specific facilities are provided for these.

4.3.5.1 Administration Building

A one-story building of 6000 to 8000 ft² provides office and storage space for the onsite administration, quality assurance, safety, and engineering personnel, provided overall administrative functions are conducted in other existing Hanford Site buildings.

FACILITY INDEX



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4.3.5.2 Maintenance Building

A one-story building of about 15,000 ft^2 provides the supporting shops and associated shop storage for the MRS/IS operation.

4.3.5.3 Material Warehouse Building

The material warehouse, a building of varying heights, consists of two functional portions: a high bay building of about 50 feet high and a low bay for administrative and small equipment storage. The total building has about 20,000 ft². The high bay portion of the building has a bridge crane for handling operating supplies and spare equipment for the WHF and other support buildings. Forklift truck access will be provided for stacked pallet racks and floor storage areas. Also, areas will be provided for outdoor storage of large equipment items.

4.3.5.4 Gate Houses

There are two, one-story gate house buildings for the area. The first provides a security check area for entering employees and visitors and the second is for rail car and truck shipments. Truck inspection and rail car inspection pits are provided adjacent to the second guard station.

4.3.6 Service Utilities

Water, electrical power, roads and railways to the MRS/IS facility are assumed to be available from sources on the Hanford Site. Descriptions of these utility systems plus several in-area systems are given below.

4.3.6.1 Water Supply

The water supply system delivers water to the required in-plant systems; these include the raw water system, water treatment, water storage, water distribution and the fire protection system. Raw water will be received from an existing export line pumping station. A water treatment plant is provided for a sanitary water supply. Distribution pumps will maintain a 100 psig normal distribution network for sanitary and process use.

The fire protection system will include a 250,000-gallon water tank and two fire pumps discharging into the facility water distribution network

supplying fire hydrants, sprinkler systems and fire hoses. One pump will be electric-motor-driven and one will be diesel-engine-driven.

4.3.6.2 Electrical Power Systems

Normal and emergency standby power systems will be provided. Offsite power will be obtained at 115 or 230 kV and will be brought to a new substation that will reduce the voltage to 13.8 kV. Dual electrical feed systems to the substation are planned for maximum reliability. From the main substation the power will be distributed to the various building and centers via 13.8 kV direct burial cables.

Emergency standby power will be provided to vital systems by means of a turbine generator set. An essential function of this system is to restore power to those essential loads which must maintain safety functions but can accept short duration interruption in power. Uninterruptable power will be supplied by batteries to those systems that cannot accept short duration interruptions.

4.3.6.3 Sanitary Waste Disposal System

A sanitary waste disposal system will be provided to collect, treat, and dispose of a maximum flow of 10,000 gallons/day of sanitary waste generated at the proposed facility. Sewage collection will be through an underground gravity pipe system. The sewer pipe will be laid under 4-1/2 feet of earth cover for frost protection. Sewage will be treated in a prepacked, extended aeration, biological treatment plant which will meet all local, state and federal effluent discharge standards. Effluent from the treatment plant will be discharged to an offsite subsurface tile drainage field. Wastes from potentially, radioactively contaminated sources will not be discharged to the sanitary waste disposal system, but will be treated within the facility waste treatment system.

4.3.6.4 Communications and Fire Alarm System

Communication systems for the facility will include a PA system, a plant intercom system, and telephone systems for both inside and outside calls.
Security communications will be handled primarily by the Hanford Site radio system. Evacuation, radiation alert, and fire alarm systems also will be provided.

The PA system will be used for paging and for emergency instructions within the WHF, including the storage fields. Paging may be done from designated telephones as well as from the emergency communications center in the Patrol Headquarters building.

The fire alarm system will be transmitted directly to the fire station as well as sounding local alarms to warn personnel to evacuate.

4.3.6.5 Radiation Monitoring and Surveillance

Radiation monitoring will be conducted both inside and outside the buildings and in the storage yards to assure that radiation levels and airborne particulate levels on or about the facility or area do not exceed preset limits. Monitors located in areas frequented by onsite personnel will have local alarm capability. Other monitors and monitoring devices will be under continuous surveillance at the environmental console or will be periodically checked by health physics personnel.

Area and perimeter monitoring will be accomplished with continuous air monitors (CAMs) and ion-chamber-type dosimeters strategically placed around the outside boundary of the site to provide continuous monitoring of the immobilized spent fuel and remote handled wastes. The heaviest concentration of units will be located downwind from the facility. The CAMs will be of the fixed-filter type and designed to withstand exposure to adverse elements of the environment.

Preliminary radiation monitors will be placed strategically around the outside boundary of the site. The heaviest concentration of units will be located downwind of the prevailing winds. Three types of monitors will be used: area gamma monitors, beta-gamma particulate monitors, and thermoluminescent dosimeters.

4.4 COST ESTIMATE AND SCHEDULES

This section contains the estimated cost for the MRS/IS facility, and the bases for developing life cycle costs for the scenarios described previously. Cost estimates are based upon the use of constant unescalated 1982 dollars. Construction schedules are adjusted to satisfy the needs as specified in the scenarios.

4.4.1 MRS/IS Facility Base Cost and Construction Schedule

It is estimated that detailed design will require 30 months. Construction will overlap the design by 1 year and is estimated to continue for 4 years. Total time from authorization to hot operation of the facility is estimated to be 5 1/2 years. The design and construction schedule is shown in Figure 4.21.

It is assumed that the facility is constructed during the period 1985 to 1990. The disbursement schedule associated with this construction time table is: a 5 percent expenditure in 1985, a 15 percent expenditure in 1986, a 20 percent expenditure in 1987, 25 percent expenditures in 1988 and 1989, and a 10 percent expenditure in 1990.

The estimated cost to design, construct and outfit the facilities described in Subsection 4.3 is \$178 million. Initially, the facility consists of: 1) a waste handling building, 2) a basic storage yard consisting of one TRUSS building and a cask storage yard designed to accommodate 1000 storage units but equipped only with 100 concrete storage pads, and 3) support or auxiliary buildings (i.e., an administration, maintenance, warehouse, and patrol buildings), security system, etc. A summary of the cost estimates is provided in Table 4.7.

The capital costs include the direct construction costs and the percentages of construction costs assigned for the functions of design, indirect labor, contingency, and owner's cost for contract management. The general bases used for the capital, operating, and decommissioning costs are presented in Table 4.8.

ACTIVITY DESCRIPTION	1	2	3	4	5	6	7
TITLE I & II ENGINEERING DESIGN PREPARE SPECIFICATIONS AND PROCURE EQUIPMENT SITE-YARD EARTHWORK							
WASTE HANDLING FACILITY			• • • • •		<u> </u>		
AUXILIARY BUILDINGS					···· ··· ·· ·· · · · ·		
UTILITIES					•		
PERIMETER INSTRUMENTATION					•		
CHECKOUT OF EQUIPMENT							
ATPS						inanyi iliya	
COMPLETE READINESS REVIEW							
HOT OPERATION STARTUP		48-M	ONTH CON	STRUCTION		▼	

YEARS AFTER AUTHORIZATION

FIGURE 4.21. Postulated MRS/IS Facility Design and Construction Schedule

	TABLE 4.7. Construction Capital Cost Sum (thousands of mid-1982 dollar	nary s)
A.(a)	Construction	
	Offsite Development (electrical, roads, railroads, water)	\$7,500
	Land Improvements (railroads, roads, sidewal	ks) 4,200
	Waste Handling Facility	44,200
	Cargo Receiving and Shipping8,00Hot Cell11,00Radwaste System10,80Hot Maintenance Shop70Mechanical Electrical Instrument5,20System8,50	0 0 0 0 0
	Service Facilities (standby generator, security buildings)	6,000
	Storage Facilities (warehouse, rail cars)	2,500
	Other Facilities	1,850
	Waste Handling System	2,450
	Area Service Systems (electrical, security, water, radiological waste management, lighti	32,000 ng)
	TRUSS Building	2,500
	Transporter and Gantry Crane	2,000
	Subtotal	\$105,200
Β.	Cask Storage Yard (100 pads)	320
С.	Indirect Costs (12.5% of A + B)	13,200
D.	Engineering and Services (12% of A + B + C)	14,250
Ε.	Contingency (25% of A + B + C + D)	33,250
F.	Owners Cost (7% of A + B + C + D + E)	11,780
	Total Cost	\$178,000

(a) Letters refer to categories of cost as listed in Table 4.8.

TABLE 4.8. Cost Estimating Factors

	Initial Facility	Each Additional Storage Increment
Capital Costs	(a)	
Non-repetitive Repetitive	A B	_ В
Indirect Costs Construction Services and Field Office Engineering Services C = 12.5% of A + B + C	С	С
Home Office Engineering and Services D = 12% of A + B + C D ₁ = 6% of B + C	D	D ₁
Contingency E = 25% of A + B + C + D E ₁ = 25% of B + C + D ₁	E	E1
Owner's Cost F = 7% of A + B + C + D + E F ₁ = 4% of B + C + D ₁ + E ₁	F	F1
Operating Costs		
Labor (Estimated)	G	G
Consumables 10% of G	H	Н
Maintenance Supplies and Contract Labor 2% of A + B + C	Ι	Ι
G&A, Utilities, Supervision, Cost of Capital J = 12% of G + H	J	J

Decommissioning Cost = 10% of Capital Cost

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(a) These letter designations are used in Tables 4.7 and 4.14.

The estimated costs associated with bringing the utility systems to the site are presented in Table 4.9, assuming the indicated distances are appropriate for connection to existing Hanford systems.

TABLE 4.9.	Construction	Costs for	Utilities
	(millions of	mid-1982	dollars)

	<u>Per Mile</u>	<u>Total</u>
Water - River Pumps and 10-in. Pipe (7 miles)	0.160	3.83
Electrical – 115 kVA, 10 MW (5 miles)	0.087	0.44
Roads – 2 Lane, Heavy Duty (5 miles)	0.275	1.38
Railroad – Single Track (5 miles)	0.370	1.85
		7.50

4.4.2 Cost and Schedule: Reference Metal Storage Casks

The number of metal casks required to store spent fuel and HLW varies for each scenario. A schedule for the purchase of casks is provided in Table 4.10. The following assumptions are used in developing the data provided in that table:

- Metal cask storage capacities (payload) are:
 - 14 HLW waste canisters per cask
 - 52 BWR spent fuel assemblies per cask
 - 24 PWR spent fuel assemblies per cask
- Casks will be purchased in the year of their actual use.

Each cask purchased, regardless of design payload, is assumed to cost \$700,000 plus a 25 percent contingency, or \$875,000. The purchase of casks is assumed to be a capital expenditure.

4.4.3 Cost and Schedule: Metal Cask Support Pads

Cask support pads will be constructed as the need arises. Initially the facility will incorporate 100 storage pads on a storage field designed to accommodate 1000 storage units (casks). A schedule for adding additional storage pads and additional storage fields is provided in Table 4.11.

	Reference Scenario		Delayed Re	eprocessing	Delayed Disposal		
Year_	Number	<u>Cost^(a)</u>	Number	<u>Cost(a)</u>	Number	<u> Cost(a)</u>	
1990	17	14.875	47	41.125	17	14.875	
1991	33	28.875	54	47.250	33	28.875	
1992	50	43.750	67	58.625	50	43.750	
1993	50	43.750	67	58.625	50	43.750	
1994	50	43.750	102	89.250	50	43.750	
1995	50	43.750	127	111.125	50	43.750	
1996	50	43.750	152	133.000	50	43.750	
1997	50	43.750	155	135.625	50	43.750	
1998					50	43.750	
1999					50	43.750	
2000					50	43.750	
2001					67	58.625	
2002					83	72.625	
2003					100	87.500	
2004					100	87.500	
2005					100	87.500	
2006					134	117.250	
2007					166	145.250	
2008					140	122.500	
2009					140	122.500	
2010					140	122.500	
2011					174	152.250	
2012					96	84.000	
2013							
2014					80	70.000	
2015							
2016							
Total	350	306.250	771	674.625	2020	1767.500	

TABLE 4.10. Schedule and Costs for Annual Purchases of Metal Storage Casks

(a) Costs in millions of mid-1982 dollars.

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	Reference Scenario			Delayed Reprocessing				Delayed Disposal				
Year	No. Pads	Cost ^(a)	No. Fields	Cost ^(a)	No. Pads	Cost ^(a)	No. Fields	Cost ^(a)	No. Pads	Cost ^(a)	No. Fields	Cost ^(a)
1985 1986 1987 1988 1989	100	0.2	1	0.3	100	0.2	1	0.3	100	0.2	1	0.3
1990 1991					100	0.2						
1992 1993	100	0.2			100 100	0.2 0.2			100	0.2		
1994 1995	100	0.2			100 200	0.2			100	0.2		
1996 1997	100	0.2			80	0.16			100	0.2		
1998 1999									100	0.2		
2000 2001 2002		•							100 100 100	0.2 0.2 0.2		
2003 2004 2005 2006									100 100 100 200	0.2 0.2 0.2 0.4	1	0.3
2007 2008 2009									200 100 100	0.4 0.2 0.2	_	
2010 2011			_				_		200 50	$\frac{0.4}{0.1}$	1 	0.3
Total	400	0.8	1	0.3	780	1.56	1	0.3	2020	4.04	3	0.9

TABLE 4.11. Schedule and Costs for Annual Construction of Storage Pads and Storage Fields for Metal Casks

(a) Costs in millions of mid-1982 dollars.

The cost associated with each are assumed to be \$2,000 per storage pad and \$300,000 per storage field including indirect costs. It is assumed that storage pads and new storage fields are added the year prior to the need. Within reason, basic modules (additions) are assumed to be in multiples of 100 storage pads. The costs associated with construction of additional storage pads and storage areas are assumed to be a capital expenditure.

4.4.4 Cost and Schedule: Concrete Casks

Concrete storage casks will be used to store RHTRU for both the Reference scenario and the Delayed Disposal scenario. The following assumptions are used to delineate a schedule for the purchase of concrete storage casks.

- Concrete cask storage capacities are:
 - 12 RHTRU drums/cask
 - 3 RHTRU canisters/cask
- Storage casks are reused if available.
- Storage casks are purchased in the year of their need or use.

A schedule for the purchase of concrete storage casks for both the Reference scenario and the Delayed Disposal scenario is presented in Table 4.12. The cost of each concrete cask was assumed to be \$25,000. The costs associated with purchasing concrete storage casks are assumed to be capital expenditures.

4.4.5 Cost and Schedule: Concrete Cask Support Pads

Concrete cask support pads will be constructed as the need arises. The pads will be constructed in modules of 500 in storage fields designed to accommodate 1000 storage units. The first storage pads and storage field will be constructed in 1988. Subsequent storage pad modules and additional storage fields will be constructed the year prior to their need. The schedule of construction storage pads and fields for concrete casks is presented in Table 4.13. The estimated cost associated with construction of each storage pad is \$2,000 and with each storage field is \$300,000 including indirect costs. The costs resulting from adding storage pads and storage fields are assumed to be capital expenditures.

4.4.6 TRUSS Buildings

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For the Delayed Disposal scenario, additional TRUSS buildings will be constructed in the years 2003, 2006, 2009 and 2013 to store the projected quantities of CHTRU. Each additional storage unit (TRUSS building) is assumed to cost \$2.5 million. The cost associated with constructing each additional TRUSS building is assumed to be a capital expenditure.

	Referen	Reference Scenario		Delayed Disposal		
Year	Number	Cost ^(a,b)	Number	Cost ^(a,b)		
1990	81	2.025	81	2.025		
1991	162	4.050	162	4.050		
1992	241	6.025	241	6.025		
1993	241	6.025	241	6.025		
1994	241	6.025	241	6.025		
1995	241	6.025	241	6.025		
1996	241	6.025	241	6.025		
1997	242	6.050	242	6.050		
1998			241	6.025		
1999			241	6.025		
2000			241	6.025		
2001			322	8.050		
2002			402	10.050		
2003			482	12.050		
2004			482	12.050		
2005			483	12.075		
2006			643	16.075		
2007			805	20.125		
2008			630	15.750		
2009			632	15.800		
2010			632	15.800		
2011			793	19.825		
2012			378	9.450		
2013			319	7.975		
2014			318	7.950		
Total	1690	42.250	9734	243.350		
Total	1690	42.250	9734	243.350		

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TABLE 4.12. Schedule and Costs for Annual Purchases of Concrete Storage Casks

(a) Costs in millions of mid-1982 dollars.
(b) The number of significant figures is for computational accuracy and does not imply precision to the nearest \$1000.

		Referenc	e Scenar	io	Delayed Disposal				
<u>Year</u>	No. Pads	<u>Cost^(a)</u>	No. <u>Fields</u>	<u>Cost^(a)</u>	No. Pads	<u>Cost^(a)</u>	No. Fields	<u>Cost(a)</u>	
1988 1989 1990	500	1.0	1	0.3	500	1.0	1	0.3	
1991 1992 1993	500	1.0	1	0.3	500	1.0	1	0.3	
1994 1995	500	1.0			500	1.0			
1996 1997 1998	190	0.38			500 500	1.0	1	0.3	
1999 2000 2001					500	1.0	1	0.3	
2002					500 500 500	1.0 1.0 1.0	1	0.3	
2004 2005					500 500	1.0 1.0	1	0.3	
2006 2007					1000 500	2.0 1.0	1	0.3	
2008 2009 2010 2011 2012					500 500 1000 500 234	1.0 1.0 2.0 1.0 0.47	1 1 1	0.3 0.3 0.3	
Total	1690	3.38	2	0.6	9734	19.47	10	3.0	

TABLE 4.13. Schedule and Costs for Annual Construction of Storage Pads and Storage Fields for Concrete Casks

(a) Costs in millions of mid-1982 dollars.

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4.4.7 Annual Operating Expense

The annual cost associated with operating the Reference facility (i.e., labor and materials) is estimated to be \$11.53 million. A staff of approximately 138 is required to operate the MRS/IS facility and approximately 62 support personnel are needed to administer and safeguard the facility. A summary of the annual operating expense is presented in Table 4.14.

For the Reference and the Delayed Reprocessing scenarios, it is assumed the co-located geologic repository would come on-line in 1998. Since all of the MRS/IS facility except the interim storage areas would be utilized to service the underground repository, it has also been assumed that most of the operating costs after that date would be to the repository account. This would include the operating expense of removing the various wastes stored in the different interim storage areas and transferring them to the underground repository. As shown in Appendices B and C, this would require several years to accomplish.

A similar approach is assumed for the Delayed Disposal scenario. Although, the first repository comes on-line in 2008, this MRS/IS facility would function and receive wastes until after the second and third repostitories open in 2012 and 2015, respectively. Assuming the first

TABLE 4.14.	Yearly Operating Costs for the MRS/IS Facility
	(millions of mid-1982 dollars)

G.(a)	Labor	
	Waste Handling Facility (~138 staff) Support Personnel (~62 staff)	5.03 2.41
Н.	Consumables (10% of G)	0.74
Ι.	Maintenance (2% of A + B + C of Table 4.7)	2.37
J.	G&A, Utilities, Supervision, Cost of Capital (12% of G + H)	0.98
Total		11.53

(a) Letters refer to categories of cost as listed in Table 4.8.

repository would be the one co-located with this MRS/IS facility, then the operating costs of the original facility would be assumed by the repository in 2016. Between 2008 and 2016 the cost of operating the MRS/IS facility would be shared with the repository.

4.4.8 Transportation Costs

The bases for assigning transportation costs are described in Subsection 3.5, with additional details presented in Appendix C. A summary of the transportation cost for each scenario is provided in Table 4.15. The transportation cost is assumed to be an operational expense. Only those incremental offsite transportation costs associated with the MRS/IS facility that are in addition to the transportation costs normally required in the waste management system without an MRS/IS facility are included in the MRS/IS facility life cycle costs.

4.4.9 Drywell Storage

An alternative to storing spent fuel and HLW in a metal storage cask on the surface is a drywell imbedded in the soil. In this case, the RHTRU canisters and drums continue to be stored in the surface-mounted concrete casks, as before.

For the drywell storage system it is assumed that minimum changes would be required to either the design or the operation of the WHF. Since the hot cells within the building has an adequately-sized, semi-automatic system for canistering of failed fuel or HLW, no capacity increases are needed for canistering of all fuels. The other operations such as fuel unloading or loading require essentially the same systems as for the reference cask storage.

Other supporting buildings, services and utilities for drywell storage are the same as for the reference metal cask. The cost of the transporter for the drywell system is essentially the same as the cost of the trailer and gantry for the cask system.

The cost of constructing a drywell is estimated to be \$18,000 each including indirect costs. The drywells are arranged in fields of 1000 wells each and each field is estimated to cost \$300,000 to prepare.

	Referen	ce Scenario	Delayed H	Reprocessing	Delayed	Delayed Disposal		
	Total	MRS	Total	MRS	Total	MRS		
Year	System	Incremental	System	Incremental	System	Incremental		
1990	17.675	0	40.097	32.536	60.778	0		
1991	34.794	0	45.893	43.934	36.136	0		
1992	51.918	0	56.140	45.626	51.918	0		
1993	51.918	0	58.091	45.933	51.918	0		
1994	51.918	0	87.039	70.595	51.918	0		
1995	51.918	0	108.416	88.206	51.918	0		
1996	51.918	0	130.202	105.797	51.918	0		
1997	51.918	0	130.340	105.783	51.918	0		
1998		0			51.918	0		
1999		0			51.918	0		
2000		0			51.918	0		
2001		0			69.232	0		
2002		0			86.445	0		
2003		0			102.859	0		
2004		0			102.859	0		
2005		0			102.859	0		
2006		0			138.356	0		
2007		0			1/2.841	0		
2008		0			141.166	0		
2009		0			141.166	0		
2010	01 000	U			141.166	0		
2011	21.929	U	54 262	EA 262	1/5.920	U		
2012	10.300	U	54.202	54.202 42.700	92.551	0		
2013	20.898	0	42./99	42./99	45.900	0		
2014	39.035	0	10.229	/0.229 155 700	0/./10	0		
2015		0	100./00	100./00	10 006	0		
2010		0	230.430	230.430	10.990	0		
2017	<u> </u>		00.001	00.001				
Total	462.139	0	1312.600	1193.139	2163.503	0		

TABLE 4.15. Annual Transportation Costs for Each Scenario (millions of mid-1982 dollars)^(a)

(a) The number of significant figures is for computational accuracy and does not imply precision to the nearest \$1000.

Fuel placed in a drywell must be sealed within a canister. Each canister will hold 3 BWR or 1 PWR fuel assembly and is estimated to cost \$5500. The cost of preparing the field and the construction and installation of the drywells are assumed to be capital expenditures. The cost of the canisters is assumed to be an operating expense.

A schedule for the construction of storage field and drywells is given in Table 4.16, together with the annual capital expenditures for that construction and installation work for the three fuel cycle scenarios.

4.4.10 Decommissioning Costs

With the exception of the storage casks and storage fields, all of the MRS/IS facilities become the surface facilities for the co-located repository when repository operations are begun. Therefore, the cost of decommissioning the surface facilities (except for casks and storage fields), which is estimated to be about 10 percent of the capital cost of these facilities or about \$18 million, is not chargeable to the MRS/IS system but is charged to the repository system when the repository is closed. It is anticipated that the costs of decontaminating and removing the casks, support pads and storage fields will be paid from funds recovered when the decontaminated metal casks are sold for salvage. As a result, no net costs are assigned to the MRS/IS facility co-located with a repository for decommissioning.

4.5 LIFE CYCLE COSTS

To provide compatibility with other studies of spent fuel and waste disposal, life cycle costs are evaluated for the Reference, Delayed Reprocessing, and Delayed Disposal scenarios for the MRS/IS facility co-located with a repository. All costs are presented in terms of constant value, mid-1982 dollars (no escalation or inflation). The bases for costs are provided in Subsection 4.4. In addition to undiscounted program costs, a present worth program cost using a discount factor of 2 percent is included.

		Referenc	e Scenar	<u>io</u>	D	elayed Re	processi	ng		Delayed	Disposal	
	No.				No.				No.			
Year	Dry- wells	<u>Cost(a)</u>	No. <u>Fields</u>	<u>Cost(a)</u>	Dry- wells	<u>Cost</u> (a)	No. <u>Fields</u>	<u>Cost</u> (a)	Dry- <u>wells</u>	<u>Cost(a)</u>	No. <u>Fields</u>	<u>Cost(a)</u>
1988 1989	1000	18.0	1	0.3	1000	18.0	1	0.3	1000	18.0	1	0.3
1990					1500	27.0	2	0.6				
1991	500	9.0	1	0.3	1500	27.0	1	0.3	500	9.0	1	0.3
1992	1000	18.0	ī	0.3	1500	27.0	2	0.6	1000	18.0	1	0.3
1993	1000	18.0	1	0.3	2000	36.0	2	0.6	1000	18.0	1	0.3
1994	500	9.0			3000	54.0	3	0.9	500	9.0		
1995	500	9.0	1	0.3	3000	54.0	3	0.9	500	9.0	1	0.3
1996	500	9.0			3000	54.0	3	0.9	500	9.0		
1997									1000	18.0	1	0.3
1998									500	9.0	1	0.3
1999									500	9.0		
2000									1000	18.0	1	0.3
2001									1500	27.0	2	0.6
2002									1000	18.0	1	0.3
2003									1500	27.0	1	0.3
2004									1500	27.0	2	0.6
2005									2000	36.0	2	0.6
2006									2000	36.0	2	0.6
2007									2000	36.0	2	0.6
2008									2000	36.0	2	0.6
2009									2000	36.0	2	0.6
2010									2500	45.0	2	0.6
2011									1500	27.0	2	0.6
2012									500	9.0	1	0.3
2013									300	5.4		
2014												
2015 2016									100			
Total	5000	90.0	5	1.5	16,500	297.00	17	5.1	28,300	509.4	29	8.7

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TABLE 4.16. Schedule and Costs for Annual Construction of Drywells and Drywell Fields

(a) Costs in millions of mid-1982 dollars.

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4.5.1 Reference Scenario Life Cycle Costs

A summary of the program costs associated with the Reference scenario, using metal storage casks, is presented in Table 4.17. The undiscounted life cycle cost is estimated to \sim \$0.731 billion. The discounted life cycle cost is estimated to be \sim \$0.578 billion.

A similar summary for the Reference scenario, using drywells for storage of spent fuel and HLW canisters instead of metal casks, is given in Table 4.18. The undiscounted life cycle cost is estimated to be ~\$0.518 billion. The discounted life cycle cost is estimated to be ~\$0.412 billion.

In developing these cost estimates, it is assumed that for any year in which MRS/IS operations occur after the opening of the repository in 1998, the operating costs are divided approximately equally between the MRS/IS facility and the repository. Thus in the years 1998 through 2015, the annual MRS/IS facility operating cost is \$6.0 million.

Included in the operating costs for the drywell case are the cost of the canisters in which the spent fuel is encapsulated.

4.5.2 Delayed Reprocessing Scenario Life Cycle Costs

A summary of the program costs associated with the Delayed Reprocessing scenario, using metal storage casks, is presented in Table 4.19. The undiscounted life cycle cost is estimated to be \sim \$2.294 billion. The discounted life cycle cost is estimated to be \sim \$1.592 billion.

A similar summary for the Delayed Reprocessing scenario, using drywells for storage of spent fuel instead of metal casks, is given in Table 4.20. The undiscounted life cycle cost is estimated to be \sim \$2.013 billion. The discounted life cycle cost is estimated to be \sim \$1.376 billion.

As in the Reference scenario, the costs of operations in years following opening of the repository are divided between the MRS/IS facility and the repository for those years in which material was placed in storage or was shipped off-site. Again, the cost of canisters for spent fuel is included in the operating cost for the drywell case.

	Capital C	osts			
	Handling and		Operating	Transport	
Year	Support	Storage	<u> Costs </u>	Costs	<u> </u>
1985	8.900				8.900
1986	26.700				26.700
1987	35.600				35.600
1988	44.500	1.300			45.800
1989	44.500	16 000	11 500		44.500
1990	17.800	16.900	11.530		46.230
1991		32.925	11.530		44.455
1992		50.975	11.530		62.505
1993		50.075	11.530		61.605
1994		50.975	11.530		62.505
1995		49.775	11.530		61.305
1990		50.355	11.530		61.885
1997		49.800	11.530		61.330
1998			6.000		6.000
1999			6.000		6.000
2000			6.000		6.000
2001			6.000		6.000
2002			6.000		6.000
2003			6.000		6.000
2004			6.000		6.000
2005			6.000		6.000
2006			6.000		6.000
2007			6.000		6.000
2008			6.000		6.000
2009			6.000		6.000
2010			6.000		6.000
2011			6.000		6.000
2012			6.000		6.000
2013			6.000		6.000
2014			6.000		6.000
2015			6.000		6.000
Total	178.000	353.080	200.24	0.0	731.320
Discounted Total(C)					578.165

TABLE 4.17. MRS/IS Facility Co-located With a Repository--Reference Scenario, Life-Cycle Cash Flows: Cask Storage (millions mid-1982 dollars)^(a)

(a) The number of significant figures is for computational accuracy and does not imply precision to the nearest \$1000.

(c) Discount rate of 2 percent per year.

⁽b) Transportation costs are incremental to those which would be incurred if no MRS existed.

_	Capital Co	osts			
Year	Handling and Support	Storage	Operating <u>Costs</u>	Transport Costs(D)	Total
1985 1986	9.000 27.000				9.000 27.000
1987 1988 1989 1990 1991	36.000 45.000 45.000 18.000	19.600 2.025 13.350	11.530 11.530		36.000 64.600 45.000 31.555 24.880
1992 1993 1994 1995 1996		25.325 74.625 16.025 15.325 15.405	11.530 11.530 11.530 11.530 11.530 11.530		36.855 36.155 27.555 26.855 26.935
1997 1998 1999 2000 2001		6.050	$ \begin{array}{r} 11.530 \\ 6.000 \\ 6.000 \\ 6.000 \\ 6.000 \\ \end{array} $		17.580 6.000 6.000 6.000 6.000
2002 2003 2004 2005 2006			6.000 6.000 6.000 6.000 6.000		6.000 6.000 6.000 6.000 6.000
2007 2008 2009 2010 2011			6.000 6.000 6.000 6.000 6.000		6.000 6.000 6.000 6.000 6.000
2012 2013 2014 2015			6.000 6.000 6.000 6.000		6.000 6.000 6.000 6.000
Total Discounted Total(c)	180.000	137.730	200.240	0.0	517 . 970 412 . 430

TABLE 4.18. MRS/IS Facility Co-located With a Repository--Reference Scenario, Life-Cycle Cash Flows: Drywell Storage (millions mid-1982 dollars)^(a)

(a) The number of significant figures is for computational accuracy and does not imply precision to the nearest \$1000.

(b) Transportation costs are incremental to those which would be incurred if no MRS existed.

(c) Discount rate of 2 percent per year.

	Capital Co	osts				
Year	Handling and Support	Storage	Operating <u>Costs</u>	Transport Costs(D)	Total	
1985 1986	8.775 26.325				8.775 27.325	
1987 1988 1989 1990 1991	35.100 43.875 43.875 17.550	41.325 47.250	11.530 11.530	32.816 37.548	35.100 43.875 43.875 103.221 96.328	
1992 1993 1994 1995 1996		58.825 58.825 89.450 111.525 133.160	11.530 11.530 11.530 11.530 11.530 11.530	46.151 47.166 71.308 88.816 106.462	116.506 117.521 172.288 211.871 251.152	
1997 1998 1999 2000 2001		135.625	$ \begin{array}{r} 11.530 \\ 6.000 \\ 6.000 \\ 6.000 \\ 6.000 \\ 6.000 \\ \end{array} $	106.490	253.645 6.000 6.000 6.000 6.000	
2002 2003 2004 2005 2006			6.000 6.000 6.000 6.000 6.000		6.000 6.000 6.000 6.000 6.000	
2007 2008 2009 2010 2011			6.000 6.000 6.000 6.000 6.000		6.000 6.000 6.000 6.000 6.000	
2012 2013 2014 2015 2016 2017			6.000 6.000 6.000 6.000 6.000 6.000	54.262 42.799 76.229 155.783 238.458 88.851	60.262 48.799 82.229 161.783 244.458 94.851	
Total Discounted Total(c)	175.500	675.985	212.240	1193.139	2256.864 1592.323	

TABLE 4.19. MRS/IS Facility Co-located With a Repository--Delayed Reprocessing Scenario, Life-Cycle Cash Flows: Cask Storage (millions mid-1982 dollars)^(a)

⁽a) The number of significant figures is for computational accuracy and does not imply precision to the nearest \$1000.

⁽b) Transportation costs are incremental to those which would be incurred if no MRS existed.

⁽c) Discount rate of 2 percent per year.

	Capital C	osts				
Year	Handling and Support	Storage	Operating <u>Costs</u>	Costs (D)		
1985 1986	8.775 26.325				8.775 26.325	
1987 1988 1989 1990 1991	34.600 43.875 43.875 17.550	18.300 27.600 27.300	17.052 17.371	32.816 37 548	34.600 62.175 43.875 95.018 82.219	
1992 1993 1994 1995 1996		27.600 36.600 54.900 54.900 54.900	19.230 19.566 23.438 26.826 29.559	46.151 47.166 71.308 88.816 106.462	92.981 103.332 149.646 170.542 190.921	
1997 1998 1999 2000 2001			29.312 6.000 6.000 6.000 6.000	106.490	135.802 6.000 6.000 6.000 6.000	
2002 2003 2004 2005 2006		·	6.000 6.000 6.000 6.000 6.000		6.000 6.000 6.000 6.000 6.000	
2007 2008 2009 2010 2011			6.000 6.000 6.000 6.000 6.000		6.000 6.000 6.000 6.000 6.000	
2012 2013 2014 2015 2016 2017			6.000 6.000 6.000 6.000 6.000 6.000	54.262 42.799 76.229 155.783 238.458 88.851	60.262 48.799 82.229 161.783 244.458 94.851	
Total Discounted Total(c)	175.000	302.100	302.354	1193.139	1972.593 1375.594	

TABLE 4.20. MRS/IS Facility Co-located With a Repository--Delayed Reprocessing Scenario, Life-Cycle Cash Flows: Drywell Storage (millions mid-1982 dollars)^(a)

(a) The number of significant figures is for computational accuracy and does not imply precision to the nearest \$1000.

(b) Transportation costs are incremental to those which would be incurred if no MRS existed.

(c) Discount rate of 2 percent per year.

4.5.3 Delayed Disposal Scenario Life Cycle Costs

A summary of program costs associated with the Delayed Disposal scenario, using metal storage casks, is presented in Table 4.21. The undiscounted life cycle cost is estimated to be ~\$2.487 billion. The discounted life cycle cost is estimated to be ~\$1.661 billion.

A similar summary for the Delayed Disposal scenario, using drywells for storage of spent fuel and HLW instead of metal casks, is presented in Table 4.22. The undiscounted life cycle cost is estimated to be ~\$1.235 billion. The discounted life cycle cost is estimated to be ~\$0.868 billion.

	<u>Capital C</u>	osts				
Year	Handling and Support	Storage	Operating <u>Costs</u>	Transport Costs(D)		
1985 1986	8.900 26.700				8.900 26.700	
1987 1988 1989 1990 1991	35.600 44.500 44.500 17.800	1.300 16.900 32.925	11.530 11.530		35.600 45.800 44.500 46.230 44.455	
1992 1993 1994 1995 1996		50.975 50.075 50.975 49.775 50.975	11.530 11.530 11.530 11.530 11.530		62.505 61.605 62.505 61.305 62.505	
1997 1998 1999 2000 2001	2.500	50.300 50.975 49.975 51.075 67.875	11.530 11.530 11.530 11.530 11.530		64.330 62.505 61.505 62.605 79.405	
2002 2003 2004 2005 2006	2.500	84.175 100.750 101.350 100.775 136.025	11.530 11.530 11.530 11.530 11.530		98.205 112.280 112.880 112.305 150.055	
2007 2008 2009 2010 2011		166.775 139.750 139.800 140.800 173.175	$11.530 \\ 6.000 \\ 6.000 \\ 6.000 \\ 6.000 \\ 6.000$		178.305 145.750 145.800 146.800 179.175	
2012 2013 2014 2015 2016	2.500	93.920 7.975 77.950	6.000 6.000 6.000 6.000 6.000		99.920 16.475 83.950 6.000 6.000	
Total Discounted Total(c)	188.000	2037.320	261.540	0.0	2486.860 1660.739	

TABLE 4.21. MRS/IS Facility Co-located With a Repository--Delayed Reprocessing Scenario, Life-Cycle Cash Flows: Cask Storage (millions mid-1982 dollars)^(a)

(a) The number of significant figures is for computational accuracy and does not imply precision to the nearest \$1000.

(c) Discount rate of 2 percent per year.

⁽b) Transportation costs are incremental to those which would be incurred if no MRS existed.

	<u> Capital Costs </u>				
	Handling and	<u>C</u>	Operating	Transport	T . 4 . 1
Year	Support	Storage	LOSTS	LOSTS	lotal
1985	9.000				9.000
1986	27.000				27.000
1987	35.500	10.000			35.500
1988	45.000	19.600			64.600
1989	45.000	2 025	11 520		45.000
1990	18.000	2.025	11.530		31.555
1991		13.330	11.550		24.000
1992		25.325	11.530		36.855
1993		24.625	11.530		36.155
1994		16.025	11.530		27.555
1995	2.500	15.325	11.530		29.355
1996		16.025	11.530		27.555
1997		24.650	11.530		36.180
1998		16.325	11.530		27.855
1999		15.025	11.530		26.555
2000		25.625	11.530		37.155
2001		36.650	11.530		48.180
2002	2.500	29.650	11.530		43.680
2003		40.350	11.530		51.880
2004		40.950	11.530		52.480
2005	0 500	49.675	11.530		61.205
2006	2.500	54.9/5	11.530		69.005
2007		57.725	11.530		69.255
2008		53.650	6.000		59.650
2009		53.700	6.000		59.700
2010		63./00	6.000		69./00
2011		48.425	6.000		54.425
2012		19.220	6.000		25.220
2013	2.500	13.375	6.000		21.875
2014		7.950	6.000		13.950
2015			6.000		6.000
2016			6.000		6.000
Total ,	189.500	783.92	261.540		1234.960
Discounted Total(C	;)				867.676

TABLE 4.22. MRS/IS Facility Co-located With a Repository-- Delayed Disposal Scenario, Life-Cycle Cash Flows: Drywell Storage (millions mid-1982 dollars)(a)

(a) The number of significant figures is for computational accuracy and does not imply precision to the nearest \$1000.

(b) Transportation costs are incremental to those which would be incurred if no MRS existed.

(c) Discount rate of 2 percent per year.

5.0 RELATION TO OTHER FACILITIES

The monitored retrievable storage/interim storage (MRS/IS) facility co-located with a geologic repository, as one part of the overall nuclear fuel cycle system, has interfaces with several other parts of the system, such as the nuclear power stations, the reprocessing plants, and the geologic repositories. It also has a number of interfaces with the support systems and services already present in the vicinity of the site. These interfaces are discussed in this section.

5.1 REACTOR POWER STATIONS

As presently conceived, the MRS/IS facility could receive spent fuel from the reactor stations as necessary for the stations to maintain their full core reserve storage capacity. This fuel would be stored until either a reprocessing plant is operating, at which time the fuel would be shipped to the reprocessor, or, if the operation of reprocessing plants is delayed until after a geologic repository is available, some or all of the fuel might be emplaced in the repository without reprocessing. In any event, the principal interface between the MRS/IS facility and the reactor stations is the transportation link by which the spent fuel is transported from the reactors to the MRS/IS facility. Thus, it is essential that the facility is capable of receiving, unloading, loading, and decontaminating any of the present generation of spent fuel shipping casks.

5.2 REPROCESSING PLANTS

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The interface between the MRS/IS facility and the reprocessing plant is also the transportation link whereby spent fuel is shipped from storage to the reprocessor, and solidified high-level waste (HLW) and transuranic (TRU) waste from the reprocessing operation are shipped to the MRS/IS facility for storage pending availability of a geologic repository. Some additional receiving, unloading, and decontamination capability is necessary to accommodate the TRU waste packages.

5.3 GEOLOGIC REPOSITORIES

The reference MRS/IS facility for this study is located near the planned location of a geologic repository. In most respects, the reference MRS/IS facility is equivalent to the surface facilities that would normally be required to support the geologic repository. The radioactive waste is received, unloaded, examined, decontaminated and provided with additional packaging if necessary, and transported to the storage location. The principal differences between placing the waste into the MRS/IS facility or into a repository are in the types of additional packaging that might be required and in the methods of transporting the wastes to the storage location. Only the actual storage containers' storage fields are left unused when the MRS/IS facility is converted into the receiving and handling facility for the repository. Transport of wastes from the handling facility to the repository shaft would be accomplished using essentially the same equipment as is used for the MRS/IS facility.

The unused storage capacity of the MRS/IS facility provides a convenient surge storage for the repository, when and if needed. A list of the main items and functions common to the MRS/IS facility and the repository that would serve to reduce the capital costs for the paired system is given in Table 5.1.

5.4 LOCAL SITE SUPPORT SYSTEMS

The selection of the Hanford Site as the location of the MRS/IS facility co-located with a repository makes possible the utilization of many support services already available on the Site. These services are discussed briefly in this subsection.

5.4.1 Transportation Services

The Hanford Site is served by an existing network of rail lines extending to nearly all parts of the Site. The Hanford rail network is connected directly to the principal railroads operating in the Pacific Northwest, with connections to other major railroads in the U.S.

TABLE 5.1. Items and Functions Shared or Used by Both MRS/IS Facility and the Repository

Capital

Permits and Licenses

Design and Engineering

Site Preparation

Facilities

- Administration
- Receiving/Surge Storage
- Packaging/Transfers
- Support

Engineered Equipment

- Cranes
- Packaging/Transfers
- Decontamination
- Ventilation and Containment
- Spare Parts

Operations

Inspection and QA

Support

Utilities

Operational Personnel

Security Personnel

Maintenance Personnel

Decontamination and Decommissioning

Disposal

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Rehabilitation

Extension of the existing Hanford rail networks to the MRS/IS/Repository site can be accomplished relatively easily, with the length of new track likely to be in the vicinity of 5 miles or less.

The Hanford Site is also served by a network of onsite highways, with connections to major state and interstate highways. Extensions of the existing highway network to the MRS/IS/Repository site can also be accomplished relatively easily, with the length of roadway to be added likely to be in the vicinity of 5 miles or less.

The Hanford Site is also served by river barge on the Columbia River, thus making the shipment of large, heavy items relatively easy.

5.4.2 Essential Services

The Hanford Site is served by a large network of electric power transmission lines owned and operated by the Bonneville Power Administration. These lines interconnect the principal electricity generating stations in the Pacific Northwest and provide an assured source of electrical energy to the facilities on the Hanford Site. Extension of the existing Hanford distribution system to the MRS/IS/Repository site can be accomplished readily.

Water for use at the site would be pumped from the Columbia River at an existing pumping station by the installation of new pumps and delivered to the site through a new delivery line. Alternatively, if the demand for water is not too great, wells could be drilled into the underlying aquifer and the necessary water pumped to the surface. In any event, ample water supplies can be made available.

Sludges from the sanitary waste disposal system and from process waste evaporation ponds would be disposed of at the existing Hanford sludge disposal facilities.

In view of the close proximity of the MRS/IS/Repository to existing Hanford waste treatment facilities, and since the quantities of radioactive waste generated within the MRS/IS/Repository complex are expected to be quite small, extensive systems for treatment of radioative wastes should not be required at the complex.

The Hanford Site is served by an existing telephone system which is connected into the national telephone network. Additional communications are available through the plant radio network, under the control of the plant security forces.

Security for the Hanford Site and for government-owned facilities on the Site is provided by the Hanford Patrol organization. Rapid response to any situations requiring such a response is made possible by a closely-integrated communications system, a fleet of emergency response vehicles, and a large force of well-trained personnel. It is expected that security at the MRS/IS/Repository site would be provided by the Hanford Patrol organization.

5.4.3 Other Support Services

The existing central stores, employee transport, contaminated laundry service, central heavy equipment and vehicle maintenance, and central computing services already in operation on the Hanford Site are available as needed by the MRS/IS/Repository complex.

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6.0 RESULTS AND RECOMMENDATIONS

The monitored retrievable storage/interim storage (MRS/IS) facility design which is evaluated in this study is derived from a design developed by Kaiser Engineers for the Basalt Waste Isolation Program. The design by Kaiser Engineers encompassed all of the facilities required on the earth's surface to service the deep geologic repository. For this study, those facilities not required to serve MRS/IS functions are eliminated, and the storage fields and transuranic (TRU) warehouse are added. The resulting reference MRS/IS facility design has an estimated capital cost of \$178 million in mid-1982 dollars. Included in this base cost are: the waste handling facility (WHF); the initial storage field for metal casks with 100 storage pads; the initial warehouse building for storing contact-handled TRU (CHTRU) wastes; and the necessary support facilities as described in Subsection 4.3 of this report. The metal casks or drywells used for storing spent fuel and high-level wastes (HLW) and the concrete casks used for storing remote-handled TRU (RHTRU) wastes are purchased as required throughout the operational life of the facility.

The results of the analyses for the three principal scenarios are presented and discussed in Subsection 6.1. The advantages and disadvantages of co-locating an MRS/IS facility with a repository are discussed in Subsection 6.2, and recommendations derived from consideration of the analyses results and the advantages and disadvantages are presented in Subsection 6.3.

6.1 RESULTS OF STUDY ANALYSES

The components of the life cycle cost (undiscounted) for each of the three scenarios and for two storage devices (metal casks, drywells) are presented in Table 6.1, together with the percentages of total cost that each component represents. These percentages, illustrated in Figure 6.1, indicate the relative importance of each cost component, and suggest which of the cost components might be most useful to examine in search of cost reductions.

	Structures	Casks/ Drywell	Concrete Casks	Pads/ Fields	<u>Operations</u>	Transportation	Total
Reference							
<u>Scenario</u>				4 50			744 44
Metal Casks	1/8.0	306.250	42.25	4.58	200.24		/31.32
Percent	24.3	41.9	5.8	0.6	27.4		100.0
Drvwells	180.0	90.0	42.25	4.98	200.24		517.97
Percent	34.8	17.4	8.2	1.0	38.7		100.0
Delaved							
Reprocessing							
Metal Casks	175.5	674.625		1.36	212.240	1193.139	2256.864
Percent	7.8	29.9		0.1	9.4	52.9	100.0
Drvwells	175.0	297.000		5.1	302.354	1233.612	2013.066
Percent	8.7	14.8		0.3	15.0	61.3	100.0
Delaved							
Disposal							
Metal Casks	188.0	1767.5	243.35	26.91	261.54		2486.860
Percent	7.6	71.1	9.8	1.1	10.5		100.0
Drvwells	189.5	509.4	243.35	31.17	261.54		1234.96
Percent	15.3	41.2	19.7	2.5	21.2		100.0

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TABLE 6.1.	Components of Life Cycle Costs, Percentages and Tot	tals
	(millions of mid-1982 dollars, undiscounted)	



6.1.1 Comparison of Metal Storage Casks with Drywells

The total life cycle costs for each of the alternatives considered in this analysis are summarized in Table 6.2. The cost reduction obtained by utilizing drywells for storage of spent fuel and HLW canisters ranges from \$213 million to over \$1.25 billion. While many more drywells than metal casks are needed to store the same quantity of material, the greatly reduced capital cost of the reference drywell as compared with the reference metal cask (\$18,000 versus \$875,000) makes the drywell a reasonably attractive alternative for locations suitable for drywell installation.

Possible disadvantages of drywells compared with storage casks are the much larger land surface area needed, the greater difficulty of decontamination and removal from the ground, and the perception of permanence that is engendered by the emplacement of the well assembly into the ground. Another disadvantage of drywells relative to metal casks is that the drywells can only be used for storage at the installed location while the metal casks can be transported to other locations for use, if appropriate.

<u>TABLE 6.2</u>. Undiscounted and Discounted Life Cycle Costs for the Scenarios and Storage Alternatives Studied (billions of mid-1982 dollars)

	Reference	Delayed	Delayed
	Scenario	Reprocessing	Disposal
Undiscounted Cost:			
Metal Casks Drywells Casks> Drywells	0.731 0.518	2.257 1.973	2.487 1.235
Δ Cost	-0.213	-0.284	-1.252
% Change	-29.1	-12.6	-50.3
Discounted Cost:			
Metal Casks	0.578	1.592	1.661
Drywells	0.412	1.376	0.868
Casks→ Drywells	-0.166	-0.215	-0.793
	-28.7	-13.6	-47.7

6.1.2 Possibilities for Cost Reduction

It is instructive to review Figure 6.1 to select components of cost that should be examined for possible cost reductions. Since transportation of radioactive materials to and from the MRS/IS facility comprises from about 54 to 61 percent of the total life cycle cost of the system for the Delayed Reprocessing Scenario, transportation is a logical cost component to consider first.

Two alternatives to reduce the cost of transportation for the MRS/IS system are considered. These are: 1) consolidation of spent fuel bundles at the source site before shipment, thus reducing the number of shipments by a factor of 2, and 2) utilization of the large metal storage cask to ship spent fuel and solidified HLW from the source site to the MRS/IS facility, thus reducing the number of shipments by a large factor. These alternatives are discussed in the following subsections.

6.1.2.1 Consolidation of Spent Fuel Assemblies

Consolidating spent fuel assemblies into closely packed arrays within containers results in packing the equivalent of two assemblies into the space formerly occupied by one assembly. Three cost components are affected by consolidation: transportation, storage containers, and storage pads. The number of spent fuel shipments is reduced by half, as is the number of metal casks or drywells required to store the spent fuel. The estimated values for these cost components with the fuel assemblies unconsolidated and consolidated are given in Table 6.3, where it is seen that the possible cost reduction resulting from fuel consolidation is about \$934 million, or over 41 percent of the life cycle cost for the Delayed Reprocessing scenario.

6.1.2.2 Shipment in Large Metal Storage Casks

The spent fuel and HLW canisters are assumed to be shipped 50 percent by volume by truck and 50 percent by volume by rail. If it were possible to license the reference metal storage cask for shipment of spent fuel and HLW canisters, the number of shipments could be greatly reduced. While incremental transportation cost is a contributor to the MRS/IS facility life cycle cost

TABLE 6.3.	Effect of Fuel Assembly, Consolidation on MRS/IS	
	System Life Cycle Costs ^(a,D)	

Cost Component	Delayed Reprocessing
Unconsolidated:	
Transportation (Incremental)	1193.139
Metal Casks	674.625
Pads/Fields Total	$\frac{1.360}{1869.124}$
Consolidated:	934.562
Reduction in Total Life Cycle Cost	
Δ Cost	934.562
% Reduction	41.4

(a) Millions of mid-1982 dollars, undiscounted.

(b) The number of significant figures is for computational accuracy and does not imply precision to the nearest \$1000.

only for the Delayed Reprocessing scenario, transportation is a major factor in overall waste management system costs. The effect on total waste management system cost of using the reference storage cask for shipment is illustrated in Table 6.4.

The possible waste management cost reductions resulting from utilization of the reference metal storage cask for shipment of spent fuel and HLW canisters range from \$259 million to over \$1.2 billion, depending upon the scenario.

6.1.2.3 Combined Effect of Fuel Consolidation and Storage Cask Transport

It is useful to examine the total reductions in waste management costs that can be obtained by utilizing both fuel consolidation and storage cask transport.

The combined effect of fuel consolidation and use of metal storage casks for transport and storage of spent fuel and HLW canisters is shown in Table 6.5.
TABLE 6.4.	Effect of	Shipment	in Metal,	Storage	Casks	on	Waste
	Management	: System (Costs(a,b)				

Cost Component	Reference Scenario	Delayed Reprocessing	Delayed Disposal
Transport in Standard Casks: Spent Fuel HLW	291.875	1312.600	1283.630
Transport in Storage Casks:		E0.052	
Spent Fuel HLW	27.171		156.813
Reduction in Waste Management Cost	264.704	1252.747	1126.817

(a) Millions of mid-1982 dollars, undiscounted.

(b) The number of significant figures is for computational accuracy and does not imply precision to the nearest \$1000.

 $\frac{\text{TABLE 6.5.}}{\text{Storage Casks on Waste Management System Costs}} (a,b)$

Cost Component	Reference Scenario	Delayed Reprocessing	Delayed Disposal
Transport in Standard Casks Unconsolidated: Spent Fuel HLW Storage (Spent Fuel) Total	291.875 291.875	1312.600 	1283.630 1283.630
Transport in Storage Casks Consolidated: Spent Fuel HLW Storage (Spent Fuel) Total	27.171 27.171	29.927 <u></u> <u>337.993</u> 367.920	156.813 156.813
Reduction in Waste Management Cost	264.704	1620.665	1126.817

(a) Millions of mid-1982 dollars, undiscounted.

⁽b) The number of significant figures is for computational accuracy and does not imply precision to the nearest \$1000.

As shown in Table 6.5, the possible waste management cost reductions resulting from the combination of fuel consolidation and storage cask shipment range from about \$265 million to over \$1.6 billion, depending upon the scenario.

6.2 ADVANTAGES AND DISADVANTAGES OF CO-LOCATION

The principal advantage of co-locating a storage facility with a geologic repository is that the structures and services installed for the storage facility become the surface facilities for the repository when the repository is placed in operation. Duplication of facilities is avoided, thus reducing the total capital investment in facilities for the waste management system by nearly \$200 million, as compared with equivalent facilities located separately.

Another related advantage is that the surface facilities remain in useful service over the combined lifetimes of the storage facility <u>and</u> the repository. The capital investment in facilities can be amortized over a period of more than 40 years rather than the 15 to 20 years appropriate for just the storage facility, thus reducing the cost to electricity customers due to waste management.

Since transport of the radioactive materials through the waste management system is the principal component of the system cost, it is desirable to minimize the length and number of shipments that must be made. The advantage or disadvantage of an MRS/IS/Repository facility for reducing transport costs depends largely on the scenario that is considered. In a situation like the Delayed Reprocessing scenario, where spent fuel assemblies are first shipped to the storage facility and stored, then to the reprocessing plant for reprocessing, and finally to a repository for disposal, the MRS/IS/Repository is a definite disadvantage since it would tend to maximize transportation costs. On the other hand, if the reprocessing plant is placed in operation early enough to avoid any interim storage of spent fuel, the MRS/IS/Repository will receive only solidified HLW and TRU wastes for eventual emplacement in the repository, and transport costs will be minimized.

Another advantage of the MRS/IS/Repository is that the stored material can be transferred directly from storage to the repository, using the same transporter equipment as was used to place the material in storage initially. No shipments beyond the site boundary would be required, minimizing the potential for transportation accidents and the possible exposure of the public resulting from such accidents.

6.3 RECOMMENDATIONS

Because transportation of the radioactive materials to the storage site is the largest component of the system life cycle cost, those actions that will reduce transport costs should be implemented to the extent possible. The action to be taken first should be the consolidation of all spent fuel assemblies prior to shipment from the source site(s). For compatibility with the internal structures of shipping and storage casks, the consolidated rods must be contained in canisters whose dimensions match those of an intact fuel assembly. Consolidation of fuel assemblies for storage has been demonstrated on an experimental basis in reactor fuel pools. Scaling these efforts up for production-level consolidation is within the present state-of-the-art, and should be a licensed process in the near future.

The next immediate beneficial action should be the licensing of the large storage casks for shipment when filled with spent fuel or HLW canisters. Should licensing be accomplished before any shipments are made to the storage facility, most of the structures at the facility would be unnecessary, since the radioactive material would be sealed in the storage cask at the source site. All that would be required at the storage site would be the capability to remove the cask from its rail car and to place the cask on its storage pad. The shielded handling facility would not be required until the repository is opened and the materials sealed in casks are removed for emplacement in the repository.

The use of the reference metal storage casks is a very costly approach for storing the large quantities of material postulated in the three principal scenarios. In the Delayed Disposal scenario, 2020 casks are needed, at a

cost of nearly \$1.8 billion. The use of the reference drywells in the same scenario would cost just over \$0.5 billion. On a cost-effectiveness basis, the drywells should be the preferred choice.

Another consideration is the availability of the raw materials needed to fabricate the casks or drywells. About 50 tons of lead is used in each of the reference metal casks, or a total of about 100,000 tons for the Delayed Disposal scenario. Slightly smaller quantities of stainless steel would be required. The drywells would require essentially no lead and greatly reduced quantities of stainless steel, another factor favoring the drywell concept.

A recent analysis by Kaiser Engineers has suggested that water pool storage for spent fuel is about equivalent in cost to drywell storage. While not analyzed in this study, in view of the massive quantities of material that would be stored under the Delayed Disposal scenario, a water pool storage facility may be the most cost-effective approach. A detailed analysis of a water pool facility should be made before embarking on the establishment of a cask or drywell facility.

7.0 <u>SENSITIVITY OF ESTIMATED COSTS TO VARIATIONS</u> IN CONCEPTS AND ASSUMPTIONS

The scope of this study is limited to dry storage concepts: metal casks, and drywells. The prior assumption is made, perhaps erroneously, that either of the dry storage concepts can be developed and utilized for a monitored retrievable storage/interim storage (MRS/IS) facility on a more cost-effective basis than can the fully-developed and demonstrated water pool storage concept.

The principal components of cost are listed in Table 7.1 for the three scenarios considered. Also shown in the table are the percent changes in life cycle costs that are estimated to result from using a different storage device (drywell instead of metal cask), from consolidating the spent fuel assemblies at the source site(s) prior to shipment, and from shipping the radioactive materials to the storage facility in the large metal storage casks.

As might be expected, the Delayed Reprocessing and Delayed Disposal scenarios are more costly than the Reference scenario by about a factor of 3. This result suggests that placing the reprocessing plants and the repositories in operation at the earliest possible time would also minimize the life cycle cost for the MRS/IS facility.

The major component of cost for the delayed reprocessing scenario (~54 percent) is the transporting of the spent fuel to and/or from the MRS/IS facility. Since the total waste management system cost for each of the three scenarios evaluated is very sensitive to transportation costs, ways and means to reduce transportation costs should be developed and applied in the selected waste processing system. For example, if incorporated into the commercial nuclear waste system, the concept of consolidating fuel assemblies at the reactor sites would not only reduce the transport costs but would also reduce the capital and operating costs of the MRS/IS facility. As shown in Table 7.1, fuel consolidation is estimated to produce a net reduction in MRS/IS facility costs of 41.4 percent for the Delayed Reprocessing scenario. This total includes possible reductions in transportation charges, purchase of fewer storage casks and construction of fewer storage cask pads and fields.

		Scenario	
	Reference	Delayed Reprocessing	Delayed Disposal
Total Undiscounted Cost (\$ Billions)	0.731	2.257	2.487
Total Cost Breakdown (by %)			
Structures Metal Cask Concrete Cask Pads/fields Operations Shipping (Incremental)	24.3 41.9 5.8 0.6 27.4 0.0	7.8 29.9 0.1 9.4 52.9	7.6 71.1 9.8 1.1 10.5 0.0
Fuel Consolidation at Reactor Sites (% change)		-41.4	
Ship in Storage Cask (% change)	-36.2	-50.2	-45.3
Fuel Consolidation and Shipment in Storage Casks (% change)	-36.2	-66.5	-45.3
Drywells in lieu of Casks (% change)	-29.1	-12.6	-50.3

TABLE 7.1. Estimated Life Cycle Costs and Possible Variations

This approach would also lessen the demands on items such as stainless steel, lead, boron steel and other scarce and expensive materials.

Another concept that, if developed and used in the commercial nuclear waste storage system, would also reduce costs is the use of a common cask for both shipment and storage. The reduction of 50.5 percent for the Delayed Reprocessing scenario (as shown in Table 7.1) represents savings due to the reduction in the number of cask shipments required.

If both fuel consolidation and shipment using large metal storage casks were implemented, estimated cost reductions of 36.2, 66.5, and 45.3 percent for the Reference, Delayed Reprocessing, and Delayed Disposal scenarios, respectively, could be realized.

The potential cost reductions, if drywells were used for the storage of spent fuel and HLW instead of surface casks, are significant for each of the three scenarios, as shown in Table 7.1. Although the use of drywells is not analyzed in depth in this study, it is felt that their use would result in considerable reduction in the demands on stainless steel, lead, and other gamma-shielding materials.

Since the majority of the structures that make up the MRS/IS facility co-located with a repository can and will also serve as the basic surface facility for the repository, the overall costs to the commercial nuclear waste system can be reduced by using the co-located facilities. As shown in Table 4.7, the capital cost of the MRS/IS facility is about \$180 million. If separate MRS/IS facilities and repository surface facilities were to be built, the combined facility cost would approximately double.

In addition to reduced capital costs, the operating and decommissioning costs for a co-located facility would also be less than the associated costs for an MRS/IS facility and a repository that are separated.

As noted previously, the scope of this study does not include the "wet" storage concept. However, considering the need to provide a relatively large storage capacity in the very near time frame that would be required to operate for about 20 to 30 years, it appears that water pool storage is an option worthy of further consideration. It definitely would be one that would not require such large quantities of stainless steel, lead, and other scarce or expensive shielding materials.

One of the basic ground rules of this study is that only one MRS/IS facility would be built for the system required to handle and store nuclear wastes from commercial reactors. However, based on the magnitude of the transport requirements and costs as compared to facility costs for all of the scenarios studied, it may be prudent and cost-effective to use two MRS/IS facilities in the commercial waste system. While this concept has not been evaluated in any depth, it appears that the most cost-effective system may be one with an MRS/IS facility at both the reprocessing plant and at the site of the first repository.

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8.0 TECHNICAL STATUS/RESEARCH AND DEVELOPMENT REQUIREMENTS

The methods and systems to be used at a monitored retrievable storage/interim storage (MRS/IS) facility are, for the most part, well within the state-of-the-art and most have either been used or demonstrated at various facilities in the United States or abroad. The status of the principal components and areas needing further research and development are discussed in this section.

8.1 RECEIVING AND HANDLING

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A considerable amount of experience has been gained in the use of rail and truck casks, both wet and dry, for the transportation of irradiated fuel elements in the United States.

Shipping cask unloading and fuel handling storage have been routinely performed at two reprocessing plants and in the spent fuel storage basin at commercial LWRs for a number of years. Dry receiving, unloading and storage have been considered and proposed in a number of different types of facilities ranging from reprocessing plants to repositories; they have been performed at the Nevada Test Site (NTS) in support of both the Spent Fuel Dry Surface Storage Program conducted by ONWI at the E-MAD facility and the disposal demonstration program conducted by the Lawrence Livermore Laboratory at the CLIMAX facility.

Transporter/emplacement systems for use with both casks and drywells of equivalent weight and configuration being considered for the MRS/IS facility have been demonstrated at E-MAD as part of the Spent Fuel Surface Storage Program.

8.2 STORAGE

Drywell development programs and projects at NTS, Hanford and the Idaho National Engineering Laboratory (INEL) have all provided experience with procedures and equipment, heat transfer data in soil and confirmation of the feasibility of the method.

The use of drywells has been demonstrated at NTS/E-MAD as part of the Spent Fuel Surface Storage Program. Drywells have been used to store HTGR and LMFBR fuels at INEL for over ten years.

Surface storage casks have also been demonstrated at NTS under the Spent Fuel Surface Storage Program. In addition, large surface storage casks have been used for spent fuel storage and for storage demonstrations in both Canada and West Germany.

Required storage monitoring such as gas sampling and measuring, and temperature measuring systems are all well developed and can be applied to either storage concept.

8.3 RESEARCH AND DEVELOPMENT REQUIREMENTS

As noted above, the general systems and components required at an MRS/IS facility have been developed and demonstrated. It is anticipated that the R&D requirements will essentially be the same for all MRS/IS facilities no matter where they are located. An exception for the MRS/IS/Repository is that geological, hydrological and geotechnical exploration and data evaluation will be required to assure the facility is located on an acceptable and viable geologic repository site.

The need to achieve a relatively high facility throughput and capacity will require additional development and improvements to some of the present systems and methods. Specific devices for monitoring and safeguard applications will need to be developed and refined. Additional R&D efforts will be required to develop:

- licensed truck and rail casks designed for dry mode transfers of contents
- licensed shippable storage casks
- efficient licensed TRU waste containers and shipping casks
- standardized and licensed waste containers.

Development and testing will be required to:

- confirm the heat rejection capabilities of large surface storage casks
- establish drywell heat transfer parameters for site-specific environments
- establish large surface storage cask heat transfer parameters for site-specific environments.

Development and prototype testing should be conducted on:

- grapples to handle canisters and waste packages
- automated cask decontamination station
- remotely operated contamination detection equipment
- container leak testing systems.

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APPENDIX A

CONSIDERATIONS FOR MRS/IS COST EVALUATION

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APPENDIX A

CONSIDERATIONS FOR MRS/IS COST EVALUATION

The MRS/IS facility is conceived as a government-owned facility for providing temporary storage capability for spent fuel and/or reprocessing wastes while reprocessing capability and repositories for geologic disposal are introduced.

To provide compatibility with other studies performed in evaluation of spent fuel and waste disposal, all costs should be presented in terms of constant-value, mid-1982 dollars (without cost escalation or inflation). All costs from the present to the final year of decommissioning are to be entered into a cash flow table (Table A.1) and presented both as undiscounted costs and as discounted at 2 percent per year. The annual costs should be summed over all years included, to provide undiscounted program costs and the present worth costs at 2 percent discount. The discounted (present worth) costs will be used in comparing alternatives.

To ensure that all alternatives are equitably treated during comparisons, the details of component costs, background, and cost bases must be presented in support of the costs given in Table A.1. Tables A.2 through A.7 are provided for this purpose. These tables in turn should be supported by the cost schedules indicating the cost bases or components for each category in the tables. Typical cost categories are outlined in Attachment 1, following these tables. Insofar as possible, cost breakdowns by these categories should be provided. If other cost bases are used, these should be detailed.

Table A.2 summarizes the capital construction costs for the first module of the MRS/IS; costs for additional modules should be entered on Table A.6 (in multiple copies if needed). Costs for each module should be prorated into the appropriate years, using Table A.3, and the prorated annual costs should then be included in the cash flow summary of Table A.1.

Owner's costs are defined separately for three periods: those costs incurred during the construction period (Table A.5), annual operating costs for the facility (Table A.6), and decommissioning costs (Table A.7). The costs summarized on Tables A.5 and A.7 should, as before, be prorated into the appropriate years using Table A.3.

A.1

			Costs, \$1	000's	
Year	Discount _Factor_	Capital	<u>Operating</u>	Total	Discounted Total
1982	1.000				
1983	0.9804				
1984	0.9612				
1985	0.9423				
1986	0.9238				
1987	0.9057				
1 9 88	0.8880				
1989	0.8706				
1990	0.8535				
1991	0.8368				
1992	0.8203				
1993	0.8043				
1994	0.7885				
1995	0.7730				
1996	0.7579				
1997	0.7430				
1998	0.7284				
1999	0.7142				
2000	0.7002				
2001	0.6864				
2002	0.6730				
2003	0.6598				
2004	0.6468				
2005	0.6342				

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TABLE A.1. Cash Flow and Present Worth for

			Costs, \$1	L000's	
Vear	Discount	Canital	Operating	Total	Discounted
1001	1 40 001		operating	10001	
2006	0.6217				
2007	0.6095				
2008	0.5976				
2009	0.5859				
2010	0.5744				
2011	0.5631				
2012	0.5521				
2013	0.5412				
2014	0.5306				
2015	0.5202				
2016	0.5100				
2017	0.5000				
2018	0.4912				
2019	0.4806				
2020	0.4712				
2021	0.4619				
2022	0.4529				
2023	0.4440				
2024	0.4353				
2025	0.4268				
2026	0.4184				
2027	0.4102				
2028	0.4022				
2029	0.3943				
2030	0.3865				

TABLE A.1. (contd)

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TABLE A.2.	First Module	Capital Cost	Estimate for
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Cost Element	Manhours, 1000 Non-Manual Man	's Co ual Labor	sts, \$1000 Material	's Total
Site and improvments				
Receiving facility				
Canning facility				
Drywells or casks				
Balance of storage facility				
Other buildings				
Canning equipment				
Transporter				
Other engineered equipment				
Total directs				
Indirects				
A-E services				
Contingency				
TOTAL				

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Α.3.	Cost Distribution for	
	(from Tables B.20, B.22 and B.25	

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Year Distribution Fraction Annual Cost

	Manhoung 10001c	Costs \$10001c
Cost Element	Non-Manual Manual	Labor Material Total
Site preparation		
Drywells or casks		
Balance of storage facility		
Total directs		
Indirects		
A-E services		
Contingency		
TOTAL		

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TABLE A.4. Estimate of Additional Module Capital Cost for _____

Cost Element	Manhours or Other Basis	<u>Cost</u>
Hearing preparation and testimony		
Contract management		
Inspection and QA		
Training program		
Security		
General and Administrative		
TOTAL		

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TABLE A.5. Estimate of Owner's Costs During Construction for _____

Cost Element	Manhours or Other Basis	<u>Cost</u>
Supplies		
Capital replacement allowand	ce	
Cans and lids		
Security		
Maintenance		
Receiving and shipping		
Hot cell (canning, etc.)		
Placement or removal		
Surveillance		
Outside support services		
Subtotal		
General and Administrative		•
Utility costs		
Other		
TOTAL ANNUAL COST		

TABLE A.6. Estimate of Owner's Annual Operating Costs During

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Cost Element	Manhours or Other Basis	<u>Cost</u>
Casks or drywells		
Engineered equipment		
Buildings		
Site restoration		
Supplies (decontamination, cutting, packaging)		
Security		
Shipping and burial fees		
Subtotal		
General and administrative		
Utilities		
Other		
TOTAL		

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TABLE A.7. Estimate of Owner's Costs During Decommissioning for

Table A.6 should be used for estimates of annual operating costs. Normally one table will be required for each year of operation. However, if operating costs are identical for successive years, a single table may be used with the notation in the heading as to the years the table applies to. Again, the total cost for each year should be included in the cash flow summary of Table A.1. Transportation-related expenses inside the facility fence (except transportation equipment lease or use fees) are to be estimated and included in annual operating expenses.

Cost Bases

Bases for estimates should be given in all instances. Design and construction costs are generally influenced by physical conditions at a site. Attachment 2 lists the pertinent conditions that should be described as part of this cost basis. Attachment 3 provides guidelines for social and economic factors that need to be considered and described in the bases. These procedures, should be followed, are based upon work initially done for PNL by Bechtel Corporation during preparation of DOE/ET-0028 (<u>Technology for</u> Commercial Waste Management).

A contingency of 25 percent should be used in defining construction costs.

If the design does not require a facility or an operation given in a table, a cost of zero may be entered. The detail in the tables is not intended to dictate design, only to permit normalization.

A.10

ATTACHMENT 1: OUTLINE OF COST CATEGORIES

- A. Possible capital expenses at MRS/IS
 - Reports and testimony for site approval, cost of permits and licenses
 - 2. Design engineering
 - Site preparation, access control, abatement of impacts on air and water quality
 - 4. Buildings
 - a) Receiving facility including holding areas for incoming and outgoing casks
 - b) Canning facility, transfer facility
 - c) Storage facility including drywells or casks
 - d) Administration auxiliary, etc.
 - 5. Engineered equipment
 - a) Cranes
 - b) Canning equipment
 - c) Decontamination and waste treatment equipment
 - d) Ventilation and contamination control
 - e) Spare parts inventory
 - f) Transporter for 100 ton cask or shielded transporter for cans
 - 6. Contractor indirects (percent of 4, 5 and 6)
 - 7. Construction management and inspection
 - 8. Licensing and safety reports
 - 9. Contingency

- B. Owner's costs for MRS/IS
 - Payroll for personnel at hearings and for preparation of presentation and testimony
 - 2. Contract management
 - a) Engineering
 - b) Licensing consultants
 - c) Construction contractor
 - 3. Inspection and quality assurance
 - 4. Operating supplies
 - a) Decontamination chemicals, wipes, protective clothing, dosimeters, etc.
 - b) Filter aids, demineralizers, regeneration chemicals
 - c) Annual capital replacement as used from spare parts inventory
 - d) Cans and lids
 - 5. Payroll for personnel to:
 - a) Operate training program
 - b) Guard plant and storage yard
 - Maintain cranes, decontamination equipment, waste treatment equipment, heating and ventilating equipment, and transporter
 - Receive, prepare, inspect, survey, cool, flush, and decontaminate shipping casks, storage casks, and/or shielded transporter
 - e) Move shipping cask and storage cask into hot cell and open them
 - f) Bring fuel, fuel can, hardware can and lids to work station

- g) Disassemble fuel and place fuel pins in fuel cans and hardware in hardware cans
- When cans are full, seal, test seal, decontaminate exterior and survey
- Place completed cans in a cask, shielded transporter or lag storage
- j) Mark each can and record the contents and location
- Move fuel assemblies from shipping cask to storage cask or transporter or cans from storage to the storage cask or transporter
- Close, inspect, survey and decontaminate a cask or shielded transporter
- m) Reassemble and ship the shipping cask
- Remove the storage cask from the hot cell and place in the storage yard
- Remove the shielded transporter from the hot cell, place the fuel or can in a drywell, seal the drywell, test the seal, survey, and decontaminate.
- 6. Maintenance and operating supplies for the storage period.
- 7. Payroll during storage period
 - a) Guards

- Maintenance to keep plant in standby and counteract weathering of casks or drywells
- c) Leak test casks or drywells and repair as necessary
- 8. Maintenance and operating supplies for removal
 - a) Decontamination chemicals, wipes, etc.
 - b) Filter aids, demineralizer regeneration chemicals
 - c) Capital replacements as used from spare parts inventory.

- 9. Payroll during removal for personnel to:
 - a) Guard plant and storage yard
 - b) Maintain cranes, decontamination equipment, waste treatment equipment, heating ventilating equipment and transporter
 - c) Receive, prepare, inspect, survey, cool, flush and decontaminate storage casks, shipping casks, and/or shielded transporter
 - d) Move storage cask or fuel from shielded transporter and shipping cask into hot cell and open casks
 - e) Move fuel assembly or can into shipping cask
 - f) Record location of all fuel moved
 - g) Close, inspect, survey and decontaminate casks and/or transporter
 - h) Prepare and ship the shipping cask to reprocessing or disposal (if storage cask becomes licensed for shipping, this step may replace many of the above steps)
- Pay premium or receive credit for condition of fuel relative to normal uncanned assemblies based upon impact on reprocessing or disposal.
- 11. Decommission facility
 - a) Survey, decontaminate and sell for scrap, send to shallowland burial or disposal the storage casks or drywells
 - Decontaminate, disassemble, and sell for scrap or package and ship for shallow burial or disposal all engineered equipment
 - c) Convert to other use or demolish and sell for scrap or send to shallow burial or disposal all buildings and storage structures
 - d) Prepare land for conversion to other uses.

- 12. Shipping and burial fees for decontamination wastes generated during fuel placement, storage, and removal, and during decommissioning.
- 13. General and overhead expenses (as a percentage of 4 through 12)
- 14. Contracted services.
- 15. Fuel and utilities.

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ATTACHMENT 2: DESIGN AND CONSTRUCTION BASES

Please describe the following items in your basis.

- 1. Site Location
- 2. Meterological Conditions
 - 2.1 Wind conditions as indicated below:
 - Maximum velocity
 - Average velocity
 - Design velocity (basic wind speed)
 - Design pressure.
 - 2.2 Tornado
 - 2.3 Tornado Missiles
 - 2.4 Rainfall (Precipitation)
 - Annual average precipitation
 - Maximum precipitation
 - Design maximum rate (peak 1 hr rate 50 yr recurrence)
 - Design maximum duration.
 - 2.5 Snow
 - 2.6 Temperature design basis temperature conditions
 - Summer maximum (July)
 - Winter minimum (January)
 - Design maximum, summer
 - dry bulb
 - wet bulb
 - Design minimum, winter.

3. Surface Conditions

- 3.1 Obstructions
- 3.2 Topography
- 3.3 Vegetation
- 3.4 Drainage

3.5 Flooding

3.6 Roads

Approximate new road construction required to provide access to the site from an existing highway suitable for heavy transport.

3.7 Railroads

Approximate new railroad required to provide a rail spur service to the site.

3.8 Utilities

Will temporary facilities be required during construction, or are permanent facilities part of site preparation.

4. Subsurface Conditions

4.1 Obstructions

Are there any major underground obstructions to facility construction.

4.2 Soils - Thickness

4.3 Rock - Depth type and load bearing ability

4.4 Groundwater - Depth and need for dewatering

4.5 Frost – Design ground penetration

4.6 Cavities and Small Voids

Do they exist in the soils or rock underlying the site

5. <u>Geologic and Seismic Conditions</u>

- 5.1 Faults The nearest known or inferred fault
- 5.2 Seismic Design

ATTACHMENT 3: COST ESTIMATE BASES AND METHODS

1. Construction Conditions

As a basis for cost estimating, the construction conditions described below are assumed to prevail at all sites.

- 1.1 <u>Construction Labor</u> will follow a 40-hour, single-shift work week schedule except for casual overtime (e.g., to complete a concrete pour), and in instances where twoor three-shift concrete work operations are planned to meet the construction schedule.
- 1.2 <u>Severe Work Stoppages</u> such as extensive jurisdictional disputes between labor crafts will not occur during construction.
- 1.3 <u>Labor Availability</u> in each craft will be adequate so that importing labor, except for general foremen, will not be required.
- 1.4 <u>Craft Labor Wage Rates</u>, including fringe benefits are those prevailing in the geographic region of the construction site in mid-1982.

2. Pricing: Field Costs

The various elements comprising the field costs will be priced by the methods described below:

2.1 <u>Major Equipment Costs</u> will be determined using estimated prices of similar or nearly similar equipment from other cost estimates of fuel reprocessing plants, radioactive wastes disposal processes and other plants dealing with the nuclear fuel cycle.

2.2 <u>Bulk Materials</u>. Except for instances where enough information exists to warrant quantity assessments and unit pricing of certain specifically identified material, bulk materials costs will be determined either as a function of major equipment costs or as a cost allowance.

2.3 <u>Direct Labor Costs</u> will be evaluated from estimated manhours for erection and installation sequences and operations and craft wage rates and fringe benefits in effect at mid-1982. Labor manhours are representative of the craft production rates in the area of reference jobsites.

A.18

2.4 <u>Indirect Site Construction Costs</u> such as contractor's fee, supervision, construction equipment, tools and consumable supplies, temporary facilities and utilities, material handling, cleanup and the like will be combined and evaluated as a factor of the total direct labor.

3. Architect-Engineer (A-E) Services

The costs of A-E services will be estimated as a percentage of the total field costs and will include burden and fee.

4. Owner's Cost

Owner's costs during construction will be estimated in conjunction with the operating and maintenance costs.

5. Costs Not Included

Exclusions from the estimate are generally limited to the following particular cost classifications:

- Site acquisition costs
- Escalation of costs beyond mid-1982
- Process and patent royalties
- General research and development costs
- Costs incurred beyond those that reflect the current degree of involvement in securing approvals from regulatory agencies monitoring environmental and safety considerations
- Costs generated directly by any governing or regulatory agency for administration, engineering, procurement and construction
- Sales/use tax
- Local property tax or payments in lieu thereof
- Impact payments to local government
- Insurance or prorate cost of self insurance
- Nuclear hazards insurance that may be required if nuclear hazards exist on site before completion of project
- Housing for construction workers.

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APPENDIX B

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MRS/IS FUEL CYCLE AND WASTE SCENARIOS

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APPENDIX B

MRS/IS FUEL CYCLE AND WASTE SCENARIOS

Five MRS/IS scenarios are to be used by all MRS/IS projects. Each MRS/IS facility should be designed to satisfy the reference scenario, the delayed reprocessing scenario, and the delayed disposal scenario. The early disposal scenario and the delayed disposal-no reprocessing scenario are included for information only.

Basis for Projections

The bases and assumptions used in developing the projections are as follows:

- Maximum pool expansion at reactors is assumed based on utility estimates.
- Each pool maintains a full core reserve.
- Historic spent fuel inventory data are used as reported by utilities.
- Discharge projections used are as given by utilities.
- Generic reactors added beginning in 1996 have lifetime storage capability.
- TRU wastes are sent to disposal or storage the year after reprocessing.
- The maximum receiving rate for each repository for spent fuel or equivalent HLW is 1800 MTHM/yr the first five years and 3000 MTHM/yr for the next 21 years.
- The maximum TRU receiving rates are designed to be compatible with the HLW receiving rates and are about 15 percent greater than those rates in terms of equivalent MTHM.

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- Solidified HLW is sent to disposal or storage one year after reprocessing or 10 years after reactor discharge, whichever is later.
- Time from discharge is determined by youngest fuel in the mixture.
- Oldest fuel is shipped first to MRS/IS or reprocessing.
- Shipping the oldest fuel first is assumed to relieve the at-reactor storage problems.
- Spent fuel can be sent to disposal if the overflow from reactor basins is 10 years old and reprocessing is limited.
- The first two reprocessing plants have capacities of 1500 MTHM/yr and the next two have capacities of 3000 MTHM/yr.
- The fourth reprocessing plant is a replacement for the first plant, which is assumed to be retired after about 20 years service.
- Each reprocessing plant operates at 1/3 and 2/3 capacity in its first two years.
- Spent fuel requiring storage prior to 1990 is stored in casks at reactor sites or at government-owned emergency storage.

The startup dates for reprocessing plants and repositories which define the scenarios are summarized in Table B.1. MRS/IS activity concludes before 2025 for all except the delayed disposal scenario; a fourth repository is needed in the delayed disposal scenario to permit retiring the MRS/IS at a reasonable date.

Reprocessing Plant Waste Quantities

Reprocessing plant waste quantities are based on information provided by AGNS in a draft report.^(a) The projection is based on:

• Compaction of the hulls (after separation of hardware) and other compactible and noncombustible wastes

⁽a) W. H. Carr, Estimation of Nuclear Waste from the Barnwell Nuclear Fuel Plant, Allied-General Nuclear Services, April 26, 1982 (Draft).
TABLE B.1. Startup Dates for the Scenarios

Scenario	Reprocessing	Disposal				
Reference	1989, 2000, 2005, 2010	1998, 2002, 2015				
Delayed Reprocessing	1999, 2010, 2015, 2020	1998, 2002, 2015				
Delayed Disposal	1989, 2000, 2005, 2010	2008, 2012, 2015, 2025				
Early Disposal(a)	1989, 2000, 2005, 2010	1993, 1998, 2010				
Delayed Disposal(a) no Reprocessing		2008, 2012, 2015				

(a) Information only

- Incineration of combustible wastes with cement immobilization of the ash and incinerator scrubber solution
- Immobilization of UF₆ plant particulates with cement
- Volume reduction factors based on data developed for the GEIS on commercial radioactive waste (DOE/ET-0028)
- Use of a 2-ft diameter x 10-ft long canister for hulls and other canistered wastes (excluding HLW). This size is assumed to be more compatible with storage and shipping casks than the 4-ft diameter x 8-ft long canister.

The annual quantities of waste from the 1500 MT/yr AGNS plant are summarized in Table B.2 for the volume-reduced and immobilized wastes. Table B.2 also shows the number of HLW canisters, if a standard 1-ft diameter x 10-ft long canister is used. The TRU wastes are divided into five surface dose rate categories: 0.2, 0.2-5, 5-50, 50-500, and >500 R/hr. Waste containers with surface dose rates greater than 0.2 R/hr are identified here as remote handled TRU (RHTRU). Those less than 0.2 R/hr are identified as

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TABLE B.2.	Annual AGNS Plant	t HLW and TRU	Wastes with	Volume Reduction
	and Immobilizatio	on (per 1500	MTU)	

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Waste	ft ³ yr	Container	0.2 R/hr	0.2-5	<u>5–50</u>	<u>50–500</u>	>500 R/hr
HLW glass	4,900	1 ft D x 10 ft can					700
Hulls compacted	9,600	1 ft D x 10 ft can					340
Fuel hdwr.	3,900	2 ft D x 10 ft can					140
RHTRU	1,600	2 ft D x 10 ft can		40	7	4	
RHTRU	4,600	55 gal drums		614	76	8	
CHTRU	1,380	4 ft x 6 ft x 6 ft Stl. boxes	25				
CHTRU	19,560	55 gal drums	3,293				
Mox Plant							
CHTRU	10,400	55 gal drums	1,575				
CHTRU	2,000	4 ft x 6 ft x 6 ft Stl. boxes	15				

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contact handled (CHTRU). The AGNS data included a category 0.05 to 0.5 R/hr. For this analysis one-half the waste in that category is assumed to have a surface dose rate of less than 0.2 R/hr and, therefore, to be CHTRU. The remainder is assumed to be greater than 0.2 R/hr and, therefore, to be RHTRU.

Scenario Projection

The reference scenario is summarized in Table B.3. All numbers on this table are expressed as metric tons of spent fuel or metric tons equivalent of HLW (i.e., metric tons of spent fuel reprocessed to produce the HLW). To convert from MTHM to fuel assemblies or HLW canisters, divide the listed MTHM values by 0.18 MTHM/BWR, 0.42 MTHM/PWR, 2.143 MTHM/Canister. Column headings can be defined as follows:

<u>Column</u>	Label	Definition
2	Discharge	MT spent fuel discharged per year
3	AR Inv.	At-reactor spent fuel storage inventories, MT
4	MRS Inv.	Spent fuel inventory at the MRS/IS, MT
4	MRS Inv.	Spent fuel inventory at the MRS/IS, MT
5	Reprocess	Reprocessing rate, MT/yr
6	Disposal	Spent fuel shipped to disposal, MT/yr
7	Disposal Inv.	Spent fuel inventory in reposi- tories, MT
8	HLW AR	HLW stored at reprocessing plant, MT equivalent
9	HLW MRS	HLW stored at MRS/IS, MT equivalent
10	Disposal	HLW sent to disposal, MT/yr
11	Disposal Inv.	HLW inventories in repositories, MT equivalent

YEAR	UISCHARGE	AR INV	MRS INV	REPROCESS	DISPOSAL	DISP INV	HLW A R	HLW MRS	DISPOSAL	DISP INV
1981	1090.	7871.	0.	U.	υ.	0.	0.	0.	0.	0.
1982	1237.	9108.	0.	Ú.	0.	0.	0.	0.	0.	0.
1983	1607.	10715.	0.	υ,	0.	0.	0.	0.	0.	0.
1984	1744.	12447.	13.	Ű.	0.	0.	0.	0.	٥.	0.
1985	2167.	14614.	13.	0.	υ.	0.	0.	0.	0.	0.
	•	-								
1986	2610.	17121.	116.	0.	Ο.	0.	0.	· 0.	0.	0.
1987	2622.	19567.	292.	υ.	Û.	0.	Û.	0.	0.	0.
1988	2866.	22196.	530.	U.	Ο.	0.	0.	0.	0.	0.
1989	3223.	24945.	503.	500.	υ.	0.	500.	0.	0.	0.
1990	3071.	27507.	12.	1000.	0.	0.	1000.	500.	0.	0.
	7.6.74		•	1500	0	•	1500	1600	٥	•
1991	3070.	67471.	U .	1500.	U.	0.	1500.	3000		
1992	3440	21042	0.	1500.	0.	0.	1500.	4500		0.
1993	3420.	34013	U.	1200	U •	0.	1500.	4000 ·	0	0
1994	3387.	34912.		1500.	V •	0.	1500.	7500	ů.	0
1942	3574.	70490*	U.	1200.	۷.	v.	1200.	1000	••	· •
1996	3470.	38956.	0.	1500.	0.	0.	1500.	9000.	0.	0.
1997	3498.	40954	0.	1500.	Ο.	0.	1500.	10500.	0.	0.
1998	3874.	4332H.	0.	1500.	0,	0.	1500.	10200.	.1800.	1800.
1999	3860.	45688.	Q.	1500.	0	0.	1500.	9900.	1800.	3600.
2000	3964.	47652.	0.	2000.	υ.	0.	2000.	9600.	1800.	5400.
	4 19 4 1 4				0	•	35.0.0	0400	1900	7200
2001	4380.	49538.	0.	2500.	U.	0.	2000.	9000	1000	10800
2002	4407.	50945.	0.	3000.	.	0.	3000.	6700.	3000.	10000.
2003	4567.	52515.	0.	3000.	U.	U.	3000.	6700.	4000.	10000.
2004	4919.	54434.	0.	3000.		0.	3000.	3300	4800.	20400.
2005	4841.	55214.	υ.	4000.	υ.	υ.	4000.	3300.	4000.	23200.
2006	5220.	55500.	0.	5000.	0.	0.	5000.	2500.	4800.	30000.
2007	6081.	55581	0.	6000.	υ.	0.	6000.	1500.	6000.	36000.
2008	6043.	55625.	0.	6000.	υ.	0.	6000.	1500.	6000.	42000.
2009	6537	56161.	0.	6000.	0.	0.	6000.	1500.	6000.	48000.
2010	6251.	554121	0.	7000.	0.	0.	7000.	1500.	6000.	54000.
3411	1330	55140	~		Δ	•	6500	2500	6000	60000
2011	0200.	55140.	9.	2500.	v.	U .	7500.	2000	6000	66000
2912	0301.	54022.	· · ·	7500.	U.	U .	10500.	2700	4800	70800
2013	6485.	23000.	0.	7500.	u .	U .	10500.	2700.	4000	76800.
2014	6121.	52233.	0.	/500.	U .	υ.	10500.	4200.	6000.	00000
2015	/033.	51767.	0.	/500.	0.	0.	12000*	480.	0120.	83520.
2016	6670-	50957.	0.	7500.	0.	0.	18000.	0.	4980.	88500.
2017	6869.	50326	0.	7500.	ů.	0.	18000.	0	7500.	96000.
2018	7258	50084.	0 -	7500	0	0.	18000.	0.	7500.	103500.
2019	6642	49276.	0-	1500.	Ű.	0.	22500.	0.	3000.	106500.
2020	7040.	48822.	0.	7500.	0.	0.	22500.	0.	7500.	114000.

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TABLE B.3. Reference Scenario Summary (Reference Case June 21, 1982)

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The 13 tons in MRS/IS before 1986 come from Surry-2. It is possible the ulitity will find another solution to its storage problem. Columns six and seven are provided for spent fuel disposal in other scenarios. Column eight represents the HLW inventory at the reprocessing plant, based on a minimum of one year hold up or until 10 years after reactor discharge.

Table B.4 contains the details of shipments of fuel and HLW to and from the MRS/IS. The left half of the table has BWR data and the right half PWR data. Positive numbers represent additions or shipment to the facility while negative values represent shipments or removals from the facility. In Table B.4, the amount of each shipment is given as the tonnes of heavy metal in the original fuel. Thus the HLW shipments must be converted to canisters to obtain storage requirements (see Table B.5). The exposure is the average exposure in MWd/kg. The discharge year is the year the youngest fuel in the mixture was discharged.

Table B.6 contains similar data for TRU. On this table, the left-hand column of each pair represents TRU generated while reprocessing BWR fuel and the right-hand column of each pair represents TRU generated while reprocessing PWR fuel. Number of packages of treated wastes handled each year is also given in Table B.6. In addition to the data given in Table B.6, the MOX plant is assumed to produce one 4 ft x 6 ft x 6 ft box for each 100 drums.

Tables B.7 and B.8 are similar to Tables B.3 and B.4 and present data for the delayed reprocessing scenario. Table B.8, however, does not include TRU since the MRS/IS will not receive any TRU in this scenario. Tables B.9-11 are similar to Tables B.4-6 and present data for the delayed disposal scenario. Tables B.12 through B.16 present data for the early disposal and delayed disposal-no reprocessing scenario and are for information only.

The spent fuel and HLW requirements at MRS/IS were summarized in Table B.5. The peak rates given in Tables B.4, B.8, and B.10 were averaged over 2 or 3 years since the peaks are the result of setting the age of a year's reprocessing plant production of HLW equal to the age of the youngest fuel in the mixture. This causes large and unrealistic variations in

B.7

				BWR FUEL							PWR FU	EL.		
YFAR	FUEL	STUR	AGE	HEW	STORA	AGE	REP PLNT	FUEL	STORA	GE	HLW	STORA	GF	REP PLNT
	TUNNE	EXP L	DISCHG	TUNNE	EXP L) I SCHG	POOL INV	TUNNE	EXP D	ISCHG	TONNE	EXP D	ISCHG	POOL INV
1941	0.	0.	1971	0.	0.	1970	0.	0.	0.	1971	0.	0.	1970	0.
1962	0.		1971		0.	1970	0.	0.	Ű.	1971	0.	0.	1970	0.
1903	0.	0.	1971	Ű.	0.	1970	0.	0.	0.	1971	0.	0.	1970	0.
1984	0.	i.	1971	Ŭ.	0.	1970	Ű.	13.	51.	1971	0.	0.	1970	0.
1985	Ŭ.	ΰ.	1971	0.	0.	1979	0.	0.	0.	1971	0.	0.	1970	0.
1986	0		1971	0.	0.	1970	0.	103.	21.	1972	U.	0.	1970	0.
1980	11		1972		0.	1970	ú.	165.	23.	1974	0.	0.	1970	0.
1988	177.	15.	1974		0.	1970	0.	61.	21.	1974	0.	0.	1970	0.
1989	-4.		1972	U.,	0.	1970	200.	-22.	21.	1972	0.	Ö.	1970	300.
1990	-183.	15.	1974	200.	16.	1975	400.	-307.	22.	1974	300.	21.	1975	600.
1991	υ.	Ú.	1974	400.	16.	1976	600.	-12.	21.	1974	600.	22.	1976	900.
1992	0.	U .	1974	600.	17.	1977	600.	0.	0.	1974	900.	23.	1978	900.
1993	0.	Ű.	1974	600.	20.	1979	600.	0.	0.	1974	900.	24.	1979	900.
1994	Ű.	6.	1974	609.	22.	1990	600.	0.	υ.	1974	900.	26.	1980	900.
1995	0.	Ű.	1974	609.	23.	1991	600.	٥.	0.	1974	900.	29.	1981	900.
1996	0.	U.	1974	600.	25.	1982	600.	0.	0.	1974	900.	30.	1983	900.
1997	0.	0.	1974	60V.	25.	1983	600.	0.	Ο.	1974	900.	30.	1983	900.
1994	0.		1974	-120.	16.	1975	600.	0.	0	1974	-180.	21.	1975	900.
1999	Ű.		1974	-120.	16.	1976	600.	0.	0.	1974	-180.	21.	1976	900.
2000	0.	9.	1974	-120.	16.	1970	800.	0.	0.	1974	-180.	22.	1976	1200.
2001	Ű.	0.	1974	80.	25.	1987	1000.	0.	0.	1974	120.	30.	1986	1500.
2002	υ.	Ü.	1974	-440.	16.	1977	1200.	0.	0.	1974	-660.	22.	· 1978	1800.
2003	0.	υ.	1974	-720.	18.	1979	1200.	0.	0.	1974	-1080.	23.	1979	1800.
2004	0.	Ű.	1974	-720.	21.	1980	1200.	0.	υ.	1974	-1080.	25.	1980	1800.
2005	0.	υ.	1974	-720.	23.	1981	1600.	0.	υ.	1974	-1080.	28.	1981	2400.
2006	0.	U.	1974	-320.	25.	1982	2000.	0.	0.	1974	-480.	30.	1983	3000.
2007	υ.	ΰ.	1974	-400.	25.	1983	2400.	0.	0.	1974	-600.	30.	1983	3600.
2008	Ο.	υ.	1974	0.	0.	1970	2400.	0.	0.	1974	0.	0.	1970	3600.
2009	ΰ.	. U.	1974	0.	0.	1970	2400.	0.	0.	1974	0.	θ.	1970	3600.
2010	Ű.	U.	1974	υ.	Ŭ.	1970	5200.	0.	0.	1974	0.	0.*	1970	4200.
2011	Ú.	υ.	1974	400.	25.	2001	2600.	0.	0.	1974	600.	35.	1999	3900.
2012	Ο.	Ú.	1974	200.	25.	2002	3000.	0.	0.	1974	300.	35.	2001	4500.
2013	Ű.	0.	1974	-1200-	25.	2002	6000.	0.	ų.	1974	900.	35.	2003	4500.
2014	0.	υ.	1974	600.	25.	2004	6000.	0.	0.	1974	900.	35.	2004	4500.
2015	υ.	υ.	1974	-120.	25.	2004	6000.	0	0.	1974	-3600.	34.	2004	9000.
2016	0.	U .	1974	-480.	25.	2004	9000.	0.	0.	1974	0.	0.	1970	9000.
2017	0.	υ.	1974	9.	0.	1970	9000.	0.	0.	1974	0.	0.	1970	9000.
2018	0.	Ű.	1974	0.	0.	1970	9000.	0.	0.	1974	0.	0.	1970	9000.
2019	υ.	4.	1974	υ.	0.	1970	9000.	0.	0.	1974	0.	0.	1970	13500.
2020	0,	Ú.	1974	0.	υ.	1970	9000.	0.	0.	1974	0.	θ.	1970	13500.

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TABLE B.4. Reference Scenario, Fuel and HLW Shipments at MRS (Reference Case June 21, 1982)

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TABLE B.5. Spent Fuel and HLW (MTHM) Storage Capacity Requirements at MRS/IS Facility

	Reference	Delayed Reprocessing	Delayed Disposal
Fuel capacity	(a)	7,547	(a)
HLW capacity	10,500		60,600
Annual receiving rate ^(b)	1,500	1,500	4,500
Annual removal rate ^(C)	1,800	2,200	4,800

(a) No spent fuel in stored at MRS/IS facility prior to startup in 1990

(b) Peak rates averaged over 2 years.(b) Peak rates averaged over 3 years.

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YEAR	HULLS & HO	W ZAIO CAN	REMOTE H	2X10 CAN	REHOTE H S	5 GA DRUM	CONTACT H	4X6X6 BOX	CONTACT H	55 GA DRU	M MOX PLANT	55 G DRUMS
1981	υ.	υ.	.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1982	0	0	0.	υ.	0.	0.	0.	0	٥.	0.	٥.	0.
1983	0.	υ.	0.	υ.	0.	0.	0.	0.	0.	0.	Ο.	Ο.
1984	0.	0.	U .	0.	0.	0.	Ο.	0.	0.	0.	٥.	0.
1985	0.	0.	0.	ΰ.	Q.	0.	υ.	0.	0.	0.	0.	0.
1004	0	4	0	0	•	0	0.		٥.	0.	٥.	0.
1700	v.					Å.	0.	~. ^	0.	0.		0
1967	v.	0	0.		0.	v .		.		0.		0
1440	v.	v .		v •	0.	v.	v .	••				ů.
1484		V •	V •			140	v.	U .	4 30	450	210	316
1440	04.	¥0.	7.	14.	93.	140.	3.	э.	437.	037.	210.	313.
1991	128.	192.	18.	28.	186.	279.	7.	10.	A78.	1317.	420.	630.
1992	192.	288.	58.	41.	277.	419.	10.	15.	1317.	1976.	630.	945.
1993	192.	208.	28.	41.	279.	419.	10.	15.	1317.	1976.	630.	945.
1994	192.	200.	54.	41.	219.	419.	10.	15.	1317.	1976.	630.	945.
1995	192.	208.	24.	41.	219.	419.	10.	15.	1317.	1976.	630.	945.
1996	192.	208.	20.	41.	279.	419.	10.	15.	1317.	1976.	630.	945.
1997	192.	6 D D .	28.	41.	219.	419.	10.	15.	1317.	1976.	630.	945.
1998	-13.	-109.	-10.	-10.	-106.	-159.	-4.	-0.	-501.	- 751.	-239.	-359,
1999	-13.	-109.	-19.	-10.	-106.	-159.	-4,	-6.	-501.	-751.	-239.	-359.
2000	-73,	-109.	-10.	-10.	-106.	-159.	-4.	-6.	-501.	-751.	-239.	-359.
2001	_4	-14.	-1-	-	-13.	-20	=0.	-1.	-61.	-92.	-29.	-44.
2001	-210	- 115	-30.		-305.	-458	-11.	-16	-1440.	-2160.	-689.	-1033.
2002	-323			- 7.0	-469.	-704	-17.	-25	.2213.	- 3319.	-1058.	-1588.
2003	-323		- 4 5	- 74		-704	-17	-25	-2913	-3319	-1058	-1548
2004	= J2 J.		-40.		- 34.)		-14	-20	-1401	-3497	-1058	~1285
2005	-201.	- 372 .	- 30.		-300.	-570+	-14.	-20.	-1/710	-2001.	-057.	-1203.
2006	υ.	υ.	0.	υ.	θ.	0.	0.	0.	0.	0.	0.	0.
2007	Ο.	0.	υ.	υ.	υ.	0.	0.	0.	0.	0.	0.	0.
2008	Ú.	Ú.	Ð.	υ.	υ.	0.	0.	0.	0.	0.	0.	0.
2009	0.	Ű.	0.	Ű.	0.	0.	0.	0.	Ο.	0.	0.	0.
2010	0.	0.	Ú.	υ.	0.	0.	Ű.	0.	0.	0.	, 0 .	0.
2011	13.	19.	۷.	j.	19.	28.	1.	1.	88.	132.	42.	63.
2012	-13.	-19.	-2.	-J.	-19.	-28.	-1.	-1.	-88,	-132.	-42.	-63.
2013	in.	115.	11.	17.	112.	168.	4.	6.	527.	790.	252.	378.
2014	11.	115.	11.	1/.	112.	168.	4.	6.	527.	790.	252.	378.
2015	-154.	-230.	-72.	.tt-	-223.	-335.	-8.	-12.	-1054.	-1581.	-504.	-756.
2016	b .	Ű.	0 -	٥.	۵.	0.	θ.	0.	0-	0.	0.	0.
2017		0.	11 -	u .	ů.	0.	0.	0_	0.	0.	0.	0.
2018		¥.	υ. 	ų.	0.	0.	0 .	0.	0.	0.	0.	0.
2010	Å.	0	0	ч .	с .	0.	Δ.	0.	0.	0.	<u>.</u>	0.
2030	v. ^	0		v •	с	· ·	~	~ .	Δ.	0.	ů.	0.
2020	.	· •	9 e	v.	v.	۰.	.	v .	¥.	~.	~ .	

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TABLE B.6. Reference Scenario, Number of TRU Packages Handled at MRS (Reference Case June 21, 1982)

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YEAH	DISCHARGE	AR INV	MRS INV	REPROCESS	DISPOSAL	DISP INV	HLW A R	HLW MRS	DISPOSAL	DISP INV
1981	1090.	7871.	0.	v.	0.	0.	0.	0.	0.	0.
1982	123/.	9108.	0.	υ.	0.	0.	0.	0.	0.	0.
1983	1607.	10715.	0.	υ.	0.	0.	0.	υ.	0.	0.
1984	1744.	12447.	13.	Ú.	0.	0.	0.	0.	0.	0.
1985	2167.	14614.	13.	υ.	0.	0.	0.	0.	0.	0.
1986	2610.	17121.	116.	Ο.	. 0.	0.	0.	0.	0.	0.
1987	2622.	19567.	292.	υ.	0.	0.	0.	0.	Ο.	0.
1988	2866.	22196.	530.	Ο.	Ο.	Ο.	0.	0.	0.	0.
1989	J253.	24945.	1003.	υ.	0.	0.	0.	0.	0.	0.
1990	3071.	27555.	1463.	U.	0.	0.	0.	0.	0.	0.
1991	3078.	30110.	1987.	Ο.	0.	0.	0.	0.	0.	0.
1992	3498.	75865*	2633.	υ.	0.	0.	0.	0.	0.	0.
1993	3428.	35721.	3305°	0.	Ο.	0.	0.	0.	0.	0.
1994	3389.	38110.	4302.	Û.	0.	0.	0.	Ο.	0.	0.
1995	3574.	40434.	5552.	Ű.	θ.	0.	0.	0.	0.	0.
1996	34/0.	42404.	/052.	Ű.	0.	0.	0.	0.	0.	0.
1997	3498.	44404.	8550.	Û.	0.	0.	0.	0.	0.	0.
1998	3874.	46550.	8478.	U.	1800.	1800.	0.	0.	0.	0.
1999	3860.	48456.	447R.	500.	1454.	3254.	500.	0.	0.	0.
2000	3964.	50333.	847H.	1000.	1087.	4341.	1000.	0.	500.	500.
2001	4386.	52328.	6478.	1500.	891.	5232.	1500.	91.	909.	1409.
2005	440/.	53949.	8478.	1200.	1286.	6518.	1500.	0.	1591.	3000.
2003	4569.	5822 .	d478.	1500.	1197.	7715.	1500.	0.	1500.	4500.
2004	4919.	57654.	8478.	1500.	1588.	9302 .	1500.	0.	1500.	6000.
2005	4841.	59554.	8478.	1500.	1441.	10743.	1500.	0.	1500.	7500.
2006	5226.	6180/.	8478.	1500.	1472.	12215.	1500.	0.	1500.	9000.
2007	60 0 1.	6459l.	8478.	1200.	1798.	14013.	1500.	0.	1500.	10500.
5009	6043.	67936.	8478.	1200.	1198.	15211.	1500.	0.	1500.	12000.
2009	n537.	/1287.	8478.	1500.	1686.	16896.	1500.	0.	1500.	13500.
2010	6251.	/4706.	d478.	2000.	832.	17728.	2000.	0.	1500.	15000.
2011	6228.	78370.	847B.	2200.	64.	17793.	2500.	0.	2000.	17000.
2015	6381.	82317.	1852.	3000.	Ο.	17793.	3000.	0.	2500.	19500.
2013	6485.	86358.	7356.	3000.	0.	17793.	3000.	0.	3000.	22500.
2014	6727.	90962.	6479.	3000.	Ο.	17793.	3000.	0.	3000,	25500.
2015	7033.	95787.	4687.	4000.	0.	17793.	4000.	0.	3000.	28500.
2016	6690.	100221.	1943.	5000.	0.	17793.	5000.	0.	4000.	32500.
2017	6869.	103033.	0.	6000.	υ.	17793.	6000.	0.	5000.	37500.
2018	7258.	104291.	0.	6000.	0.	17793.	6000.	Ο.	、6000。	43500,
2019	6645.	104984.	0.	6VUD.	0.	17793.	6000.	0.	6000.	49500.
2020	7046.	105030.	0.	7000.	υ.	17793.	7000.	0.	6000.	55500.

TABLE B.7. Delayed Reprocessing Scenario Summary (June 21, 1982)

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					نكرره ليست							PWP FUE	Fi		
	VEAN	FUEL	STOR	AGE		STORA	GE	REP PLNT	FUEL	STOR	GE	HLW	STORA	GF	REP PLNT
	ICAN	TONNE	EXP L	DISCHU	TUNNE	EXP L	ISCHG	POOL INV	TONNE	EXP L	ISCHG	TONNE	EXP U	ISCHG	POOL INV
	1981	0.	0.	1971	υ.	υ.	1970	0.	0.	0.	1971	0.	0.	1970	0.
	1982	0.	υ.	1971	θ.	Ο.	1970	υ.	Ο.	0.	1971	0.	0.	1970	0.
	1983	0.	U.	1971	Ŭ.	0.	1970	0.	Ο.	0.	1971	0.	ų.	1970	0.
	1984	0.	υ.	1971	Ú.	Ο.	1970	υ.	- 13.	21.	1971	0.	0.	1970	0.
	1985	0.	V.	1971	Ú.,	0.	1970	0.	0.	0.	1971	0.	U.	1970	0.
	1986	υ.	0.	1971	. 0.	0.	1970	υ.	103.	21.	1972	0.	0.	1970	0.
	1987	11.	ý.	1972	0.	υ.	1970	υ.	165.	23.	1974	0.	0.	1970	0.
	1988	177	15	1974	ш. Ш.	0.	1970	Ú.	61	21.	1974	0.	0.	1970	0.
	1000	196	10-	1975	- i -	<u>.</u>	1970	 U -	277.	21.	1975	0.	0.	1970	0.
	1990	168.	17.	1976	0.	0.	1970	ΰ.	293.	21.	1976	0.	U.	1970	ů.
	1001	141.	17.	1977	ú -	Ű.	1970	0.	193-	22.	1976	0.	0.	1970	0.
	1092	24H -	17.	1977	0.	Ű.	1970	0	398.	23.	1977	0.	0.	1970	0.
	1992	234	18.	1978		0.	1974	ů.	435.	23.	1978	0.	0.	1970	0.
	1995	388	21.	1978	υ.	0.	1970	0.	612.	23.	1979	Ö.	0.	1970	Ó.
	1995	353.	22.	1979	υ.	0.	1979	0.	898.	26.	1980	0.	0.	1970	0.
	1996	518.	23.	1980	0.	U.	1970	υ.	981.	29.	1981	0.	U.	1970	0.
I	1997	598	24.	1981	9.	0.	1970	0.	900.	30.	1983	0.	0.	1970	0.
1	1998	-71.	14.	1974	0.	0.	1970	0.	-1.	21.	1971	0.	0	1970	0.
)	1009	 0 -		1470	ί.	ü.	1970	200.	0.	0.	1970	0.	0.	1970	300.
	2000	υ.	υ.	1970	U.	ΰ.	1970	450.	0.	0.	1970	0.	0.	1970	550.
	2001	0.	0.	1970	٤.	25.	1985	550.	0.	0.	1970	88.	30.	1985	950.
	2002	0.	٥.	1970	-6.	25.	1985	600.	0.	0.	1970	-88.	30.	1985	900.
	2003	U.		1470	 U •	0.	1970	600.	0.	0.	1970	0.	0.	1970	900.
	2004	0.	0.	1970	0.	0.	1970	600.	0.	0.	1970	0.	0.	1970	900.
	2005	υ.	Ŭ.	1970	υ.	υ.	1979	600.	0.	Ű.	1970	0.	0.	1970	900.
	2006	0.	Ű.	1970	0.	υ.	1970	600.	0.	٥.	1970	0.	0.	1970	900.
	2007	Ú.		1970	0.	0.	1970	600.	0	0.	1970	0.	0.	1970	900.
	2008	Ō.	Ū.	1970	0.	Ű.	1970	600.	0.	0.	1970	0.	0.	1970	900.
	2009	Ū.	υ.	19/0	υ.	0.	1970	600.	0	0.	1970	0.	0.	1970	900.
	2010	0.	U .	1970	0.	0.	1970	800.	0.	0.	1970	0.	0.	1970	1200.
	2011	0.	·) •	1970	() .	ΰ.	1970	1000.	0.	0.	1970	0.	0.	1970	1500.
	2012	-184.	10.	1975	υ.	0.	1970	1200.	-442.	22.	1975	0.	0.	1970	1800.
	2013	-78.	16.	1975	0.	່ ບໍ	1970	1200.	-418	21.	1976	0.	0.	1970	1800.
	2014	-313	1/.	1977	U -	0.	1975	1200.	-564.	22.	1977	0.	0.	1970	1800.
	2015	-688	17.	1978	0.	0.	1970	1600.	-1103,	23.	1979	0.	0.	1970	2400.
	2016	-963.	22.	1980	υ.	0 -	1970	2000-	-1781.	27.	1981	0.	0.	1970	3000.
	2017	-923	23.	1981	Ú -	<u>.</u>	1970	2400.	-1019	30.	1983	0.	0.	1970	3600.
	2014	0.	<u> </u>	1981	0.	0.	1976	2400-	0.	0.	1983	0.	0.	1970	3600-
	2010	v •	0	1481	n.	0	1970	2400	0. 0.	0.	1983	0.	0.	1970	3600-
	6717		v •	1201	u .	¥ •	1 2 1 1	24000	v •	~ •					

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Scenario Summary (June 21, 1982)	fszoqziū beysfeū	. <u>0.8</u> 3J8AT
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•00099	•0006	*000R+	• 00522	• 0	•0	*00S/	• 0	*2288+	*9+07	5020
*000/5	*008/	*0056*	*005ZZ	• 0	• 0	• no </td <td>•0</td> <td>• 4/26+</td> <td>• 26.90</td> <td>5016</td>	•0	• 4/26+	• 26.90	5016
.00264	•00g/	•00£+S	18000°	• 0	• 0	*n0c/	• 0	*+800C	*9CZ/	8107
*1+00	*0081	1009+5	*000R1	•0	•0	•00¢j	• 0	97F0G	*6989	2102
*009EE	•0099	•006+5	18000°	• 0	• 0	·00¢/	• 0	19605	.0699	5016
•0001S	•0099	°00015	°00051	• 0	• n	•005/	• 0	•19219	*EE07	SUZ
\$0¢00	*008 *	*00409	*0050l	• U	• 0	*00SL	• 0	P5533*	•1210	5010
100951	*008 *	•00615	*00501	• 0	• 0	•009/	•0	*900ES	* 58+9	5102
10800	3600	28500	*00 <u>5</u> 1	• 0	• 0	*0052	• U	24055*	* TRE4	2015
1200.	*008 t	°00£55	•0059	• 0	• 0	•00co	• U	*0+ISS	•5254 *	5011
*00+5	°0081	°00105	.000T	• 0	• ೧	•0007	• U	*21999	•1929	5010
*009E	1900°	*0065*	*0009	• 0	• 0	•0004	• 0	*19194	·1624	6002
*0081	1800	•00/1+	•0009	• 0	• 0	*0009	• 0	*52954	•E#0a	2008
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• 0	• 0	35200	°0005	• 0	•0	•000c	• 0	*005 <u>5</u> 4	2556	5005
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-0	•0	-00582	0004	-0	10	*000*	•0	**/255	1989	5002
• 0	• 0	55500	.000E	• 0	•0	.0002	• 0	• • • • • • • • •	*616*	400Z
• 0	•0	22500	3000 ·	• 0	• 0	10005	• 0	• 51525	6954	EOOS
• 0	•0	00561	.000E	• 0	•0	•000F	• 0	5960c	• 20 7 7	2002
•0	•0 ·	-00071	*005Z	•0	-0	•0047	• 0	"PE56"	*986*	1005
• 0	• 0	*000C1	• 0 0 0 7	• 0	• n	• • • • • • • • • • • • • • • • • • • •	• 0	•269/+	14965	0002
• 0	• 0	•00cc1	*0061	• n	• 0	*n0c1	•0	*990C+	1095	6661
• 0	•0	*0002T	*00G1	• 0	• 0	*00C1	•0	•07CC+	**/UC	8661
• 0	•0	*00col	*0051	• 0	• 0	*005T	• 0	*****	*06+C	1661
• n ·	•0	*0004	10051	•	•0	100-1	• 0	*960**	9075 9076C	9661
v	v	0006	0031	U	v	0041	Ū	******	02.96	7001
•0	•0	*005L	•00ST	• 0	• 0	• n 0 = T	• U	•98695	•+LSE	566 L
•0	• 0	•0009	*00ST	•0	• 0	1 200°	• 0	34815*	*6HEE	*661
•0	•0	*00G+	10051	• 0	• 0	*005t	• 0	\$3053°	3458	E64 I
•0	• 0	*000E	*00S1	• 0	• 0	1200	• U	*5601E	*R67E	2661
• 0	• 0	*00ST	10051	• 0	•0	*009T	• U	•16067	*#10F	1661
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•0	• 0	• 0	•0	• 0	• 0	• 0	•UEC	96122	9482	886 T
•0	• 0	• 0	•0	• 0	• 0	• 0	• 242	19961	5622	1861
•0	•0	•0	•0	• 0	•0	• 0	•911	15171	*019Z	98 6 [
• 0	• 0	• 0	• 0	• 0	• 0	• 6	• 6 1	*****	•/017	5861
• ň	• 0	• 0 .	• 0	• 0	• 0	• 0	• 6 1	•/++21	***/1	5861
• 0	•0	*0	• 0	• 0	• 0	• 0	•0	• 6 1 / 0 1	1001	6961
• 0	• 0	• 0	• 0	•0	• 0	• 0	• 0	•801A	1621	2861
• 0	• 0	• ŏ	• 0	• ŏ	• 0	•0	•0	•1/9/	•060T	1861
J	-	-	v	-	-		-			
ANI dSIO	JA209210	SAM WIH	н∀ м]н	VNI 9210	14209210	REPROCESS	ANI SHH	VNI HA	JOHAHO21U	назу

TABLE B.9 (contd)

YEAR	DISCHARGE	AK INV	WRS INV	REPROCESS	DISPOSAL	DISP INV	HLW A R	HLW MRS	DISPOSAL	DISP INV
2021	7000.	48322.	0.	1500.	0.	0.	25500.	43500.	9000.	75000.
2022	7000.	4/822.	0.	/500.	U.	0.	25500.	42000.	9000.	84000.
2023	7000	4/322.	0.	7500.	Ο.	θ.	25500.	40500.	9000.	93000.
2024	7000.	46822.	0.	/500.	0.	υ.	25500.	39000.	9000.	102000.
2025	1500.	46855.	A.	7500.	0.	0.	25500.	35700.	10800.	112800.
2026	/500.	46822.	0.	/500.	ΰ.	0.	25500.	32400.	10800.	123600.
2027	7500.	46822.	0.	7530.	Ο.	Ο.	30000.	24600.	10800.	134400.
2028	/500.	46822.	0.	7500.	U.	Ο.	30000.	21300.	10800.	145200.
2029	7500.	46822.	0.	7500.	Û.	0.	30000.	18000.	10800.	156000.
2030	1500.	46822.	Ο.	1500.	0.	0.	30000.	13500.	12000.	168000.
2031	7500.	46822.	0.	750u.	0.	0.	30000.	9000.	12000.	180000.
2032	/500.	46822.	0.	7500.	U.	0.	30000.	4500.	12000.	192000.
2033	7500.	46822.	0.	/500.	0.	0.	30000.	0.	12000.	204000.
2034	7500.	46822.	0.	/500.	0.	0.	30000.	0.	7500.	211500.
2035	7500.	46822.	0.	/200.	0.	0.	30000.	Û.	7500.	219000.
2036	1500.	46822.	0.	1500.	0.	ΰ.	30000.	0.	7500.	226500.
2037	7500.	46822.	0.	7500.	0.	0.	30000.	0.	7500.	234000.
2038	7500.	40855.	0.	7500.	0.	0.	30000.	0,	7500.	241500.
2039	7500.	46822.	0.	7500.	0.	0.	30000.	0.	7500.	249000.
204 0	7500.	46822.	0.	/200.	υ.	0.	30000.	0.	7500.	256500.

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TABLE B.10.	Delayed Disposal	Scenario,	Fuel	and HLW	Shipments	at MRS	(June 21,	19 82)
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				BWR FUEL							PWR FU	EL		
YEAH	FUEL	STUR/	AGE	HL#	STOR	AGE	REP PLNT	FUEL	STOR	GE	HLW	STORA	GE	REP PLNT
	TONNE	EXP L	JISCHG	I UNNE.	EXP C	DISCHG	POOL INV	TONNE	EXP D	ISCHG	TONNE	EXP D	ISCHG	POOL INV
1981	Ű.	э.	1971	0.	0.	1970	Ű.	0.	0.	1971	0.	0.	1970	0.
1982	0.	0.	1971	V.	ΰ.	1970	μ.	0.	0.	1971	0.	0.	1970	0.
1983	0.		1971	υ.	<u>.</u>	1970	IJ.	0.	0.	1971	0.	0.	1970	0.
1984	й. И.	0.	1971	Ű.	θ.	1970	0.	13.	21.	1971	0.	0.	1970	0.
1985	υ.	υ.	1971	ů.	0.	1970	Ú .	0.	0.	1971	0.	0.	1970	0.
1986	U.	0.	1971	υ.	0.	1970	Ű.	103.	21.	1972	Û.	0.	1970	0.
1987	11.	У.	1972	u.	Ο.	1970	0	165.	23.	1974	0.	0.	1970	0.
1988	177.	15.	1974	0.	0.	1970	Û.	61.	21.	1974	0.	0.	1970	Ο.
1989	-4.	٧.	1972	θ.	Ú.	1970	200.	-22.	21.	1972	0.	Û.	1970	300.
1990	-183.	15.	1974	500.	16.	1975	400.	-307.	22.	1974	300.	21.	1975	600.
1991	υ.	υ.	1974	40J.	16.	1975	600.	-12.	21.	1974	600.	22.	1976	900.
1992	θ.	U •	1974	600.	17.	1977	60U.	0.	Ű.	1974	900.	53.	1978	900.
1993	Ű.	Ú.	1974	600.	20.	1979	600.	٥.	0.	1974	900.	24.	1979	900.
1994	υ.	9 e	1974	60u.	22.	1989	600.	0.	0.	1974	900.	26.	1980	900.
1995	υ.	Ú.	1974	6 0 0.	23.	1981	600.	0.	0.	1974	900.	29.	1981	900.
1996	υ.	U.	1974	600.	25.	1985	600.	0.	0.	1974	900.	30.	1983	900.
1997	Ο.	U.	1974	600.	25.	1983	600.	Ο.	Û.	1974	900.	30.	1983	900.
1998	0.	υ.	1974	600.	25.	1984	600.	Ο.	0.	1974	900.	30.	1984	900.
1999	Ο.	U.	1974	600.	25.	1985	600.	Ο.	Ű.	1974	900.	30.	1985	900.
2000	0.	U .	1974	600.	25.	1985	6∪0 •	0.	0.	1974	900.	30.	1986	1200.
2001	υ.	υ.	1974	A00.	25.	1987	1000.	0.	0.	1974	1200.	30.	1986	1500.
2002	ΰ.	U .	1974	1000.	25.	1988	1500*	0.	0.	1974	1500.	30.	1987	1800.
2003	٥.	Û.	1974	1200.	25.	1949	1500.	Ο.	0.	1974	1800.	30.	1988	1800.
2004	∎ نا	Q 🐽	1974	1500.	25.	1990	1200.	۰.	0.	1974	1800.	. 30.	1989	1800.
2005	υ.	0.	1974	1200.	25.	1991	1600.	0.	0.	1974	1800.	30.	1990	2400.
2006	0 .	U .	1974	1600.	25.	1992	2000.	0.	0.	1974	2400.	33.	1991	3000.
2007	Ο.	0.	1974	2000.	25.	1994	2400.	Ο.	Ο.	1974	3000.	35.	1993	3600.
5009	0.	Ú 🖕	1974	1680.	25.	1995	2400.	0.	0.	1974	2520.	35.	1994	3600.
2009	0.	0.	1974	1680.	25.	1997	2400.	0.	0.	1974	2520.	35.	1996	3600.
2010	0.	U e	1974	1689.	25.	1999	2800.	0.	υ.	1974	2520.	35.	1998	4200.
2011	Ű.	U.	1974	2080.	25.	5001	2600.	0.	0.	1974	3120.	35.	1999	3900.
2012	υ.	J e	1974	1160.	25.	2002	. 3000 .	Ο.	٥.	1974	1740.	35.	2001	4500.
2013	0.	U.	1974	-1920.	18.	1980	6000.	0.	υ.	1974	1620.	35.	\$003	4500.
2014	υ.	U •	1974	1080.	25.	2004	6000.	0.	° 0.	1974	1620.	35.	2004	4500.
2015	0.	U.	1974	360.	25.	2005	6000.	0.	0.	1974	-3960.	24.	1981	9000.
2016	0.	() .	1974	-2640.	24.	1984	9000.	0.	٥.	1974	540.	35.	2006	9000.
2017	Ο.	e تا	1974	-120+	25.	1984	9000.	Û.	0.	1974	-180.	29.	1981	9000.
2018	Ű.	U.	1974	-120.	25.	1984	9000.	٥.	0.	1974	-180.	29.	1981	9000.
2019	0.	Ü.∎	1974	-120.	25.	1985	9000.	Ο.	0.	1974	-4680.	30.	1986	13500.
2020	0.	0.	1974	-600.	25.	1986	4000 .	0.	U.	1974	-900.	30.	1986	13500.

TABLE B.10 (contd)

				HWR FUEL							PWR FU	EL		
YEAR	FUEL	STUR	AGE	HLW	STOR	AGE .	REP PLNT	FUEL	STOR	AGE	HLW	STOR	AGE	REP PLNT
	TUNNE	EXH	DISCHG	IUNNE	EXP L	DI PCHO	POOL INV	TONNE	EXP	DISCHG	TONNE	EXP	DISCHG	POOL INV
2021	0.	ΰ.	1974	-3600.	25.	1990	12000.	0.	0.	1974	-900.	30.	1987	13500.
2022	0.	Ü.	1974	-600.	25.	1990	12000.	0.	0.	1974	-900.	30.	1987	13500.
2023	0.	U .	1974	-600.	25.	1991	12000.	Ο.	0.	1974	-900.	30.	1988	13500.
2024	0.	0.	1974	-600.	25.	1991	12000.	0.	0.	1974	-900.	30.	1988	13500.
2025	υ.	υ.	1974	-1320.	25.	1992	15000.	0.	0.	1974	-1980.	30.	1990	13500.
2026	υ.	Ð.	1974	-1320.	25.	1994	12000.	0.	Ű.	1974	-1980.	31.	1991	13500.
2027	υ.	U .	1474	-1320.	25.	1994	12000.	0.	0.	1974	-6480.	34.	1994	18000.
2028	0.	U.	1974	-1320.	25.	1995	15000.	0.	ΰ.	1974	-1980.	35.	1996	18000.
2029	υ.	υ.	1974	-1320.	25.	1997	12000.	Ο.	0.	1974	-1980.	35.	1998	18000.
2030	U,	U .	19/4	-1800.	۲۶.	1999	12000.	0.	0.	1974	-2700.	35.	1999	18000.
2031	0.	υ.	1974	-1800.	25.	2001	12000.	0.	Ο.	1974	-2700.	35.	2001	18000.
2032	υ.	Ú.	1974	-1800.	25.	2002	12000.	0.	0.	1974	-2700.	35.	2003	18000.
2033	0.	U.	1974	-1800.	25.	2005	12000.	Ο.	0.	1974	-2700.	35.	2006	18000.
2034	υ.	ΰ.	1974	0.	υ.	1970	12000.	Ο.	0.	1974	0.	0.	1970	18000.
2035	0.	υ.	1974	Û.	0.	1970	12000.	0.	Ű.	1974	0.	0.	1970	18000.
2036	Ű.	U.	1974	Ű.	0.	1970	12000.	Ú.	Ű.	1974	0.	Ο.	1970	18000.
2037	υ.	U.	1974	0.	0.	1970	12000.	0.	0.	1974	· 0.	0.	1970	18000.
2038	u.	Ú.	1974	Ű.	Ű -	1970	12000.	0	υ.	1974	0.	0.	1970	18000.
2039	0.	U .	1974	Ū.	0.	1970	12000.	0.	Ű.	1974	0.	0.	1970	18000.
2040	υ.	ΰ.	1974	0.	0.	1970	12000.	0.	0.	1974	0.	0.	1970	18000.

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YEAR P	10LL5 & HD)w 2×10 CAN	REMOTE H	2XIU CAN	REMOTE H 5	5 GA DRUM	CONTACT H	4X6X6 BOX	CONTACT H	55 GA DRUM	NOX PLANT	55 G DRUMS
1981	0.	0 .	9.	v.	0.	0.	0.	٥.	0.	0.	0.	٥.
1982	0 .	υ.	0.	ΰ.	Ú.	0	.	0.	0.	0.	0.	0.
1983	0.	υ.	0.	υ.	0.	0.	0.	0.	0.	0.	0.	0.
1984	υ.	υ,	υ.	υ.	0.	0.	0.	0.	٥.	0.	0.	0.
1985	0.	٥.	0 .	۷.	υ.	0.	0.	0.	Ο.	0.	0.	٥.
1986	٥.	0.	U.	9 .	υ.	0.	0.	0.	0.	0.	٥.	0.
1987	Ο.	υ.	ν.	ú.	ν.	٥.	0.	٥.	0.	0.	0.	0.
1988	٥.	٥.	υ.	ν.	Ú.	٥.	0.	0.	٥.	0.	0.	U.
1989	Ο.	υ.	θ.	υ.	Ð.	0.	0.	0.	0.	0.	٥.	0.
1490	64.	¥6.	۷.	14.	43.	140.	3.	5.	439.	659.	210.	315.
1991	128.	192.	18.	24.	186.	279.	7.	10.	R78.	1317.	420.	630.
1992	195.	280 .	24.	41.	279.	419.	10.	15.	1317.	1976.	630.	945.
1993	192.	c08.	2H.	41.	279.	419.	10.	15.	1317.	1976.	630.	945.
1494	142.	288 .	52.	41.	279.	419.	10.	15.	1317.	1976.	630.	945.
1995	195.	208.	28.	41.	279.	419.	10.	15.	1317.	1976.	630.	94 0 .
1996	192.	208.	59.	41.	279.	419.	10.	15.	1317.	1976.	630.	945.
1997	192.	288.	26.	41.	279.	419.	10.	15.	1317.	1976.	630.	945.
1998	192.	288.	28.	41.	279.	419.	10.	15.	1317.	1976.	630.	945.
1999	192.	c08.	28.	41.	279.	419.	10.	15.	1317.	1976.	630.	945.
2000	192.	∠88.	24.	+ì.	279.	419.	10.	15.	1317.	1976.	630.	945.
2001	256.	. ۵۹4	37.	55.	372.	558.	13.	20.	1756.	2634.	840.	1260.
2002	320.	40U .	46.	0/.	465.	698.	17.	25.	2195.	3293,	1050.	1575.
2003	384.	5/6.	50.	8J.	558.	838.	20.	30.	2634.	3952.	1260.	1890.
2004	364.	516.	57.	43.	558.	838.	20.	30.	2634.	3952.	1260,	1890.
2005	364.	516.	55.	8J.	558.	838.	20.	30.	2634.	3952.	1590.	1890.
2005	512.	768.	74.	110.	744.	1117.	27.	40.	3512.	5269.	1680.	2520.
2007	640.	APD .	92.	130.	¥31.	1396.	33.	50.	4391.	6586.	2100.	3150.
2008	503.	/55.	72.	108.	731.	1097.	26.	39.	3451.	5177.	1651.	2476.
2009	503.	155.	. 77.	108.	731.	1097.	56.	39.	3451.	5177.	1651.	2476.
2010	503.	/55.	72.	108.	731.	1097.	26.	39.	3451.	5177.	1651.	2476.
2011	631.	941.	91.	130.	918.	1376.	33.	49.	4329.	6494.	2071.	3106.
2012	302.	45.3.	43.	65.	439.	659.	16.	24.	2072.	3109.	991.	1487.
2013	253.	380.	36.	55.	369.	553.	13.	50.	1739.	2608.	832.	1247.
2014	253.	300.	36.		369.	553.	13.	20.	1739.	2008.	832.	1247.
2015	-12.	-17.	-2.	-2.	-17.	-25.	-1.	-1.	-79.	-119.	- 38 .	-5/.
2016	-12.	-1/.	-2.	-2.	-1/.	-25.	-1.	-1.	-79.	-119.	-38.	-57.
2017	-186.	-202.	-71.	-41.	-274.	-410.	-10.	-15.	-1291.	-1936.	-617.	-926.
2018	-148.	-202.	-21.	-41.	-274.	-410.	-10.	-15.	-1291.	-1430.	-617.	-926.
2019	-188.	-202.	-51.	-41.	-274.	-410.	-10.	-15.	-1291.	-1936.	-617.	-926.
2020	-365.	-547 <u>.</u>	+52·	-79.	-530.	-796.	-19.	-29.	-2503.	-3754.	-1197.	-1795.

TABLE B.11. Delayed Disposal Scenario, Number of TRU Packages Handled at MRS (June 21, 1982)

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TABLE B.11 (contd)

YEAR H	IULLS & HDW	2×10 CAN	REMOTE H	2XIU CAN	REMOTE N	55 GA DRUM	CONTACT H	4X6X6 BOX	CONTACT H	55 GA DR	IUM HOX PLANT	55 G DRUMS
2021	-365.	-547.	-54.	-14.	-530.	-796.	-19.	-29.	-2503,	-3754.	-1197.	-1795.
2022	-365	-547.	-52.	-19.	-530.	-796.	-19.	-29.	-2503.	-3754.	-1197.	-1795
2023	-365	-547.	-52.	-74.	-530.	-796	-19.	-29.	-2503.	-3754.	+1197.	-1795.
2024	-365.	-54/.	-52.	-14.	-530.	-796.	-19.	-29.	-2503.	-3754.	-1197.	-1795.
2025	-630.	-945.	-91.	-136.	-916.	-1374.	-33,	-49,	-4320.	-6481.	-2066.	-3100.
2026	-630.	- 745.	-91.	-136.	-916.	-1374.	-33.	-49.	-4320.	-6481.	-2066.	-3100.
2027	-630	-945.	-91.	-136.	-916.	-1374.	-33.	-49.	-4320.	-6481.	-2066.	-3100.
2028	-630.	-945.	-91.	-130.	-916.	-1374.	-33.	-49.	-4320.	-6481.	-2066.	-3100.
2029	-630	-745.	-91.	-130.	-916.	-1374.	-33.	-49.	-4320.	-6481.	-2066.	-3100.
2030	-806	1210.	-116.	-1/4.	-11/3.	-1759.	-42.	-63.	-5532.	-8298.	-2646.	-3969.
2031	-806	1210.	-116.	-174.	-1173.	-1759.	-42.	-63.	+5532.	-8298.	-2646.	-3964.
2032	-576.	-864.	-83.	-124.	-838.	-1256.	-30.	-45.	-3952.	-5927.	-1890.	-2835.
2033	Ο.	U.	Ű.	υ.	0.	0.	0.	0.	0.	0.	0.	0.
2034	0.	U.	Ο.	u.	Ű.	0.	0.	0.	Ο.	0.	0.	0.
2035	υ.	0.	Ű .	υ.	υ.	0.	0.	0.	0.	0.	Ο.	0.
2036	0.	Ű.	Ű.	υ.	υ.	Ο.	0.	0.	0.	0.	Ο.	0.
2037	Ó.	U.	0.	υ.	υ.	0.	0.	0.	Ο.	0.	0.	0.
2038	0.	0.	Ű.	Û.	0.	0.	0.	0.	U.	0.	0.	0.
2039	Ο.	υ.	υ.	υ.	0.	0.	0.	۰.	0.	0.	0.	0.
2040	0.	υ.	0.	Ó.	0.	ů.	0.	U .	0.	0.	0 .	۰.

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YEAR	DISCHARGE	AR "INV	WH2 INA	REPRUCESS	DISPOSAL	DISP INV	HLW A R	HLW MRS	DISPOSAL	DISP INV
1981	1090.	/871.	0.	υ.	U.	0.	0.	0.	0.	0.
1982	1237.	9108.	0.	υ.	Ο.	0.	0.	0.	0.	0.
1983	1607.	10715.	0.	υ.	Ú.	0.	υ.	0.	0.	Ο.
1984	1744.	12447.	13.	Ú.	0.	0.	0.	0.	0.	0.
1985	2167.	14614.	13.	0.	υ.	0.	0.	0.	0.	0.
1986	2610.	17121.	116.	Ú.	Ú.	0.	0.	0.	0,	٥.
1987	2622.	19567.	292.	υ.	0.	0.	ΰ.	0.	υ.	0.
1988	2866.	22196.	530.	Ú.	U.	0.	0.	0.	0.	0.
1989	3223.	24945.	503.	500.	υ.	0.	500.	0.	Û.	0.
1990	3071.	2/507.	12.	1000.	0.	0.	1000.	500.	0.	0.
1991	3078.	29097.	0.	1500.	υ.	0.	1500.	1500.	0.	0.
1992	3498.	31095.	0.	1500.	Ű.	0.	1500.	3000.	0.	Ο.
1993	3428.	33023.	0.	1500.	υ.	0.	1500.	2700.	1800.	1800.
1994	3389.	34912.	0.	1500.	0.	0.	1500.	2400.	1800.	3600.
1995	3574.	36986.	0.	1500.	Ű.	0.	1500.	2100.	1800.	5400.
1996	3470.	38956.	0.	1500.	0.	0.	1500.	1800.	1800.	7200.
1997	3498.	40954.	0.	1500.	U.	0.	1500.	1500.	1800.	9000.
1998	3874.	43328.	0.	1500.	Ο.	0.	1500.	Ο.	3000.	12000.
1999	3860.	45688.	0.	1500.	U.	0.	1500.	0.	1500.	13500.
2000	3964.	47652.	0.	2000.	0.	0.	2000.	0.	1500.	15000.
2001	4386.	49538.	0.	2500.	0.	0.	2500.	0.	5000.	17000.
2002	4407.	50945.	0.	3000.	υ.	0.	3000.	0.	2500.	19500.
2003	4569.	52515.	0.	3000.	0.	υ.	3000.	0.	3000.	22500.
2004	4919.	54434.	0.	.000E	Ο.	0.	.000£	0.	3000.	25500.
2005	4841.	55274.	0.	÷000.	0 .	0.	4000.	0.	3000.	28500.
2006	5226.	55500.	0.	5000.	υ.	0.	5000.	0.	4000.	32500.
2007	6081.	55581.	0.	o000.	υ.	0.	6000.	0.	5000.	37500.
2008	6043.	55625.	0.	6000.	0.	0.	6000.	0.	6000.	43500.
2009	6537.	56161.	0.	6000.	υ.	0.	6000.	0.	6000.	49500.
2010	6251.	55412 .	0.	7000.	v.	0.	7000.	Ο.	6000.	55500.
2011	o228.	55140.	0.	6500.	υ.	0.	6500.	0.	7000.	62500.
2012	o381.	54022.	0.	7500.	Ű.	0.	7500.	0.	6500.	69000.
2013	ь485.	53006.	0.	7500.	0.	0.	10500.	0.	4500.	73500.
2014	6727.	52233.	0.	7500.	0.	0.	10500.	0.	7500.	81000.
2015	7033.	51767.	0.	7500.	Ú.	Ο.	15000.	0.	3000.	84000.
2016	6690.	50957.	0.	7500.	υ.	0.	18000.	0.	4500.	88500.
2017	6869.	50326 ·	0.	/500.	0.	0.	18000.	υ.	7500.	96000.
2018	7258.	50084.	0.	7500.	υ.	0.	18000.	0.	7500.	103500.
2019	6692.	49276.	0.	7500.	0.	0.	22500.	υ.	3000.	106500.
2020	7046	48822	6	1500	0	` ۵	22500	0	7500	114000

TABLE B.12. Early Disposal Scenario Summary (June 21, 1982)

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TABLE B.13.	Early Disposal	Scenario,	Fuel	and HLW	I Shipment	at	MRS	(June	21,	1982)	

				BWR FUEL							PWR FU	EL		
YEAR	FUEL	STUR	GE	HLW	STOR	AGE	REP PLNT	FUEL	STORA	GE	HLW	STORA	GE	REP PLNT
TEAN	TUNNE	FXP L	ISCHG	TUNNE	EXP L	ISCHG	POOL INV	TONNE	EXP D	ISCHG	TONNE	EXP C	ISCHG	POOL INV
1001	n	4.	1971	0.	0.	1970	0.	0.	0.	1971	0.	0.	1970	0.
1002		0.	1971	0.	Ő.	1970	0.	0.	õ.	1971	Ű.	0.	1970	0.
1982	0.		1971	() .	0.	1970	0.	0.	0.	1971	0.	0.	1970	0.
1604	0		1971		0.	1970	0.	13.	21.	1971	0.	0.	1970	0.
1985	0.	υ.	1971	υ.	ΰ.	1970	0.	0.	ΰ.	1971	0.	0.	1970	0.
1004	•	a	1971	à	n	1970	0.	103	21.	1972	0.	0.	1970	0.
1960		¥•	1072		.	1475	0.	165	21.	1974	0.	0.	1970	0.
1987	11.	1-	1772	0.		1070	0.	61	21.	1974	0.	0.	1970	0.
1960	111.	1.7.	1072	9 • 0	Å.	1470	200.	-22	21	1972	0.	0.	1970	300.
1484	1.1.7	y .	1976	300	16	1076	200.	-207	22	1974	300.	21.	1975	600.
1990	-193*	12.	1414	2000	10.	1975	400.	-301.	"	1914	3004	L • •	1915	
1991	0.	U.	1974	400.	16.	1976	600.	-12.	21.	1974	600.	22.	1976	900.
1495	0.	υ.	1974	600.	17.	19//	600.	0.	U .	1974	900.	23.	19/0	900.
1993	Ο.	υ.	1974	-120+	16.	1975	600.	0.	0.	1974	-180*	21.	19/5	900.
1994	υ.	ΰ.	1974	-120-	16.	1970	600.	U .	0.	1974	-180.	21.	1976	900.
1995	0.	U •	1974	-150+	16.	1976	600.	0.	0.	1974	-180.	22.	1410	900.
1996	Ο.	ú .	1974	-120.	16.	1976	600.	0.	0.	1974	-180.	22.	1976	900.
1997	Ο.	U.	1974	-120.	16.	1976	600.	0.	0.	1974	-180.	22.	1976	900.
1998	υ.	υ.	1974	-600.	17.	1977	600.	0.	0.	1974	-900 .	23.	1978	900.
1999	J.	J.	1974	Ű.	υ.	1970	600.	0.	0.	1974	0.	Ο.	1970	900.
2000	Ú.	Ú.	1974	U.	0.	1970	800.	Ο.	0.	1974	0.	0.	1970	1200.
2001	0.	υ.	1974	U.	υ.	197%	1000.	Ο.	0.	1974	0.	0.	1970	1500.
2002	0.	υ.	1974	0.	0.	1970	1200 .	Ο.	Ο.	1974	0.	0.	1970	1800.
2003	U.		1974	9.	0.	1970	1200.	0.	0.	1974	0.	0.	1970	1800.
2004	0.	ΰ.	1974	0.	0.	1970	1200.	0.	0.	1974	0.	0.	1970	1800.
2005	Ű.	U .	1974	0.	0.	1970	1600.	0.	0.	1974	Q.	Ο.	1970	2400.
2006	0 -	μ.	1974	0.	0.	1970	2000.	0.	0.	1974	Ú.	0.	1970	3000.
2007	0.		1974	0.	0.	1970	2400.	0.	0.	1974	υ.	0.	1970	3600.
2008	0	0.	1974	Ű.,	0.	1970	2400.	0.	0.	1974	0.	0.	1970	3600.
2000	0		1074	() - () -	0.	1	2400.	0.	0.	1974	0.	0.	1970	3600.
2010	υ.	U.	1974	υ.	0.	1976	2800.	0.	0.	1974	0.	0.	1970	4200.
2411			1076	a	41	1070	2600	•	٥	1974	0.	0.	1970	3900.
2011	.	U •	1074	0.	U .	1070	2000.	U.	0	1974	0.	0.	1970	4500.
2012	.	U .	1974	U •	U .	1970	5000.	U.	.	1974	0	0	1970	4500.
2013	U .	0.	1914	U .	U .	1970		0.	.	1974	0		1070	4500.
2014	U .	0.	1974	U .	U .	1970	6000.	<i>v</i> .	U .	1974		0	1970	9000
2012	υ.	¥ •	1974	9 .	Ű.	1910	6000•	U.	U .	17/4	U.	v.	1910	7 000 •
2016	0.	0.	1974	Û.	0.	1970	9000.	0.	0.	1974	0.	0.	1970	9000.
2017	0.	0.	1974	Ü 🖕	0.	1970	9000.	0.	0.	1974	0.	U.	1410	A000*
2018	ΰ.	U.	1974	0 e	θ.	1970	9000.	Ο.	0.	1974	0.	0.	1970	9000.
2019	0.	0.	1974	0.	0.	1970	9000.	Ο.	٥.	1974	0.	0.	1970	13500.
2020	ΰ.	Ú.	1974	Ú.	0.	1970	9000.	0.	0.	1974	0.	0.	1970	13200.

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TABLE B.14. Early Disposal Scenario, Number of TRU Packages Handled at MRS (June 21, 1982)

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	YEAR P	HULLS & HO	W 2XIU CAN	HÉMOTE H	ZXIJ CAN	REMOTE H S	5 GA DRUM	CONTACT H	4X6X6 BOX	CONTACT H	55 GA DRUH	HOX PLANT	55 G DRUMS
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1981	Ο.	υ.	0.	υ.	0.	٥.	0.	0.	0.	0.	0.	٥.
	1942	0.	ΰ.	· U.	Û.	Ο.	٥.	0.	0.	0.	0.	0.	٥.
	1983	Ú.	0.	0.	υ.	Ú.	0.	0.	0.	0.	0.	0.	0.
1985 0.	1984	Ο.	Ο.	9.	U.	0.	0.	0.	0.	0.	0.	0.	0.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1985	0.	υ.	Ű.	U.	Ŭ.	0.	0.	0.	0.	0.	0.	Ο.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1986	٥.	υ.	U.	υ.	0.	0.	٥.	0.	0.	٥.	0.	0.
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1987	0.	0.	0.	U.	0.	٥.	0.	0.	θ.	0.	0.	0.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1988	υ.	0.	0.	U.	0.	0.	0.	0.	0.	0.	- 0.	U.
1990 \mathbf{e}_{4} \mathbf{y}_{6} \mathbf{y}_{*} 1_{*} \mathbf{y}_{3} 140_{*} 3_{*} 5_{*} 439_{*} 659_{*} 210_{*} 315_{*} 1991 $\mathbf{12e}_{*}$ $\mathbf{14e}_{*}$ $\mathbf{14e}_{*}$ $\mathbf{24e}_{*}$ $\mathbf{41e}_{*}$ 210_{*} 71_{*} 100_{*} 71_{*} 100_{*} 71_{*} 100_{*} 71_{*} 100_{*} 71_{*} 100_{*} 71_{*} 100_{*} 71_{*} 100_{*} 71_{*} $$	1989	θ.	0.	Ű.	υ.	ΰ.	0.	0.	0.	0.	0.	0.	0.
	1990	b4.	¥6.	۶.	14.	93.	140.	з.	5.	439.	659.	210.	315.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1991	128.	172.	14.	28.	186.	279.	7.	10.	A78.	1317.	420.	630.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1995	192.	283.	24.	41.	219.	419.	10.	15.	1317.	1976.	630.	945.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1993	-/3.	-103.	-]0 .	-10.	-106.	-159.	-4.	-6.	-501.	-751.	-239.	-359.
1995 -73 , -109 , -10 , -10 , -106 , -159 , -4 , -6 , -501 , -751 , -239 , -359 , 1996 -73 , -109 , -10 , -106 , -159 , -4 , -6 , -501 , -751 , -239 , -359 , 1996 -73 , -109 , -10 , -106 , -159 , -4 , -6 , -501 , -751 , -239 , -359 , 1997 -10 , -10 , -10 , -106 , -159 , -4 , -6 , -501 , -751 , -239 , -359 , 1998 -19 , -20 , -20 , -20 , -20 , -20 , -20 , -20 , -20 , -239 , -359 , 1999 0.<	1994	-/3.	-109.	-10.	-lo.	-106.	-159.	-4.	-6.	-501.	-751.	-239.	-359.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1995	-73.	-104	-10.	-10.	-106.	-159.	-4.	-6.	-501.	-751.	-239.	-359.
1997 -73 , -109 , -10 , -10 , -10 , -159 , -159 , -4 , -6 , -501 , -751 , -239 , -359 , 1998 1998 -19 , -29 , -32 , -62 , -122 , -132 , -1984 , -63 , 99 , 359 , -359 , -359 , -3200 1999 0 , 0 , 0 , 0 , 0 , 0 , 0 , 0 ,	1996	-73.	-109.	-10.	-10.	-106.	-159.	-4.	-6.	-501.	-751.	-239.	-359.
1998 -1929. -34. -2642. -12. -132198. -6399. 1999 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 2000 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 2001 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 2002 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 2004 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 2005 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 2006 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 2006 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 2006 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 2006 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 2008 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	1997	-73,	-109.	-1V.	-10.	-106.	-159.	-4.	-b.	-501.	-751.	-239.	-357.
1999 $0.$	1998	-19.	-27.	-J.	-+.	-25.	-42.	-1.	-5.	-132.	-198.	-63.	-94.
2000 0. 0	1999	υ.	υ.	Ú.	Ú.	0.	0.	0.	0.	0.	0.	0.	0.
2001 0. 0	2000	٥.	Û.	' U.	V.	Ŭ.	0.	0.	۰.	0.	0.	0.	0.
2002 0. 0	2001	0.	υ.	Ú.	υ.	0.	0.	0.	0.	0.	0.	0.	٥.
2003 0, <	2002	υ.	Ű.	0.	υ.	Ο.	Ŭ.	0.	0.	0.	0.	0.	0.
2004 0. <	2003	0.	υ.	Ο.	υ.	0.	0.	Ο.	υ.	0.	0.	0.	0.
2005 0. <	2004	θ.	Ο.	υ.	Ο.	υ.	٥.	θ.	0.	0.	0.	0.	Ο.
2006 0. <	2005	Ű.	u.	Ú.	Ú.	0.	0.	ΰ.	0.	0.	0.	. 0.	0.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2006	٥.	υ.	0.	υ.	0.	0.	Ο.	0.	0.	0.	0.	٥.
2008 0. <	2007	• 0.	0.	Ο.	υ.	0.	٥.	0.	0.	0.	0.	0.	0.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2008	Ο.	υ.	Ú.	υ.	Ο.	0.	0.	0.	0.	0.	0.	0.
2010 0. <	2009	υ.	0.	0.	υ.	0.	0.	0.	Ο.	0.	0.	0.	0.
2011 0. <	2010	0.	υ.	0.	υ.	0.	٥.	0.	٥.	0.	0.	0.	0.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2011	U.	υ.	Ű.	υ.	0.	0.	υ.	0.	0.	0.	0.	0.
2013 0. <	2012	Ο.	Ú.	υ.	υ.	0.	0.	0.	0.	0.	0.	0.	0.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2013	ΰ.	Ú.	Ú.	Ο.	0.	٥.	0.	0.	0.	0.	0.	0.
2015 0. <	2014	υ.	υ.	ΰ.	υ.	Ο.	υ.	0.	0.	0.	0.	0.	Ο.
2016 U. U. U. U. O. <	2015	0.	U .	0.	Ú.	0.	0.	0.	0.	٥.	0.	0.	0.
2017 0. <	2016	U.	0.	U.	U.	0.	0.	0.	0.	0.	0.	0.	0.
2018 0. <	2017	0	ü.	υ.	υ.	0.	0.	0.	0.	0.	0.	0.	Ú.
2019 0. U. D. U. O.	2018	0.	0.	0.	υ.	0.	0.	0.	0.	0.	0.	0.	0.
	2019	0.	0 .	0	0.	0.	0.	0.	0.	0.	0.	0.	0.
	2020	0.	U.	0.	υ.	0.	٥.	0.	0.	0.	0.	0.	0.

YEAR	DISCHARGE	AR INV	WR2 INV	REPROCESS	DISPOSAL	DISP INV	HLW & H	HLW MRS	DISPOSAL	DISP INV
1981	1090.	/871.	0.	Ú.	0.	0.	0.	0.	0.	0.
1982	1237.	910d.	0.	Ο.	υ.	0.	0.	0.	0.	Ο.
1983	1607.	10715.	0.	Ο.	U.	Ο.	0.	υ.	0.	0.
1984	1744.	12447.	13.	υ.	υ.	0.	0.	0.	0.	0.
1985	2167.	14614.	13.	Ű.	0.	0.	0.	0.	Ο.	0.
1980	2010.	1/121.	116.	Ű.	Ο.	0.	0.	θ.	θ.	0.
1987	2622.	19507.	292.	Ű.	0.	Ü.	Û.	0.	0.	0.
1488	2866.	22190.	530.	Ű.	0.	0.	Ú.	Ο.	0.	0.
1989	3223.	24945.	1003.	θ.	Ű.	0.	Ú.	0.	0.	0.
1990	3071.	27555.	1463.	υ.	υ.	0.	0.	υ.	0.	0.
1991	3078.	JU110.	1987.	U.	U.	0.	. 0.	υ.	0.	0.
1992	3498.	32962.	2633.	υ.	v.	0.	Ű.	Ü.	0.	0.
1993	3428.	35721.	1205.	υ.	J.	0.	υ.	0.	0.	0.
1994	1344.	38110.	4302.	0.	Ú.	0.	Ú.	0.	0.	0.
1495	3574.	40434.	5552.	U.	J.	0.	0.	0.	0.	0.
1996	3410.	42404.	1052.	U.	0.	0.	0.	0.	0.	0.
1497	3448.	44404.	8550.	U.	Û.	υ.	0.	υ.	0.	0.
1998	38/4.	46550.	10278.	υ.	U.	0.	0.	0.	0.	0.
1999	3860.	48456.	12232.	V.	ú.	0.	Ú.	ΰ.	υ.	0.
2000	3964.	50333.	14319.	U.	υ.	0.	0.	υ.	0.	0.
2001	4386.	5232B.	10/10.	Ű.	Ű.	0.	0.	0.	0.	0.
2002	4407.	53949.	19496.	Ο.	Ο.	0.	0.	0.	0.	0.
2003	4569.	55822.	22193.	υ.	υ.	0.	0.	0.	0.	0.
2004	4919.	57654.	29280.	υ.	U.	0.	0.	0.	0.	0.
2105	4841.	59554 .	20221.	υ.	Û.	0.	Ű.	0.	0.	0.
2006	5220.	b1807.	31193.	U.	Ű.	0.	0.	0.	θ.	0.
2007	6081.	64541.	3449].	Ű.	Ű.	0.	0.	0.	0.	0.
2008	604 3 .	67936.	ARECE	Ο.	1800.	1800.	Ű.	0.	0.	0.
2009	6537.	11287.	36/74.	υ.	1800.	3600.	0.	Ű.	0.	0.
2010	o251.	14706.	31006.	J.	1800.	5400.	Ű .	0.	0.	0.
2011	6266.	78370.	34570.	υ.	1800.	7200.	0.	0.	0.	0.
2012	6381.	62377.	31344.	V.	3600.	10800.	0.	0.	0 .	0.
2013	5485.	86358.	35049.	υ.	480U.	15600.	0.	0.	U .	0.
2014	6727.	90962.	32371.	υ.	4800.	20400.	0.	0.	υ.	0.
2015	7033.	95787.	21480.	Ű.	6600 .	27000.	0.	0.	0.	0.
2016	6690.	100221.	23635.	U.	6600.	33600.	υ.	0.	0.	0.
2017	6869.	105269.	1/056.	υ.	7800.	41400.	0.	0.	0.	0.
2018	7258.	110646.	11/38.	υ.	7800.	49200.	0.	0.	0.	0.
2019	0692.	115700.	5571.	U.	7800.	57000.	Ű.	Ú.	Ű.	0.
2020	7046.	119322.	۰.	Ο.	9000.	66000.	0.	0.	0.	0.

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TABLE B.15. Delayed Disposal No Reprocessing Scenario Summary (June 21, 1982)

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repository delivery rates when a full year's production of HLW is held at the reprocessing plant and a portion of it is not yet 10 years old. The TRU capacity requirements are summarized in Table B.17 and the annual handling requirements in Table B.18. The peak rates for the Delayed Disposal case are based on the average removal rates in 2030, 2031, and 2032; however, if a design is modular, it may be desirable to design for a lower rate and add capacity as needed.

TABLE B.17. Required Capacity for TRU Packages at MRS/IS Facility

	Reference	Delayed Reprocessing	Delayed Disposal
Hulls and hardware cans	3,400	0	19,400
RHTRU 2 x 10 ft cans	500	0	2,800
RHTRU 55 gal drums	5,000	0	28,200
CHTRU 4 x 6 x 6 ft boxes	175	0	1,010
CHTRU 55 gal drums	24,000	0	133,000
MOX Plant 55 gal drums	12,000	0	64,000
MOX Plant 4 x 6 x 6 ft boxes	120	0	640

TABLE B.18. Annual Receiving or Removal Rate for TRU Packages at MRS/IS Facility

	Reference	Delayed Reprocessing	Delayed Disposal
Hulls and hardware cans	760	0	1,850
RTHRU 2 x 10 ft cans	110	0	270
RHTRU 55-gal drums	1,100	0	2,700
CHTRU 4 x 6 x 6 ft boxes	40	0	95
CHTRU 55 gal drums	5,200	0	12,500
MOX Plant 55-gal drums	2,500	0	6,000
MOX Plant 4 x 6 x 6 ft boxes	25	0	60

				BWR FUEL							PWR FU	EL		
YEAH	FUEL	STUR	AGE	HLW	STORA	GL	REP PLNT	FUEL	STORA	GE	HLW	STORA	GF	REP PLNT
	TONNE	EXH I	DISCHG	TUNNE	EXP L	ISCHG	POOL INV	TONNE	EXP C	ISCHG	TONNE	EXP D	ISCHG	POOL INV
1981	υ.	U.	1971	Ű.	0.	1970	Ú.	Ο.	0.	1971	0.	0.	1970	0.
1982	0.	υ.	1971	υ.	0.	1970	υ.	0.	Ú.	1971	0.	0.	1970	0.
1983	0.	ΰ.	1971	ΰ.	0.	1970	0.	0.	Ο.	1971	Ο.	υ.	1970	0.
1984	0.	0.	1971	υ.	υ.	1970	υ.	13.	21.	1971	0.	0.	1970	0.
1985	υ.	ŧ+ •	1971	U.	0.	1970	υ .	0.	0.	1971	0.	0.	1970	0.
1986	υ.	U.	1971	υ.	0.	1976	0.	103.	21.	1972	0.	0.	1970	0.
1987	11.	٧.	1972	ΰ.	ΰ.	1976	υ.	165.	53.	1974	υ.	0.	1970	0.
1988	177.	12.	1974	Ú.	0.	1970	υ.	61.	21.	1974	0.	0.	1970	0.
1989	196.	10.	1975	. 0.	0.	1970	0.	277.	21.	1975	0.	0.	1970	0.
1990	108.	1/.	1976	0.	Û.	1970	0.	293.	21.	1976	0.	0.	1970	. 0.
1991	331.	1/.	1977	0.	0.	1970	0.	193.	22.	1976	0.	0.	1970	0.
1992	248.	17+	1977	0.	Ŭ.	1970	0.	398.	23.	1977	0.	Ο.	1970	0.
1993	234.	18.	1978	U.	0.	1970	0.	435.	23.	1978	0.	Ũ.	1970	0.
1994	399.	21.	1,978	Ü 🖕	Ο.	1970	υ.	612.	23.	1979	0.	Ο.	1970	0.
1995	353.	22.	1979	0.	Ű.	1970	Ú.	898.	26.	1980	0.	0.	1970	0.
1996	518.	23.	1980	Ű.	0.	1970	0.	981.	29.	1981	0.	0.	1970	0.
1997	596.	2+.	1981	Ű.	0.	1970	Ú.	900.	30.	1983	Ű.	Ο.	1970	0.
1999	528.	22.	1985	ΰ.	0.	197u	0.	1199.	30.	1984	0.	Ο.	1970	0.
1999	757.	25.	1984	Ű.	0.	1970	ΰ.	1195.	30.	1985	υ.	Ű.	1970	0.
2000	854.	22 .	1985	Ű.	0.	1970	0.	1233.	30.	1986	0.	0.	1970	0.
2001	822.	25.	1480	0.	ΰ.	1970	Ú.	1568.	30.	1987	0.	0.	1970	0.
2002	987.	25.	1987	Ο.	ΰ.	1970	0.	1799.	30.	1988	0.	Ο.	1970	0.
2003	1147.	52.	1986	U.	Ο.	1970	υ.	1550.	30.	1988	0.	0.	1970	0.
2004	1190.	25.	1989	υ.	0.	1970	0.	1898.	30.	1989	0.	0.	1970	0.
2005	1140.	22.	1990	J .	Ű.	197 0	Ű.	1751.	30.	1990	0.	0.	1970	0.
2006	1254.	25.	1991	υ.	υ.	1970	Ű.	1718.	33.	1991	0.	0.	1970	0.
2007	1230.	52.	1992	U.	0.	1970	0.	2068.	35.	1992	0.	٥.	1970	0.
2008	324.	25.	1993	υ.	ა.	1970	0.	573.	35.	1993	0.	0.	1970	0.
2009 -	754.	22.	1994	ύ.	0,	1970	0.	631.	35.	1994	0.	0.	1970	0.
2010	349,	25.	1995	.0.	Ű.	1970	Ű.	683.	35.	1995	0.	0.	1970	0.
2011	330.	25.	1996	Ó.	0.	197u	0.	434.	35.	1995	0.	0.	1970	0.
2012	-424.	16.	1976	Ü.	0.	1970	0.	-802.	21.	1976	0.	V.	1970	0.
2013	-798.	17.	1978	0.	0.	1970	0.	-1498.	23.	1979	0.	0.	1970	0.
2014	-1033.	21.	1960	0.	υ.	1970	U.	-1644.	26.	1981	0.	0.	1970	0.
2015	-1728.	24.	1984	0.	0.	1910	0.	-2663.	30.	1985	0.	0.	1970	0.
2016	-1603.	25.	1986	0.	0.	1970	Ű.	-2741.	30.	1987	0.	0.	1970	0.
2017	-2460.	22.	1988	θ.	0.	1970	υ.	-3519.	30.	1988	0.	0.	1970	0.
2018	-2167.	25.	1990	0.	υ.	1970	0.	-3731.	30.	1990	υ.	0.	1970	0.
2019	-2443.	25.	1992	۵.	υ.	1970	0.	-3725.	33.	1992	θ.	0.	1970	0.
2020	-2264.	25.	1996	ΰ.	0.	197a	0.	-3307.	35.	1995	0.	Ú.	1970	0.

TABLE B.16. Delayed Disposal No Reprocessing Scenario, Fuel and HLW Shipments at MRS (June 21, 1982)

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APPENDIX C

TRANSPORTATION INFORMATION

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APPENDIX C

TRANSPORTATION INFORMATION

Presented in this appendix are standardized bases, requirements and unit costs for transporting spent fuel, solidified high-level wastes, remotehandled transuranic wastes, and contact-handled transuranic wastes as required in the various fuel cycle scenarios. Also presented are the numbers of packages and shipments of each type and the estimated costs for each.

C.1 TRANSPORTATION UNIT COSTS

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This section contains the unit transportation costs used in the preconceptual design studies for the Monitored Retrievable Storage/Interim Storage (MRS/IS) program in FY-82. The bases and assumptions pertaining to transportation for use in the preconceptual design study are also documented in this section. Unit transportation costs are calculated for four fuel cycle materials: spent fuel, high-level wastes (HLW), remote-handled transuranic (RHTRU) wastes, and contact-handled (CH) TRU wastes. RHTRU wastes are further subdivided into three categories: wastes that are packaged in special cylindrical canisters (including compacted cladding hulls), wastes that are packaged in "standard" 210-liter (55 gal) drums with surface dose rates less than 5 R/hr, and drummed wastes with surface dose rates greater than 5 R/hr. Transportation costs are calculated for shipments by truck and by rail.

Three waste management scenarios are currently under study by the MRS/IS program. They include interim storage facilities located either at a fuel reprocessing plant, a geologic waste disposal repository, or a stand-alone facility. The transportation links and the assumed mileages between each facility are defined. Transportation in this study stops at the fences of the terminal facilities; i.e., onsite transportation is considered as facility handling operations. The reference shipping systems for transporting the spent

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fuel and HL and TRU wastes between the facilities are selected. Several criteria were used for selecting these systems, in particular the use of existing or near-existing technology, licensability, and compatibility with reference canister sizes. The reference shipping systems selected for use in this study are shown in Table C.1. The reference canister dimensions are also defined.

Transportation costs for the FY-82 MRS/IS program studies are based on the assumption that private industry will provide the transportation services as a commercial venture, although the services could be owned and provided by the government. Therefore, total transportation costs are the sum of the shipping charges, special equipment and security costs (where applicable) and shipping container rental fees. The unit transportation costs for truck and rail shipments of the six different cargoes are summarized in Table C.2.

Special equipment charges and security costs are currently required for shipments of spent fuel and may be required for shipments of high-level wastes in the future. The costs for HLW shipments shown in Table C.2 include these additional costs.

Introduction

The objectives of the MRS/IS program are to provide Federal contingency capability for storing spent nuclear fuel until a reprocessing facility can eliminate the need for such storage and to provide Federal capability for storing solidified high-level wastes (HLW) and transuranic (TRU) wastes until a waste disposal repository becomes available. Currently, two dry storage concepts are being evaluated to determine their effectiveness for reducing near-term spent fuel and waste storage space shortages. The two concepts consist of storage in large metal casks and drywells. Both concepts offer passive, low cost, easily maintained systems that can be expanded in increments which can be constructed according to demand. The degree of flexibility of these storage concepts is being assessed by comparing the results of using casks and drywells to provide interim storage. The two storage concepts are being evaluated as to their technical status, life cycle costs, safety and licensing issues, environmental issues, transportation considerations, and research and development requirements.

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Material	Shipping Mode	Shipping Container	Canisters per Shipment	Leasing Fee, \$/Day
Spent fuel	Truck	NAC-1	1 PWR or 2 BWR	2000(a)
	Rail	IF-300	7 PWR or 18 BWR	5750
High-level wastes	Truck	NAC-1	1 canister	2000
	Rail	IF-300	5 canisters	5750
RHTRU special canister	Truck	HLW-T	1 canister	1750
	Rail	HLW-R	5 canisters	4375
RHTRU drums <5 R/hr	Truck	CNS 14-170	14 drums	175
	Rail(b)	CNS 14-170	42 drums	525
RHTRU drums >5 R/hr	Truck	CNS 7-100	7 drums	175
	Rail(b)	CNS 7-100	21 drums	525
CHTRU wastes	Truck	TRUPACT	36 drums or 3 boxes	700
	Rail(c)	TRUPACT	72 drums or 6 boxes	1400

TABLE C.1. Reference Shipping Systems Selected for Study

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(a) Leasing fee for the NAC-1 is calculated from a schedule.(b) It is assumed that three of these shipping containers can be transported per railcar.
(c) Assumes two truck TRUPACT versions are transported per railcar.

	Shipping	One-Way Miles, \$/Shipment(b,c)					
Material	Mode	500	2000	2500			
Spent fuel(d)	Truck	12,170	29,010	34,710			
	Rail	91,140	216,920	26,240			
High-level(d) wastes	Truck	12,200		31,510			
	Rail	91,210		262,410			
RHTRU wastes;	Truck	9,280		23,030			
special callisters	Rail	69,670		193,770			
RHTRU wastes;	Truck	3,450		10,825			
	Rail	21,090		57,530			
RHTRU wastes;	Truck	3,380		10,645			
urullis >> K/IIr	Rail	20,770		55,680			
CHTRU wastes	Truck	5,310		14,380			
	Rail	25,600		70,600			

<u>TABLE C.2</u>. Round-Trip Transportation Costs for Truck and Rail Shipments of Spent Fuel and High-Level and Transuranic Wastes^(a)

(a) Transportation costs include shipping charges, special equipment and security costs (where applicable) and shipping system rental fees.

(b) Rounded to the nearest ten dollars.

(c) These costs do not include demurrage fees for truck shipments. These are, on the average, \$29.30 for each hour of turnaround time at the terminal facilities. Rail demurrage fees are calculated using shipping system rental fees.

(d) Costs include charges for special equipment and escort services.

The purpose of this document is to provide standardized assumptions and unit costs for transportation to be used to set a baseline for common comparison of lifetime transportation costs. Unit costs are developed for transporting four types of radioactive materials: spent fuel, solidified high-level wastes, remote-handled transuranic (RH-TRU) wastes, and contact-handled TRU (CH-TRU) wastes. RH-TRU wastes are further divided into special canisters and two types of drummed wastes, so a total of six fuel cycle materials are considered in this study. In addition to transmitting standardized assumptions and transportation unit costs, this report defines the reference transportation systems for the MRS/IS program. Also included is an estimate of the costs of requiring security provisions for high-level waste shipments similar to those required for spent fuel in transit.

Bases_and Assumptions

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The bases for calculating unit transportation costs and key assumptions that were made to facilitate these calculations are discussed in this section. The section includes definition of the transport links connecting the fuel cycle facilities considered in this study. Transportation in this study refers only to offsite shipments, in the general public domain (i.e., between fences of the terminal facilities). Onsite transportation is considered as handling at the facility and is not included here. However, onsite handling of the cross-country vehicles and packagings can affect facility turnaround times and thus the cost of cross-country transport. Shipping parameters and transportation costs for six fuel cycle materials are considered: spent fuel, solidified high-level wastes, RHTRU cladding hulls, other RHTRU wastes, and CHTRU wastes.

At this time in the U.S., no commercial reprocessing of spent nuclear fuel to reclaim valuable uranium and plutonium is occurring. As a result, the spent fuel is being stored in reactor fuel storage basins. The maximum capacity of many of these basins is being reached. The strategy used in the MRS/IS studies assumes that: 1) the government will accept and store excess spent fuel in a federally owned facility until a fuel reprocessing plant (FRP) becomes available; 2) in the reference case, a 1500 MgHM/year FRP will open in 1989 and the MRS/IS will accept and store HL and TRU waste from that operation until a repository is available; 3) the HL and TRU waste generated by the FRP will ultimately be shipped to a repository for final isolation; and 4) a generic mixed-oxide fuel fabrication plant will begin operation in 1989. A gap exists between the 1998 planned opening date for the repository and the FRP opening date of 1989. The HLW and TRU wastes generated during this period will be shipped to an MRS/interim storage facility until they can be shipped to the repository for final isolation.

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Transport links connecting the storage facilities and power reactors are shown in Figure C.1. Co-locating the MRS/IS facility at the repository eliminates transportation of HLW and TRU wastes from interim storage to the repository.

One purpose of this report is to define the reference transportation systems for use in the facility evaluations. There is no intent to endorse or reject any particular shipping system. Reference systems, however, were selected to provide consistency within this study using state-of-the-art hardware. Primarily, the systems selected were existing and licensed where available. If no such systems exist, those that are well along in the design stage were selected. Another criterion that must be met by the shipping system is that of licensability. Application of this criterion requires judgment as to whether or not a conceptual shipping system is expected to eventually meet the packaging regulations in 10 CFR 71.



FIGURE C.1. Transportation Links for Co-locating the Interim Waste Storage Facility with the Repository

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A third criterion concerning the selection of the shipping systems is the sizes of the reference canisters assumed as the primary container for the high-level and transuranic wastes. The reference canister sizes for this study are shown in Table C.3.

The reference shipping systems in this study were selected to accommodate these sizes of canisters. Some inconsistencies may exist between these canisters and the canisters that the FRP is planning to use. For example, the cladding hulls canister the FRP is planning to use is 1.1 m (3.7 ft) in diameter and 2.3 m (7.5 ft) long. This canister, due to its large diameter, was not transportable in any of the spent fuel or high-level waste truck shipping casks. Therefore, to be more compatible with storage and shipping casks, the equivalent volume of waste is assumed to be transported in a larger number of 0.62 m (2 ft) diameter canisters for this study.

TABLE C.3. Reference Canister Sizes and Weights for Definition of Shipping Systems and Shipment Parameters

Fuel Cycle Material	Dimensions, m	Net ^(a) Capacity, m ³ (ft ³)	Average Weight Loaded, kg (1b)
Spent fuel PWR assembly BWR assembly	NA NA	NA NA	658 (1448) 284 (625)
Solidified high-level waste canister	0.31D x 3.1	0.17 (6.0)	1050 (2310)
RHTRU wastes Hulls canister 210 L (55 gal) drum	0.62D x 3.1 0.62D x 0.92	0.75 (2.6) 0.17 (6.0)	3500 (7700)
CH-TRU Wastes 210 L (55-gal) drum Metal box	0.62D x 0.92 1.2 x 1.9 x 1.9	0.19 (6.7) 3.5 (123.6)	300 (660) 4000 (8800)

NA = Not applicable.

(a) Based on maximum of 80 percent full.

A key assumption that simplifies the selection of the shipping systems is that the canister provides the second level of containment for plutonium bearing wastes, as required in federal regulations (10 CFR 71). The casks or shipping packagings provide only one level of containment. A final assumption concerning selection of the truck shipping systems is that they will all be legal-weight systems, i.e., gross-vehicle weight (tractor plus trailer plus loaded cask weights) do not exceed 36,400 kg (80,000 lb). It is recognized that over-weight truck shipments may be more economical than legal-weight shipments, but for this study, there was insufficient time to adequately calculate the charges for over-weight shipments. This would include defining specific routes and finding what each state on each route charges as an over-weight penalty. In addition, the use of overweight trucks routinely for numerous shipments would require considerable administrative efforts to obtain repeatedly the special permits from the states involved.

Shipping distances must be defined to calculate transportation costs. For the purposes of this study, two distances that represent somewhat bounding cases are defined. The first distance is 4000 km (2500 miles), which represents a cross-country shipment. The second distance is 800 km (500 miles), which was chosen because it approximates a typical distance between eastern power reactors and BNFP. The cost for each transport link in the evaluation studies of three sites for MRS/IS facilities is calculated using both of these distances.

The assumed distances must be assigned to the various transportation links in Figure C.1. Since most of the commercial reactors are in the east and the FRP will be in the east, the transportation link connecting these facilities is assumed to be 800 km (500 miles). The disposal repository is assumed to be in the west, which results in the 4000 km (2500 mile) transport distance between the FRP and repository and the MOX-FFP and repository. The MRS/IS facility is also assumed to be 4000 km from the reactors.

It is assumed in this study that 50 percent of the spent fuel and waste transported to the MRS/IS facility is to be shipped by truck and 50 percent by rail. This shipping mode split was chosen because it is not clear what mode

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of transport will be most extensively used in the future. Each has its own advantages and disadvantages. The reference truck/rail shipping split reflects no bias toward either mode.

Mid-year 1982 dollars were used when calculating transportation unit costs. Transportation costs are calculated as though private industry was shipping on a commercial basis even though that may eventually not be the case. Costs include operating costs plus amortization costs of hardware plus profits, at commercial rates. Therefore, transportation costs include the shipping charges assessed by carriers and the rental fees assessed by transportation hardware suppliers. A third factor in transportation costs is a fee for demurrage or detention of a carrier's equipment (railcars or truck-trailer rigs) and for drivers while unloading at terminal facilities. These three transportation factors are assumed to be supplied by the private sector as a commercial venture. Thus the total transportation costs are calculated as follows:

			Special		Shipping		
Total	Round-trip		Equipment/		Container		Demurrage
Transportation =	Shipping	+	Security	+	Leasing	+	Fees
Costs	Charges		Costs		Fees		

Transportation System Descriptions

This section describes transportation systems selected for this study for the five fuel cycle materials under consideration in this study: spent fuel, solidified HLW, TRU-contaminated fuel cladding hulls, other RHTRU wastes, and CHTRU wastes. Two shipping systems, one truck version and one rail version, are described for each material. It is believed that the future nuclear waste management system will integrate their waste container designs with transportation system designs to provide compatible and optimum shipping configurations. Therefore, if a minor modification to the shipping containers results in significantly increased capacities, it is assumed this will be done. These modifications are noted where they occur.

Table C.4 lists the important shipping parameters and characteristics of the truck and rail shipping systems used in this study. Supplementary descriptive information is contained in the following sections.

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Fuel Cycle <u>Material</u>	Shipping Container Designation	Transport Mode	Shipment Capacity	External Dimensions, m	Cargo Compartment Dimensions, m	Thermal Limit, kW	Shiel Material	ding Equiv. Stl. Thick, cm	Weight, kg	Gross Vehicle Weight, kg Loaded
Spent fuel	1F-300	Rail	7 PWR or 18 BWR elements	1.91D × 5.03 PWR 5.28 BWR	0.95D x 4.25 PWR 4.57 BWR	61.5 Wet 11.7 Dry	U/St/H ₂ 0	37	63,490	119,270
	NAC-1	Truck	1 PWR or 2 BWR elements	1.27D x 5.13	0.34D x 4.52	2.5 Dry 11.5 Wet	Pb/St/H ₂ O	27	22,660	33,200
Solidified HLW(b)	1F-300	Rail	5 canis- ters of HLW glass	1.91D x 5.28	0.95D x 4.57	61.5 Wet 11.7 Dry	U/St/H ₂ O	37	63,490	119,270
	NAC-1	Truck	1 HLW canister	1.27D x 5.13	0.34D x 4.52	2.5 Dry 11.5 Wet	P/St/H ₂ O	27	22,660	33,200 ^(b)
Canistered RH-TRU	HLW-R(d)	Rail	5 canis- ters	2.69D x 3.84	2.25D x 3.20	2.7 Dry	Al/St	23	52,150	119,600
Wastes	HLW-T(d)	Truck	l canis- ter	1.26D x 4.12	0.83D x 3.43	0.5 Dry	Al/St	15	11,700	33,000
RH-TRU wastes(e) <5 R/hr	CNS 14-170(f)	Rail	42 drums	2.1D × 2.2	1.9D x 1.9	NA	Pb/St	5.4 (Pb)	15,400 (each CNS 14-170)	97,000
	CNS 14-170	Truck	14 drums	2.1D x 2.2	1.9D x 1.9	NA	Pb/St	5.4 (Pb)	15,400	35,500
RH-TRU wastes(e) >5 R/hr	CNS-7-100(f)	Rail	21 drums	2.2D x 1.4	1.9D x 1.1	NA	Pb/St	8.9 (Pb)	16,100 (each CNS 7-100)	93,000
	CNS-7-100	Truck	7 drums	2.2D x 1.4	1.9D x 1.1	NA	Pb/St	8.9 (Pb)	16,100	34,100
CH-TRU wastes(g)	TRUPACT	Rail	72 drums or 6 boxes	2.4 x 2.7 x 7.5	NA	NA	Essentially	None	10,000 (each TRUPACT)	83,000
	TRUPACT	Truck	36 drums or 3 boxes	2.4 x 2.7 x 7.5	1.8 x 2.1 x 5.6	NA	Essentially	None	10,000	33,000

TABLE C.4. Characteristics of Transportation Systems for the MRS/IS Program

NA = Not Available.

(a) Gross vehicle weights include cooling systems, tie-down systems, transport vehicles and other miscellaneous equipment.
 (b) Solidified HLW are assumed to be packaged in 0.3 m (1 ft) diameter by 3.1 m (10 ft) long stainless steel canisters.

(c) Cladding hulls are assumed to be treated to reduce volumes and placed inside stainless steel canisters measuring 0.6 m (2 ft) in diameter by 3.1 m (10 ft) long.

(d) Cask designed for transportation of defense HLW by the General Atomic Co. for the DOE.

(e) Assumed to be packaged in 210 L (55 gal) steel drums.

(f) Truck and rail containers are identical. Three can be shipped per railcar; one per truck.

(g) Assumed to be packaged in 210 L (55 gal) drums or 1.9 m x 1.3 m x 0.95 m (6.2 ft x 4.2 ft x 3.1 ft) modular boxes. TRUPACT = Transuranic Package Transporter. Rail TRUPACT is assumed to be identical to truck version. One TRUPACT is shipped per truck trailer and two per railcar.

(h) It is assumed that the modification required in this cask to transport HLW can reduce the cask weight enough to keep this a legal-weight truck shipment, e.g., drainage of the neutron shield tank.

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Spent fuel Shipping System

The representative truck and rail shipping systems used in this study are the NAC-1 owned by the Nuclear Assurance Corporation and the IF-300 owned by the General Electric Company, respectively. The NAC-1 and IF-300 shipping casks are depicted in Figures C.2 and C.3, respectively. The NAC-1 legal weight truck system uses a water-filled cask designed to transport one PWR or two BWR spent fuel assemblies. Decay heat from the spent fuel is removed by conduction and natural convection through the cask body and is released to the atmosphere by natural convection and radiation. The NAC-1 is currently shipped at a reduced heat loading.

The IF-300 cask of General Electric Company is a water-filled cask (although it is currently shippped dry), designed for rail transport of 7 PWR or 18 BWR spent fuel assemblies. Decay heat is removed from the fuel by natural circulation of the coolant (water, when used), by natural convection and conduction to the external surface, and by forced convection from the external surface to the environment. The forced convection (air impingement) system consists of two diesel-driven blowers and appropriate air ducts. In addition, the cask outer surface is corrugated to facilitate external cooling. The maximum heat-rejection capacity is 76 kW with blowers operating and 62 kW without blowers.

High-Level Waste Shipping Systems

Transportation systems for solidified high-level wastes have been conceptually designed but not built. These systems are expected to resemble the current generation of spent fuel shipping casks. Therefore, the shipping systems previously described for transport of spent fuel are also assumed to be used to transport high-level wastes in this study. Some minor modifications to the spent fuel casks are required, e.g., designing a new internal basket for the IF-300 with a capacity for five HLW canisters, but it is assumed that these casks would be licensable for HLW shipments by using appropriate baskets and spacer inserts. The only change to the "cask characteristics" is the cargo weights. It is recognized that the NAC-1 and IF-300 are not optimized for transporting high-level wastes and that future transportation systems may have higher cargo capacities for a given gross weight.





FIGURE C.3. IF-300 Rail Spent Fuel Shipping Cask

RHTRU Waste Shipping Systems

Different shipping systems are required to transport "standard" 55 gal drums and other special canisters for RHTRU wastes. Special canisters (0.62 m in diameter and 3.1 m long) are assumed to be transported in casks currently designated HLW-T and HLW-R for truck and rail versions, respectively. These casks are being designed by the General Atomic Company to transport defense high-level wastes for the DDE. They are assumed in this study to be licensable for transporting commercial RH-TRU wastes. The HLW-T cask is a thick-walled steel cylinder similar to the current generation of spent fuel truck casks. This cask can accommodate one special canister. The HLW-R cask is a cylindrical, solid steel cask capable of transporting five canisters. Conceptual drawings of these casks are shown in Figures C.4 and C.5, respectively.

RHTRU wastes are also packaged in standard 55-gal drums, having various dose rates from 200 mR/hr to several hundred R/hr. To make the economics of transport more realistic for the additional shielding needs, two shipping containers with different features are assumed to be used. For RHTRU waste drums with surface dose rates less than 5 R/hr, the shipping container selected is the Chem-Nuclear Systems, Inc. cask designated CNS 14-170 (Figure C.6 shows a drawing of the CNS 14-170). This is a top-loading, lead and steel shipping cask for dewatered or solidified waste material. It is assumed to be licensable for transportation of TRU wastes.

RHTRU waste drums with surface dose rates exceeding 5 R/hr are assumed to be shipped in the CNS 7-100 cask. The maximum dose rate for drums in the CNS 7-100 is 100 R/hr. Any exceeding this value are assumed to be shipped in the HLW-T and HLW-R casks. The CNS 7-100 is a lead and steel shipping cask (Figure C.7) currently used to transport dewatered or solidified waste material. It is also assumed to be licensable for transporting transuranic wastes.


FIGURE C.4. Reference Truck Cask for Transportation of Hulls Canisters (HLW-T cask)



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FIGURE C.5. Reference Rail Cask for Transportation of Hulls Canister (HLW-R cask)



FIGURE C.6. CNS 14-170 Shipping Container

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FIGURE C.7. CNS 7-100 Shipping Cask

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CHTRU Waste Shipping Systems

The <u>TRansUranic PACkage Transporter</u> is the reference CHTRU waste shipping system selected for use in this study. The TRUPACT is being developed by the Sandia National Laboratories/Transportation Technology Center and the General Atomic Company for the DOE specifically to provide the containment required to haul large quantities of defense CHTRU wastes. Both truck and rail versions of the TRUPACT are being developed. However, because there are more uncertainties about the availability of a rail version, the TRUPACT system used for rail transport in this study consists of two truck versions shipped on a railroad flatcar. The truck system consists of a single TRUPACT shipped on a flatbed truck trailer.

As presently conceived, the TRUPACT (Figure C.8) will have inner and outer steel frameworks made of rectangular tubing. Steel sheets covering the inner and outer surfaces of the inner and outer frameworks are separated by about 0.3 m (12 in.) of high-temperature insulation and rigid polyurethane foam.

The inner liner is built of stainless steel sheets; the outer shell may be carbon steel or stainless steel. A steel puncture-resistant plate is located between the two frameworks to prevent puncture damage to the inner liner. Access to the cargo cavity is through two hinged, sealed closures in series at one end that are bolted in place during transport.

Unit Transportation Costs for MRS/IS

The bases for the various elements of transportation costs are given in this section. The cost elements include shipping charges, special equipment and security charges, shipping container leasing fees, and demurrage fees. Total transport costs are provided at the end of this section.

The actual fee charged by a truck or rail carrier to transport spent fuel, high-level wastes, or transuranic wastes cannot be determined until a contract is negotiated. These charges are based on several conditions, including shipment origins and destinations, shipment weight, shipment size,



FIGURE C.8. TRUPACT Truck Version. One TRUPACT is shipped per rail truck and two are shipped per rail car.

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the route, volume shipped, frequency of shipments, and the existing competition. Fortunately, basic shipping charge structures for these materials do exist in various forms in the U.S. Shipping container rental fees are based on personal contacts with cask suppliers. The purpose of this report is to provide transportation unit costs for the aforementioned materials to be utilized in the preconceptual designs of MRS/IS facilities.

Charges for Shipments by Truck

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The truck shipping charges included in this report are from a single carrier (Tri-State Motor Transit Co. 1981). This carrier services the 48 contiguous states and has the capability to comply with NRC requirements for shipping spent fuel. Since transportation requirements for spent fuel are the most stringent, it is expected that this carrier can also comply with the regulations for shipping HL and TRU waste. In addition, the use of a single carrier provides a uniform basis for calculating truck shipping charges.

Basic charges for shipping spent fuel and wastes with legal-weight and legal-dimension vehicles do not vary across the country. Basic weight and dimension charges for spent fuel, high-level wastes and transuranic wastes are shown in Table C.5.

In addition to the charges listed in Table C.5, other charges are imposed on shipments of spent fuel and potentially will be imposed on HLW shipments. If a shipment requires specially equipped vehicles and specially trained personnel, as specified in NRC regulations (10 CFR 73), an additional charge per loaded mile will be imposed on shipments. The regulations require that these shipments must be scheduled, in writing, at least seven days in advance. If a shipment is cancelled or rescheduled during that seven-day period, a \$1000 fee is charged. When the carrier is required to furnish armed driver(s) or escort(s), an additional charge is assessed. If a separate escort vehicle is required or necessary, another fee is added to the shipping charge.

······································	Rates	in Dollars	per 100 Pounds ⁽	b)	<u> </u>
Miles- Not Over	<u>Full</u>	Empty	Miles- Not Over	Full	Empty
100	1.52	.98	950	4.68	3.71
110	1.60	.99	975	4.76	3.81
120	1.61	1.03	1000	4.84	3.89
130	1.65	1.06	1025	4.93	4.01
140	1.71	1.08	1050	5.10	4.10
150	1.77	1.10	1075	5.20	4.17
160	1.84	1.11	1100	5.35	4.27
170	1.90	1.14	1125	5.45	4.42
180	2.02	1.17	1150	5.56	4.48
190	2.07	1.21	1175	5.72	4.56
200	2.16	1.24	1200	5.80	4.68
225	2.23	1.31	1225	5.94	4.76
250	2.35	1.39	1250	6.07	4.87
275	2.42	1.40	1275	6.19	4.96
300	2.49	1.45	1300	6.31	5.08
325	2.59	1.56	1325	6.41	5.15
350	2.68	1.60	1350	6.57	5.25
375	2.73	1.61	1375	6.66	5.36
400	2.83	1.65	1400	6.79	5.45
425	2.94	1.77	1425	6.91	5.54
450	3.02	1.82	1450	7.01	5.63
475	3.09	1.90	1475	7.17	5.75
500	3.19	1.97	1500	7.27	5.82
525	3.24	2.12	1525	7.38	5.95
550	3.32	2.20	1550	7.53	6.05
575	3.44	2.29	1575	7.63	6.12
600	3.51	2.39	1600	7.77	6.21
625	3.60	2.50	1625	7.90	6.33
650	3.67	2.62	1650	7.98	6.41
675	3.76	2.66	1675	8.13	6.52
700	3.84	2.72	1700	8.24	6.61
725	3.93	2.89	1725	8.35	6.79
750	4.01	2.98	1750	8.49	6.87
775	4.08	3.03	1775	8.59	6.98
800	4.16	3.11	1800	8.73	7.11

TABLE C.5.	Truck Shipping Charges for Spent Fuel and High-Level
	Wastes (Tri-State Motor Transit Co. 1981 ^(a)

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	Rates	in Dollars	per 100 Pounds ⁽	Ь)	
Miles- Not Over	Full	Empty	Miles- Not Over	<u>Full</u>	Empty
825	4.26	3.22	1825	8.84	7.17
850	4.31	3.30	1850	8.96	7.25
875	4.44	3.39	1875	9.08	7.37
900	4.49	3.50	1900	9.23	7.50
925	4.57	3.63	1925	9.34	7.57
1950	9.43	7.64	3200	15.53	12.55
1975	9.60	7.76	3250	15.77	12.78
2000	9.68	7.84	3300	16.02	12.92
2025	9.83	7.93	3350	16.22	13.14
2050	9.94	8.65	3400	16.49	13.35
2075	10.07	8.16	3450	16.74	13.53
2100	10.19	8.24	3500	16.98	13.72
2125	10.30	8.32	3550	17.20	13.91
2150	10.40	8.44	3600	17.45	14.12
2175	10.56	8.53	3650	17.69	14.33
2200	10.67	8.65	3700	17.95	14.48
2250	10.92	8.82	3750	18.18	14.74
2300	11.16	9.04	3800	18.42	14.92
2350	11.40	9.23	3850	18.64	15.11
2400	11.65	9.42	3900	18.92	15.29
2450	11.91	9.62	3050	19.16	15.50
2500	12.10	9.83	4000	19.41	15.69
2550	12.35	10.00	4050	19.63	15.92
2600	12.60	10.21	4100	19.87	16.09
2650	12.85	10.39	4150	20.10	16.29
2700 2750 2800 2850 2900	13.09 13.34 13.57 13.83 14.05	10.61 10.77 11.00 11.18 11.39	4200 4250 4300	20.38 20.61 20.84	16.48 16.65 16.87
2950 3000 3050 3100 3150	14.32 14.52 14.79 15.03 15.27	11.53 11.78 11.96 12.12 12.32			

TABLE C.5 (contd)

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⁽a) Updated April 22, 1982.
(b) Source: Tri-State Motor Transit Co., Docket MC-109397. Item No. 200, First Revision.

NRC regulations (10 CFR 73) state that a spent fuel transport vehicle within a heavily populated area must be occupied by at least two individuals, one of whom serves as an escort. It must be escorted by an armed member of the local law enforcement agency or by a vehicle ahead and one behind, each of which contains at least one armed guard. A spent fuel transport vehicle not within heavily populated areas must be occupied by at least one driver and one escort, or occupied by one driver and escorted by a separate vehicle occupied by at least two escorts, or escorted as required for transport vehicles in heavily populated areas. It is not known at this time whether high-level waste shipments will require these security considerations, but such is assumed here. For this study, security costs are assumed to include one driver and one escort.

The Code of Federal Regulations does not reference security clearance requirements for drivers or escorts. However, if clearances are required, an additional charge will be assessed. These charges are not included in the transportation costs.

A fuel use surcharge was assessed in the past on top of all other charges and surcharges per shipment. This charge was adopted in 1979 when fuel costs became unstable. However, this surcharge has recently been incorporated into the basic shipping charges shown in Table C.5. Many other charges can apply if any deviations occur in the original route, schedule, delivery acceptance, or in-transit stops, but these are ignored in this study.

Summarized in Table C.6 are the additional fees or surcharges that are imposed on spent fuel shipments and assumed here to be imposed on HLW shipments.

A final fee charged by truck carriers is a charge for their equipment being idle at the terminal facilities while the shipping container is being loaded, unloaded, or held up by the facility operator. Drivers are assumed to deliver their shipment, wait for it to be unloaded, and then depart with the same shipping system they arrived with. Typically, this demurrage fee is negotiated prior to the shipment and the actual fee varies between contracts.

TABLE C.6. Truck Surcharges for Spent Fuel and High-Level Waste Shipments

Type of Charge	Cost	NRC Requirement
Special equipment	\$0.92 per loaded mile	Х
Armed driver/escort	\$0.20 per mile	X
Separate escort vehicle	\$1.28 per mile ^(a)	х ^(b)
"L" cleared driver	\$0.12 per mile	
"Q" cleared driver ^(c)	\$0.15 per mile	

- (a) Total miles are normally based on special equipment and personnel domiciled at Joplin, Missouri. Mileages are computed to point of origin of shipment, then through to the destination, then back to domicile point of shipment. Mileages to Joplin, Missouri, are not included for simplification purposes.
- (b) Required in heavily populated areas.

(c) Each additional "Q" cleared driver is a fixed charge of \$200 per shipment.

This fee is assessed to compensate for idle equipment and the driver's wages and living expenses while the truck is not with a load. To keep additional calculations as simple as possible, the average fee per hour (based on 24 hours demurrage using a schedule from Tri-State Motor Transit Co., Docket No. MC-109397, Item No. 500) will be utilized. From this basis, the demurrage fee used in this study is \$29.30 per hour.

Charges for Shipments by Rail

Rail shipping charges are much more complicated than truck shipping charges. Rail charges are often not uniform with the distance traveled and can be affected by topography, state regulations, competition, and the route traveled. It is assumed in this study that Special Trains^(a) will not be used, so the rail shipping charges that are developed are for general freight service.

⁽a) Special Trains are defined as trains made up solely for the shipment of one commodity or for one shipper.

Shipping charges assessed by rail carriers are specific for each origin-destination combination. Each origin and destination lies in a particular "rate-basing area" which is a major rail point where branch lines connect to local towns or communities. The shipping charges are assessed for transporting a commodity between specific rate-basing areas, regardless of the route or mileages traveled. Therefore, there is no such thing as a "generic" rail shipping charge. Specific origin-destination combinations must be defined. To obtain meaningful cost numbers for this study, charges were obtained for transporting radioactive materials between the locations shown in Table C.7. Shipping charges are the same regardless of the direction the materials were being transported; i.e., east to west or west to east. Also shown on this table are the approximate mileages between each location and the approximate transit times. Note that in some cases, especially in long hauls, the mileages and charges quoted may be the same for two different shipment origins. This is because shipping charges are established between rate-basing areas regardless of the route or distance traveled. The rail transit times are the hardest to define with any certainty. Too many variables are involved between any origin/destination combination to obtain a precise value. The times reported in Table C.7 are based on past experience and judgment for the areas and/or routes involved.

The charges for general freight service for spent fuel and HL and TRU wastes are somewhat uniform when based on the mileages shown in Table C.7. Curves showing the shipping charges (per 100 lb) as a function of one-way miles are shown in Figure C.9 for loaded and empty containers. Minor variations are evident between shipments entirely within the East and entirely within the West. It appears that western shipments have higher charges, but there are too few data points to establish a conclusive pattern.

Rail shipments of spent fuel require security provisions as do truck shipments. Rail shipments within heavily populated areas must be accompanied by two armed escorts that may or may not be members of a local law enforcement agency. A shipment not within a heavily populated area must be accompanied by at least one escort (10 CFR 73).

From (Origin)	To (Destination)	Dollar 100 p Loaded	s per ounds Empty	Approximate One-way Mileages	Approximate One-way Transit Time (Days)
Hanford, WA	Barnwell, SC	16.89	15.83	2700	12–15
Mercury, NV	Barnwell, SC	16.89	15.83	2200	10-13
Berwick, PA	Barnwell, SC	7.13	6.69	750	5–7
Palo, IA	Barnwell, SC	8.82	8.27	1050	9–12
Port Gibson, MS	Barnwell, SC	6.79	6.37	700	6–8
Waterford, CT	Barnwell, SC	7.88	7.39	900	8-11
Eureka, CA	Barnwell, SC	19.15	17.95	2950	12-15
Hanford, WA	Mercury, NV	11.09	10.40	1000	9–12
Berwick, PA	Mercury, NV	16.89	15.83	2400	12-15
Palo, IA	Mercury, NV	13.39	12.55	1500	10-13
Port Gibson, MS	Mercury, NV	14.78	13.86	1600	10-13
Waterford, CT	Mercury, NV	16.89	15.83	2650	12–15
Eureka, CA	Mercury, NV	9.25	8.67	800	7–9
Rainier, OR	Hanford, WA	5.22	4.90	300	3–5
Satsop, WA	Hanford, WA	5.03	4.72	350	4–7
Eureka, CA	Hanford, WA	10.86	10.18	1200	7–9

TABLE C.7. Rail Shipping Charges, Distances, and Transit Times for Several Origin/Destination Combinations

Source: Personal communication with Mr. Frank Votaw, Rockwell, Hanford Operations, Traffic Division, Motor Rates and Routes.

Rail carriers have no provisions to supply an armed escort service, and it is expected that this service will be provided by the shipper. Rail carriers have indicated they will supply a car or caboose for the escorts to ride in. The charge for this service would be the price of a coach-class passenger ticket, or approximately 9 cents per mile per escort.^(a)

(a) B. M. Cole. 1981. <u>Shipping Charges for LWR Spent Fuel</u> (letter report to John Cashwell, Sandia National Laboratories). Pacific Northwest Laboratory, Richland, Washington.

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FIGURE C.9. Rail Shipping Charges for Loaded and Empty Shipments

The total security costs must also include the wages and living expenses of the escorts. The charge for rail escorts can be estimated by using the truck charge of 20 cents per mile as an index. A truck with two drivers can travel about 900 miles in one day. The salary and expenses per escort is thus \$180 per day. At least two escorts per trip are required so that the shipment can be constantly under surveillance. Using the approximate mileages and transit times shown in Table C.7, the average distance travelled per day by rail is 119 miles, which works out to an average speed of 5 miles per hour.

This average makes the charge for rail escort service about \$1.50 per escort per mile or \$3.00 per mile for continuous surveillance. Adding the cost of the coach-class passenger ticket for each escort brings the total for rail escort service to about \$3.18 per mile.

Demurrage charges for rail shipments are included in the shipping system rental fees. This is because there are no guards or drivers who must wait for the shipping system to be loaded or unloaded. Demurrage charges for the transport vehicle (rail car or flatbed trailer) are included in the rental fees.

Shipping Container Rental Fees

One basis for this study is that transportation services for spent fuel, HL and TRU wastes will be supplied by private industry as a commercial venture. Therefore, the total transportation costs must include a fee for rental or lease of the shipping containers from their suppliers. These additional costs include operating costs, amortization of transport hardware, and profits. These costs would be calculated differently if, in the future, the U.S. Government decides to procure and operate its own transportation hardware.

Rental fees charged by shipping container suppliers are a negotiable item that can vary in each contract. These cask use and service charges include some field services, training, and maintenance of equipment in addition to operating and amortization costs and profits. Typical rental fees for the shipping system used in this study were obtained from contacts with the supplier companies. The reference rental fees are shown in Table C.8. Use and service charges for conceptual transportation equipment (i.e., HLW-T, HLW-R, and TRUPACT) are assumed to be the same portion of the capital costs as those for the equipment currently in use. It should be noted that the use and service charges shown in Table C.8 are based on short-term leases and are not the charges that would be assessed if the shipping containers were leased for a year or longer. Long-term use of shipping containers would result in significantly lower use and service charges than those shown in Table C.8.

		Single Ship	ment Cost, \$
Shipping Container	Charge, \$/Day	500 One-Way Miles	2500 One-Way Miles
G.E. IF-300	5,750(a)	57,500	184,000
NAC-1	2,000 ^(b)	6,000	16,000
HLW-T	1,750(c)	5,250	14,000
HLW-R	4,375(d)	43,750	140,000
CNS-7-100	175/container	525(T) ^(f) and 5250(R)	1,400(T) and 16,800(R)
CNS-14-170	75/container	525(T) and 5,250(R)	1400(T) and
TRUPACT	700/container(e)	2,100(T) and 14,000(R)	5,600(T) 44,800(R)

TABLE C.8. Shipping Container Rental and Service Charges (Mid-1982 Dollars)

- (a) Based on truck and round-trip transit times of 3 and 8 days and rail transit times of 10 and 32 days for 500 and 2500 one-way mile trips, respectively.
- (b) Calculated from first 30 days of use in schedule below:

1-1030,00011-30ADD31-90ADD1100/da	No. Days of Use		Charge
91-180 ADD 900/da over 180 ADD 800/da	1-10 11-30 31-90 91-180 over 180	ADD ADD ADD ADD	30,000 1500/day 1100/day 900/day 800/day

- (c) Fabrication costs for HLW-T cask are estimated at about \$1 M. This is a conceptual cask system, and rental fees have not been calculated. The value in this table was calculated as follows. The estimated fabrication costs of the CNS-14-170 is \$100,000. Assume the same ratio of fabrication costs to rental fee for HLW-T cask.
- (d) Fabrication costs for HLW-R cask are estimated at about \$2.5 M. See footnote (c) for rental fee calculation.
- (e) Fabrication costs for TRUPACT are estimated at about \$400,000. See footnote (c) for rental fee calculation.
- (f) (T) = Truck, (R) = Rail.

One factor that may tend to balance this effect is that the rental fees reported do not include fabrication of new equipment (that is, these fees are based partially on recovering the capital costs of equipment fabricated several years ago). The costs of fabricating new equipment have increased significantly, and therefore the rental fees charged by suppliers will most likely increase.

Calculation of Unit Transportation Costs

The final information required for transportation costs is the average weights of shipments or the average commodity (i.e., waste plus canister) unit weights. For the materials in this study, the average commodity unit weights are expressed in kilograms. Transportation unit costs will be expressed primarily in dollars per shipment for each type of waste and shipping system.

The average commodity unit weights for the high-level waste, RH-TRU waste special canister, and RHTRU waste drum shipping containers are straightforward because they haul only a single type of waste container. Their average commodity unit weights are calculated by multiplying the capacity of the shipping containers (see Table C.4) by the average weights of the loaded waste canisters (see Table C.3). To develop the average commodity unit weight for spent fuel truck shipments, the information in Tables C.3 and C.4 is used. Also, since about two-thirds of the commercial reactors are PWRs, an estimated two-thirds of the shipments will be PWR fuel elements. This ratio provides an average commodity weight of 628 kg (1385 lb) for truck shipments and 4775 kg (10,500 lb) for rail shipments. Similar procedures were used to calculate the average commodity weights for the TRUPACT. The ratio of drum shipments to box shipments was calculated from data derived by Fletcher^(a) from estimates of waste quantities and characteristics from the Barnwell Nuclear Fuel Plant.^(b) The average commodity weights and empty and loaded shipping container weights used to calculate transportation unit costs are shown in Table C.9.

(b) W. H. Carr (Draft). 1982. Estimation of Waste Types, Characteristics, and Quantities from the Barnwell Nuclear Fuel Plant. ONWI/3092/TOP-01. Allied-General Nuclear Services, Barnwell, South Carolina.

⁽a) See Appendix B.

Material/ Shipping Container	Average Commodity Weight, kg/Shipment	Shipping C Weight Empty	ontainer , kg Loaded
Spent fuel IF-300 NAC-1	4,775 628	63,490 22,660	68,265 23,288
High-level wastes IF-300 NAC-1	5,250 1,050	63,490 22,660	68,740 23,710
RHTRU canisters HLW-R HLW-T	17,500 3,500	52,150 11,700	69,650 15,200
RHTRU drums (<5 R/hr) CNS 14-170 (R) ^(a) CNS 14-170 (T)	12,600 4,200	46,200 15,400	58,800 19,600
RHTRU drums (>5R/hr) CNS 7-100 (R) CNS 7-100 (T)	6,300 2,100	48,300 26,100	54,600 18,200
CHTRU wastes TRUPACT (R)(b) TRUPACT (T)	21,950 9,610	20,000 10,000	41,950 19,610

TABLE C.9. Average Commodity Weights and Empty and Loaded Shipping Container Weights Used In Transportation Unit Cost Calculations

(a) Rail version consists of three shipping containers, transported on a railcar. Reported weights include this factor.

(b) Two TRUPACTs shipped per railcar. Reported weights include this factor.

Figures C.10 and C.11 show the transportation costs for each type of shipment under consideration in this study for truck and rail shipments, respectively. Each curve represents a different type of shipment. All curves represent the sum of the truck or rail shipping charges, cask use and service charges, and security costs (if applicable). These curves were drawn by plotting two points, one at 800 km (500 miles) and one at 4000 km (2500 miles).





Therefore the uncertainty of these curves increases with the distance along the curve from these points. Care must be taken when using these data due to the many assumptions and uncertainties outlined throughout the text. Note that the unit transportation costs in these figures are the costs per shipment. To convert these costs to dollars per kilogram (waste plus canister), the appropriate factors can be found in Table C.5. Demurrage charges for truck shipments must be added to the total shipments costs by applying the charge rate previously reported to the facility turnaround times.

Special equipment charges and security costs are included in the curves for spent fuel and high-level waste shipping costs. If these additional charges are later determined to be not required for high-level waste shipments, the transportation costs for truck shipments would be reduced by 14 percent and 19 percent for 500 mile and 2500 mile one-way trips, respectively. The corresponding reductions in rail costs for 500 and 2500 one-way mile trips are 5 percent and 7 percent, respectively.

C.2 COST ESTIMATES FOR SPECIFIC SCENARIOS

The transportation costs developed for the MRS/IS facility co-located with a repository are presented in this appendix. The transportation costs are assessed only for offsite shipments, i.e., costs for onsite transfer of wastes from the MRS/IS facility to the disposal repository are not included. Throughput quantities for each of the waste forms considered in this study are obtained from Appendix B. The calculated throughput volumes are shown in Tables C.10 to C.14 for each fuel cycle scenario. Transportation unit cost data are from Subsection 3.5 of the main report. These data are used to develop the transportation costs for each year of MRS/IS facility operation.

The annual throughputs presented in Tables C.10 through C.14 are summed to provide the cumulative waste form storage requirements for the MRS/IS facility, for each scenario, in Tables C.15 through C.19.

The procedure used to calculate MRS/IS facility transportation costs is as follows. First, the waste throughput rates are converted to the number of truck and rail shipments of each waste form required to transport the throughput quantity. It is assumed that approximately 50 percent of the volume of each waste form is transported by truck and 50 percent by rail. The total number of shipments (truck plus rail) is minimized by filling the rail shipments to their maximum capacities first and then transporting the remainder by truck. This is done simply by dividing the annual throughput volume for each waste type by 2 (50 percent shipping mode split), dividing this volume by the single rail shipment capacity and rounding the number of rail shipments to the next largest whole number. The remaining volume is shipped by truck. Thus, somewhat more than 50 percent of the waste volumes are shipped by rail in these calculations. These data are shown in Tables C.20 to C.24 for each of the fuel cycle scenarios in this study.

The final step in the transportation cost calculations is to convert the annual number of offsite shipments in Tables C.20 to C.24 to annual transportation costs. This is done by multiplying the number of shipments by the unit cost per shipment developed for this study shown in Tables C.25 and C.26. It is assumed that the average turnaround time for a truck shipment is 24 hours and that for a rail shipment is 48 hours (required for demurrage fee calculations). The annual transportation costs for each waste form in mid-1982 dollars are shown in Tables C.27 to C.31 for each fuel cycle scenario. All transport distances are assumed to be 2500 miles, one-way, except for the spent fuel shipped to the MRS/IS facility. There, distances of 2000 miles and 2500 miles, one-way, were assumed.

TABLE C.10.

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Annual Waste Form Processing Requirements at MRS/IS Handling Facility - Reference Scenario (Packages)

	Spent	Fuel	ыгы		Dee	IMC		CH_TON
Year	BWR	PWR	<u>Canisters</u>	<u>Canisters</u>	<5R/hr	<u>>5R/hr</u>	Drums	Boxes
1990			233	183	205	28	1623	13
1991	0		467	368	410	55	3245	27
1992	0	0	700	549	614	84	4868	41
1993	0	0	700	549	614	84	4868	41
1994	0	0	700	549	614	84	4868	41
1995	0	0	700	549	614	84	4868	41
1996	0	0	700	549	614	84	4868	41
1997	0	0	700	549	614	84	4868	41
1998	0	0	0	0	0	0	0	0
1999	0	0	0	0	0	0	0	0
2000	0	0	0	0	0	0	0	0
2001	0	0	93	0	0	0	0	0
2002	0	0	0	0	0	0	0	0
2003	0	0	0	0	0	0	0	0
2004	0	0	0	0	0	0	0	0
2005	0	0	0	0	0	0	0	55
2006	0	0	0	0	0	0	0	0
2007	0	0	0	0	0	0	0	0
2008	0	0	0	0	0	0	0	0
2009	0	0	0	0	0	0	0	0
2010	0	0	0	0	0	0	0	.C
2011	0	0	467	37	41	6	325	3
2012	0	0	233	0	0	0	0	0
2013	0	0	420	220	246	34	1947	16
2014	0	0	700	220	246	34	1947	16
2015	0	0	0	0	0	0	0	0
2016	0	0	0	0	0	0	0	0
2017	0	0	0	0	0	0	0	0
2018	0	0	0	0	0	0	0	0
2019	0	0	0	0	0	0	0	0
2020	0	0	0	0	0	0	0	0

NOTE: Positive number denotes incoming shipment, negative number denotes outgoing shipment.

	Spent Asser	t Fuel nblies	HLW	RH-TRU	Dru	JMS	CH-TRU	CH-TRU
Year	BWR	PWR	<u>Canisters</u>	Canisters	<u><5R/hr</u>	>5R/hr	Drums	Boxes
1990	933	698	0	0	0	0	0	0
1991	1839	459	0	0	0	0	0	0
1992	1378	947	0	0	0	0	0	0
1993	1300	1036	0	0	0	0	0	0
1994	2155	1458	0	0	0	0	0	0
1995	1961	2138	0	0	0	0	0	0
1996	2878	2335	0	0	0	0	0	0
1997	3322	2143	0	0	0	0	0	0
1998			0	0	0	0	0	0
1999	0	0	0	0	0	0	0	0
2000	0	0	0	0	0	0	0	0
2001	0	0	43	0	0	0	0	0
2002	0	0	0	0	0	0	0	0
2003	0	0	0	0	0	0	0	0
2004	0	0	0	0	0	0	0	0
2005	0	0	0	0	0	0	0	0
2006	0	0	0	0	0	0	0	0
2007	0	0	0	0	0	0	0	0
2008	0	0	0	0	0	0	0	0
2009	0	0	0	0	0	0	0	0
2010	0	0	0	0	0	0	0	0
2011	0	0	0	0	0	0	0	0
2012	-1022	-1052	0	0	0	0	0	0
2013	-434	-995	0	0	0	0	0	0
2014	-1739	-1343	0	0	0	0	0	0
2015	-3822	-2626	0	0	0	0	0	0
2016	-5350	-4240	0	0	0	0	0	0
2017	-3400	-9 58	0	0	0	0	0	0
2018								
2019								
2020								

TABLE C.11. Annual Waste Form Processing Requirements of the MRS/IS Facility - Delayed Reprocessing Scenario (Packages)

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NOTE: Positive number denotes incoming shipment, negative number denotes outgoing shipment.

N a au	Spent Assemt	Fuel	HLW	RH-TRU	Dru	ims	CH-TRU	CH-TRU
Tear	BWK	PWR	Lanisters	Lanisters	<u><5K/hr</u>	<u>>58/nr</u>	Drums	Boxes
19 9 0			233	183	205	28	1623	13
1991	0		467	368	410	55	3245	27
1992	0	0	700	549	614	84	4868	41
1993	0	0	700	549	614	84	4868	41
1994	0	0	700	549	614	84	4868	41
1995	0	0	700	549	614	84	4868	41
1996	0	0	700	549	614	84	4868	41
1997	0	0	700	549	614	84	4868	41
1998	0	0	700	549	614	84	4868	41
1999	0	0	700	549	614	84	4868	41
2000	0	0	700	549	614	84	4868	41
2001	0	0	993	732	818	112	6490	54
2002	0	0	1167	915	1023	140	8113	68
2003	0	0	1400	1098	1228	168	8552	81
2004	0	0	1400	1098	1228	168	8552	81
2005	0	0	1400	1098	1228	168	8552	81
2006	0	0	1867	1464	1638	223	12,981	109
2007	0	0	2334	1830	2048	279	16,227	135
2008	0	0	1960	1438	1609	219	12,755	106
2009	0	0	1960	1438	1609	219	12,755	106
2010	0	0	1960	1438	1609	219	12,755	106
2011	0	0	2427	1805	2019	275	16,000	134
2012	0	0	1353	863	966	132	7659	65
2013	0	0	-140	724	811	111	6426	54
2014	0	0	1260	724	811	111	6426	54
2015	0	0		0	0	0	0	0
2016	0	0		0	0	0	0	0
2017	0	0	0	0	0	0	0	0
2018	0	0	0	0	0	0	0	0
2019	0	0	0	. 0	0	0	0	0
2020	0	0	0	0	0	0	0	0

TABLE C.12. Annual Waste Form Processing Requirements at MRS/IS Handling Facility - Delayed Disposal Scenario (Packages)

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NOTE: Positive number denotes incoming shipment, negative number denotes outgoing shipment.

Year	HLW <u>Canisters</u>	RH-TRU <u>Canisters</u>	Dri <5R/hr	ums >5R/hr	CH-TRU Drums	CH-TRU Boxes
1990	233	183	205	28	1623	13
1991	467	368	410	55	3245	27
1992	700	549	614	84	4868	41
1993	0	0	0	0	0	0
1994	0	0	0	0	0	0
1995	0	0	0	0	0	0
1996	0	0	0	0	0	0
1997	0	0	0	0	0	0
19 9 8	0	0	0	0	0	0
1999	0	0	0	0	0	0
2000	0	0	0	0	0	0
2001	0	0	0	0	0	0
2002	0	0	0	0	0	0
2003	0	0	0	0	0	0
2004	0	0	0	0	0	0
2005	0	0	0	0	0	0
2006	0	0	0	0	0	0
2007	0	0	0	0	0	0
2008	0	0	0	0	0	0
200 9	0	0	0	0	0	0
2010	0	0	0	0	0	0
2011	0	0	0	0	0	0
2012	0	0	0	0	0	0
2013	0	0	0	0	0	0
2014	0	0	0	0	0	0
2015	0	0	0	0	0	0
2016	0	0	0	0	0	0
2017	0	0	0	0	0	0
2018	0	0	0	0	0	0
2019	0	0	0	0	0	0
2020	0	0	0	0	0	0

TABLE C.13. Annual Waste Form Processing Requirements at MRS/IS Handling Facility - Early Disposal Scenario (Packages)

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NOTE: Positive number denotes incoming shipment, negative number denotes outgoing shipment.

Year	Spent <u>Assem</u> BWR	Fuel blies PWR	HLW Canisters	RH-TRU Canisters	Dru <5R/hr	ms >5R/hr	CH-TRU Drums	CH-TRU Boxes
1000						•	0	•
1990	934	698	0	0	0	0	U	U
1991	1839	460	0	0	0	0	0	0
1992	1378	948	0	0	0	0	0	0
1993	1300	1013	0	0	0	0	0	0
1994	2156	1457	0	0	0	0	0	0
1995	1961	2138	0	0	0	0	0	0
1996	2878	2336	0	0 `	0	0	0	0
1997	3322	2143	0	0	0	0	0	0
1998	2934	2855	0	0	0	0	0	0
1999	4217	2346	0	0	0	0	0	0
2000	4745	2936	0	0	0	0	0	0
2001	4567	3647	0	0	0	0	0	0
2002	5484	4184	0	0	0	0	0	0
2003	6373	3605	0	0	0	0	0	0
2004	6611	4414	0	0	0	0	0	0
2005	6611	4072	0	0	0	0	0	0
2006	6967	3996	0	0	0	0	0	0
2007	6834	4810	0	0	0	0	0	. 0
2008	1800	1333	0	0	0	0	0	0
2009	4189	1468	0	0	0	0	0	0
2010	1939	1587	0	0	0	0	0	0
2011	1834	1010	0	0	0	0	0	0
2012	0	0	0	0	0	0	0	0
2013	0	0	0	0	0	0	0	0
2014	0	0	0	0	0	0	0	0
2015	0	0	0	0	0	0	0	0
2016	0	0	0	0	0	0	Ο.	0
2017	0	0	0	0	0	0	0	0
2018	0	0	Ó	0	0	0	0	0
2019	0	0	0	0	0	0	0	0
2020	0	0	0	0	0	0	0	0

TABLE C.14.	Annual Waste Form Processing Requirements at MRS/IS Handling
	Facility-Delayed Disposal, No Reprocessing Scenario (Packages)

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NOTE: Positive number denotes incoming shipment, negative number denotes outgoing shipment.

	Spent Assem	Fuel blies	ны	RH_TRU	PH_TRU	CH_TRU	СН_ТРИ
Year	BWR	PWR	Canisters	<u>Canisters</u>	Drums	Drums	Boxes
1990	0	31	233	183	233	1623	13
1991	0	0	700	551	698	4868	40
1992	0	0	1400	1100	1396	9736	81
1993	0	0	2100	1649	2094	14604	122
1993	0	0	2800	2198	2792	19472	163
1995	0	0	3500	2747	3490	24340	204
1996	0	0	4200	3296	4188	20208	245
1997	0	0	2900	3845	4886	34076	286
1998	0	0	4760	3637	4621	28526	270
1999	0	0	4620	3429	4356	28300	254
2000	0	0	4480	3221	4091	28526	238
2001	0	0	4573	3196	4058	28300	236
2002	0	0	4060	2596	3295	22928	192
2003	0	0	3220	1673	2122	14750	124
2004	0	0	2380	750	949	6572	55
2005	0	0	1540	0	0	0	0
2006	0	0	1167	0	0	0	0
2007	0	0	700	0	0	0	0
2008	0	0	700	0	0	0	0
2009	0	0	700	0	0	0	0
2010	0	0	700	0	0	0	0
2011	0	0	1167	37	47	325	3
2012	0	0	1400	0	0	0	0
2013	0	. 0	1260	220	246	1947	16
2014	0	0	1960	440	492	3894	32
2015	0	0	. O	0	0	0	0
2016	0	0	0	0	0	0	0
2017	0	0	0	0	0	0	0
2018	0	· 0	0	0	0	0	0
2019	0	. 0	0	0	0	0	0
2020	0	0	0	0	0	0	0

TABLE C.15. Cumulative Waste Form Storage Requirements at MRS/IS Facility - Reference Scenario (Packages)

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TABLE C.16.

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Cumulative Waste Form Storage Requirements at MRS/IS Facility – Delayed Reprocessing Scenario (Packages)

N	Spent Asser	t Fuel mblies	HLW	RH-TRU	Dru		CH-TRU	CH-TRU
fear	BWK	PWK	Lanisters	Lanisters	<u><5K/hr</u>	<u>>5K/hr</u>	Drums	Boxes
1990	933	698	0	0	0	0	0	0
1991	2772	1157	0	0	0	0	0	0
1992	4150	2104	0	0	0	0	0	0
1993	5450	3140	0	0	0	0	0	0
1994	7605	4598	0	0	0	0	0	0
1995	9566	6736	0	0	0	0	0	0
1996	12444	9071	0	0	0	0	0	0
1997	15766	11214	0	0	0	0	0	0
1998	15766	11214	0	0	0	0	0	0
1999	15766	11214	0	0	0	0	0	0
2000	15766	11214	0	0	0	0	0	0
2001	15766	11214		0	0	0	0	0
2002	15766	11214	0	0	0	0	0	0
2003	15766	11214	0	0	0	0	0	0
2004	15766	11214	0	0	· 0	0	0	0
2005	15766	11214	0	0	0	0	0	0
2006	15766	11214	0	0	0	0	0	0
2007	15766	11214	0	0	0	0	0	0
2008	15766	11214	0	0	0	0	0	0
2009	15766	11214	0	0	0	0	0	0
2010	15766	11214	0	0	0	0	0	0
2011	15766	11214	0	0	0	0	0	0
2012	14744	10162	0	0	0	0	0	0
2013	14310	9167	0	0	0	0	0	0
2014	12571	7825	0	0	0	0	0	0
2015	7849	5199	0	0	0	0	0	0
2016	3399	959	0	0	0	0	0	0
2017	0	0	0	0	0	0	0	0

	Spent Assem	Fuel blies	HLW	RH-TRU	RH-TRU	CH-TRU	
Year	BWR	PWR	Canisters	Canisters	Drums	Drums	Boxes
1990	0	31	233	183	233	1623	13
1991	0	0	700	549	698	4868	41
1992	0	0	1400	1098	1396	9736	82
1993	0	0	2100	1647	2094	14604	123
1994	0	0	2800	2196	2792	19472	164
1995	0	0	3500	2745	3490	24340	205
1996	0	0	4200	3294	4188	29208	246
1997	0	0	4900	3843	4886	34076	287
1998	0	0	5600	4392	5584	38944	328
1999	0	0	6300	4941	6282	43812	369
2000	0	0	7000	5490	6980	48680	410
2001	0	0	7933	6222	7910	55170	464
2002	0	0	9100	7137	9073	63283	532
2003	0	0	10500	8235	10469	71835	613
2004	0	0	11900	9333	11865	80387	694
2005	0	0	13300	10431	13261	88939	775
2006	0	0	15167	11895	15122	101920	884
2007	0	0	17500	13725	17449	118147	1010
2008	0	0	19460	15163	19277	130902	1125
2009	0	0	21420	16601	21105	143657	1231
2010	0	0	23380	18039	22933	156412	1337
2011	0	0	25807	19844	25227	172412	1471
2012	0	0	2716 0	20707	26325	180071	1536
2013	0	0	27020	21431	27247	186497	1590
2014	0	0	28280	22155	28169	192923	1644
2015	0	0	. 28280	J.	J:	L	.1.
2016	0	0	28280	Y	Y	Y	Y
2017	0	0					
2018	0	0	On-Site	On-Site	On-Site	On-Site	On-Site
2019	0	0	to	Iransfer to	Iransfer to	Iransfer to	Iransfer to
2020	0	0	Disposal	Disposal	Disposal	Disposal	Disposal

TABLE C.17. Cumulative Waste Form Storage Requirements at MRS/IS Facility - Delayed Disposal Scenario (Packages)

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Year	Spent Fuel Assemblies BWR PWR	HLW <u>Canisters</u>	RH-TRU Canisters	RH-TRU Drums	CH-TRU Drums	CH-TRU Boxes
1990	0	233	183	233	1623	13
1991	0	700	551	698	4868	30
1992	0	1400	1100	1396	9736	81
1993	0	0	0	0	0	0
1994	0	0	0	0	0	0
1995	0	0	0	0	0	0
1996	0	0	0	0	0	0
1997	0	0	0	0	0	0
1998	0	0	0	0	0	0
1999	0	0	0	0	0	0
2000	0	0	0	0	0	0
2001	0	0	0	0	0	0
2002	0	0	0	0	0	0
2003	0	0	0	0	0	0
2004	0	0	0	0	0	0
2005	0	0	0	0	0	0
2006	0	0	0	0	0	0
2007	0	0	0	0	0	0
2008	0	0	0	0	0	0
2009	0	0	0	0	0	0
2010	0	0	0	0	0	0
2011	0	0	0	0	0	0
2012	0	0	0	0	0	0
2013	0	0	0	0	0	0
2014	0	0	0	0	0	0
2015	0	0	0	0	0	0
2016	0	0	0	0	0	0
2017	0	0	0	0	0	0
2018	0	0	0	0	0	0
2019	0	0	0	0	0	0
2020	0	0	0	0	0	0

TABLE C.18. Cumulative Waste Form Storage Requirements at MRS/IS Facility - Early Disposal Scenario (Packages)

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TABLE C.19.	Cumulative Waste Form Storage Requirements at MRS/IS
<u> </u>	Facility – Delayed Disposal, No Reprocessing
	Scenario (Packages)

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	Spent	Fuel					
Year	<u>Assem</u> BWR	PWR	Canisters	Canisters	RH-TRU Drums	CH-IRU Drums	Boxes
1990	0	31	233	183	233	1623	13
1991	0	0	700	551	698	4868	40
1992	0	0	1400	1100	1306	9000	40 01
1992	0	0	0	0	0	97.30	0
1994	0	0	0	0	0	0	0
1995	0	0 0	0	0	0	0	0
1996	0	0 0	0	0	0	0	0
1997	0	0	0	0	0	0	0
1998	0	0	0	0	0	0	0
1999	0	0	0	0	0	0	0
2000	0	0	0	0	0	0	0
2001	0	0	0	0	0	0	0
2002	0	0	0	0	0	· 0	0 0
2003	0	0	0	0	0	0	0
2004	0	0	0	0	0	0	0
2005	0	0	0	0	0	0	0
2006	0	0	0	0	0	0	0
2007	0	0	0	0	0	0	0
2008	0	0	0	0	0	0	0
2009	0	0	0	0	0	0	0
2010	0	0	0	0	0	0	0
2011	0	0	0	. 0	0	0	0
2012	0	0	0	0	0	0	0
2013	0	0	0	0	0	0	0
2014	0	0	0	0	0	0	0
2015	0	0	0	0	0	0	0
2016	0	0	0	0	0	0	0
2017	0	0	0	0	0	0	0
2018	0	0	0	0	0	0	0
2019	0	0	0	0	0	0	0
2020	0	0	0	0	0	0	0

TABLE C.20.

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O. Number of Offsite Shipments Handled Annually at MRS/IS Facility – Reference Scenario

	Spent Fuel		High-Level RH-TRU Wastes Canisters		RH-TRU <5R/hr		Drui >5R,	Drums >5R/hr		CH-TRU Drums		CH-TRU Boxes		
	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail
1990			117	24	92	19	6	3	1	1	23	12	3	1
1991			234	47	184	37	15	5	2	2	45	23	5	2
1992	0	0	350	70	275	55	20	8	6	2	68	34	7	4
1993	0	0	350	70	275	55	20	8	6	2	68	34	7	4
1994	0	0	350	70	275	55	20	8	6	2	68	34	7	4
1995	0	0	350	70	275	55	20	8	6	2	68	34	7	4
1996	0	0	350	70	275	55.	20	8	6	2	68	34	7	4
1997	0	0	350	70	275	55	20	8	6	2	68	34	7	4
1998	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1999	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2000	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2001	0	0	47	10	0	0	0	0	0	0	0	0	0	0
2002	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2003	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2004	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2005	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2006	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2007	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2008	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2009	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2010	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2011	0	0	234	47	19	4	0	1	1	0	6	3	1	0
2012	0	0	117	24	0	0	0	0	0	0	0	0	0	0
2013	0	0	210	42	110	22	9	3	2	1	27	14	3	2
2014	0	0	350	70	110	22	9	3	2	1	27	14	3	2
2015	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2016	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2017	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2018	0	0	0	0	0	0	0	0	0	0	0	0	0	0 '
2019	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2020	0	0	0	0	0	0	0 ′	0	0	0	0	0	0	0

Note: Positive number denotes incoming shipment, negative number denotes outgoing shipment.

		Spent Fuel		_evel tes	RH-TH Canis	RH-TRU Canisters		fRU 'hr	Drums >5R/hr		CH-TRU Drums		CH-TRU Boxes	
	Truc	k Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail
1990	583	76	0	0	0	0	0	0	0	0	0	0	0	0
1991	690	84	0	0	0	0	0	0	0	0	0	0	0	0
1992	819	107	0	0	0	0	0	0	0	0	0	0	0	0
1993	832	110	0	0	0	0	0	0	0	0	0	0	0	0
1994	1268	165	0	0	0	0	0	0	0	0	0	0	0	0
1995	1560	208	0	0	0	0	0	0	0	0	0	0	0	0
1996	1888	247	0	0	0	0	0	0	0	0	0	0	0	0
1997	1903	246	0	0	0	0	0	0	0	0	0	0	0	0
1998			0	0	0	0	0	0	0	0	0	0	0	0
1999	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2000	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2001	0	0			0	0	0	0	0	0	0	0	0	0
2002	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2003	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2004	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2005	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2006	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2007	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2008	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2009	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2010	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2011	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2012	-770	-105	0	0	0	0	0	0	0	0	0	0	0	0
2013	-598	-84	0	0	0	0	0	0	0	0	0	0	0	0
2014	-1100	-145	0	0	0	0	0	0	0	0	0	0	0	0
2015	-2258	-295	0	0	· 0	0	0	0	0	0	0	0	0	0
2016	-3453	-452	0	0	0	0	0	0	0	0	0	0	0	0
2017	-1320	-164	0	0	0	0	0	0	0	0	0	0	0	0
2018	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2019	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2020	0	0	0	0	0	0	0	0	0	0	0	0	0	0

TABLE C.21. Number of Offsite Shipments Handled Annually at MRS/IS Facility - Delayed Reprocessing Scenario

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Note: Positive number denotes incoming shipment, negative number denotes outgoing shipment.

TABLE C.22.

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Number of Offsite Shipments Handled Annually at MRS/IS Facility - Delayed Disposal Scenario

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	Sp Fu	Spent Fuel		High-Level Wastes		RH-TRU Canisters		'RU 'hr	Drum >5R/	is hr	CH-TRU Drums		CH-T Box	CH-TRU Boxes	
	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	
1990			117	24	92	19	6	3	1	1	23	12	3	1	
1991			234	47	184	37	15	4	2	2	45	23	5	2	
1992	0	0	350	70	275	55	20	8	6	2	68	34	7	4	
1993	0	0	350	70	275	55	20	8	6	2	68	34	7	4	
1994	0	0	350	70	275	55	20	8	6	2	68	34	7	4	
1995	0	0	350	70	275	55	20	8	6	2	68	34	7	4	
1996	0	0	350	70	275	55	20	8	6	2	68	34	7	4	
1997	0	0	350	70	275	55	20	8	6	2	68	34	7	4	
1998	0	0	350	70	275	55	20	8	6	2	68	34	7	4	
1999	0	0	350	70	275	55	20	8	6	2	68	34	7	4	
2000	0	0	350	70	275	55	20	8	6	2	68	34	7	4	
2001	0	0	463	94	362	74	29	10	7	3	91	45	8	5	
2002	0	0	582	117	460	91	35	13	8	4	112	57	11	6	
2003	0	0	700	150	658	110	43	15	12	4	118	60	13	7	
2004	0	0	700	140	548	110	43	15	12	4	118	60	13	7	
2005	0	0	700	140	548	110	43	15	12	4	118	60	13	7	
2006	0	0	932	187	729	147	57	20	14	6	179	91	17	10	
2007	0	0	1164	234	915	183	72	25	19	7	225	113	21	12	
2008	0	0	980	196	718	144	55	20	14	7	117	89	18	9	
2009	0	0	980	196	718	144	55	20	14	7	117	89	18	9	
2010	0	0	980	196	718	144	55	20	14	7	117	89	18	9	
2011	0	0	1212	243	900	181	70	25	19	7	223	111	21	12	
2012	0	0	674	136	433	86	33	12	10	3	105	54	10	6	
2013	0	0	376	76	364	72	28	10	7	3	89	45	8	5	
2014	0	0	630	126	364	72	28	10	7	3	89	45	8	5	
2015	0	0	83	17	0	0	0	0	0	0	0	0	0	0	
2016	0	0	122	26	0	0	0	0	0	0	0	0	0	0	
2017	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
2018	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
2019	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
2020	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

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Note: Positive number denotes incoming shipment, negative number denotes outgoing shipment.

	Sp Fu	Spent Fuel		.evel tes	RH-TH Canisi	RU ters	RH-T <5R/	RU hr	Drur >5R,	ns /hr	CH-TR Drum	U s	CH-TR Boxe	U s
	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail
1990			117	24	92	19	6	3	1	1	23	12	3	1
1991			234	47	184	37	15	5	2	2	45	23	5	2
1992	0	0	350	70	275	55	20	8	6	2	68	34	7	4
1993	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1 994	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1995	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1996	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1997	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1998	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1999	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2000	O	0	0	0	0	0	0	0	0	0	0	0	0	0
2001	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2002	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2003	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2004	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2005	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2006	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2007	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2008	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2009	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2010	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2011	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2012	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2013	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2014	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2015	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2016	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2017	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2018	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2019	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2020	0	0	0	0	0	0	0	0	0	0	0	0	0	0

TABLE C.23. Number of Offsite Shipments Handled Annually at MRS/IS Facility - Early Disposal Scenario

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Note: Positive number denotes incoming shipment, negative number denotes outgoing shipment.

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	Spent Fuel		High-Level Wastes		RH-TRU Canisters		RH→TRU <5R/hr		Drums >5R/hr		CH-TRU Drums		CH-TRU Boxes	
	Truc	k Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail	Truck	Rail
1990	583	76	0	0	0	0	0	0	0	0	0	0	0	0
1 991	690	84	0	0	0	0	0	0	0	0	0	0	0	0
1 992	819	107	0	0	0	0	0	0	0	0	0	0	0	0
1993	832	110	0	0	0	0	0	0	0	0	0	0	0	0
1994	1268	165	0	0	0	0	0	0	0	0	0	0	0	0
1995	1560	208	0	0	0	0	0	0	0	0	0	0	0	0
1996	1888	247	0	0	0	0	0	0	0	0	0	0	0	0
1997	1903	246	0	0	0	0	0	0	0	0	0	0	0	0
1 998	2156	286	0	0	0	0	0	Ο,	0	0	0	0	0	0
1 999	2465	322	0	0	0	0	0	0	0	0	0	0	0	0
2000	2658	341	0	0	0	0	0	0	0	0	0	0	0	0
2001	2961	388	0	0	0	0	0	0	0	0	0	0	0	0
2002	3456	452	0	0	0	0	0	0	0	0	0	0	0	0
2003	3384	436	0	0	0	0	0	0	0	0	0	0	0	0
2004	3852	500	0	0	0	0	0	0	0	0	0	0	0	0
2005	3685	475	0	0	0	0	0	0	0	0	0	0	0	0
2006	3731	480	0	0	0	0	0	0	0	0	0	0	0	0
2007	4109	534	0	0	0	0	0	0	0	0	0	0	0	0
2008	1111	1 46	0	0	0	0	0	0	0	0	0	0	0	0
2009	1775	222	0	0	0	0	0	0	0	0	0	0	0	0
2010	1275	168	0	0	0	0	0	0	0	0	0	0	0	0
2011	957	124	0	0	0	0	0	0	0	0	0	0	0	0
2012	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2013	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2014	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2015	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2016	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2017	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2018	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2019	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2020	0	0	0	0	0	0	0	0	0	0	0	0	0	0

TABLE C.24. Number of Offsite Shipments Handled Annually at MRS/IS Facility - Delayed Disposal, No Reprocessing Scenario

Note: Positive number denotes incoming shipment, negative number denotes outgoing shipment.

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Cargo/ Shipping Distance	Cask Rental Fee	<u>Shippin</u> Loaded	g Charge Empty	Security <u>Costs</u>	Demurrage at Origin	Demurrage at MRS/IS	Total <u>(\$/Shipment)</u>
Spent Fuel 500 mi 2000 mi 2500 mi	46,000 138,000 172,500	9,910 22,220 25,910	8,590 19,140 22,630	3,640 14,560 18,200	11,500 11,500 11,500	11,500 11,500 11,500	91,140 216,920 262,240
High-Level Wastes 500 mi 2500 mi	46,000 172,500	9,980 26,090	8,590 22,630	3,640 18,200	11,500 11,500	11,500 11,500	91,210 262,410
RHTRU Waste Cans 500 mi 2500 mi	35,000 131,250	10,110 26,430	7,060 18,590	0 0	8,750 8,750	8,750 8,750	69,670 193,770
RHTRU Drums <5 R/hr 500 mi 2500 mi	4,200 15,750	8,540 23,320	6,250 16,360	0 0	1,050 1,050	1,050 1,050	21,090 57,530
RHTRU Drums >5 R/hr 500 mi 2500 mi	4,200 15,750	7,930 20,720	6,540 17,110	0 0	1,050 1,050	1,050 1,050	20,770 55,680
CHTRU Wastes 500 mi 2500 mi	11,200 42,000	6,090 15,920	2,710 7,080	0 0	2,800 2,800	2,800 2,800	25,600 70,600

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Cargo/ Shipping Distance	Cask Rental Fee	<u>Shipping</u> Loaded	g Charge Empty	Security Costs	Demurrage at Origin	Demurrage at MRS/IS	Total <u>(\$/Shipment)</u>
Spent Fuel 500 mi 2000 mi	4,000	1,630	980 3 910	860 3 440	2,000	2,700	12,170
2500 mi	14,000	6,810	4,900	4,300	2,000	2,700	34,710
High-Level Wastes							
500 mi 2500 mi	4,000 14,000	1,660 6,310	980 4,900	860 4,300	2,000 2,000	2,700 2,700	12,200 34,210
RHTRU Waste Cans							
500 mi 2500 mi	3,500 12,250	1,070 4,050	510 2,530	0 0	1,750 1,750	2,450 2,450	9,280 23,030
RHTRU Drums <5 R/hr							
500 mi 2500 mi	350 1,225	1,380 5,220	670 3,330	0 0	175 175	875 875	3,450 10,825
RHTRU Drums >5 R/hr							
500 mi 2500 mi	350 1,225	1,280 4,890	700 3,480	0 0	175 175	875 875	3,380 10,645
CHTRU Wastes							
500 mi 2500 mi	1,400 4,900	1,380 5,220	430 2,160	0 0	700 700	1,400 1,400	5,310 14,380

TABLE C.26. Truck Shipment Unit Cost Elements

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YEAR	Spent Fuel	High- Level Wastes	RH-TRU Special Canisters	RH-TRU Drums	CH-TRU Drums and Boxes	TOTAL
1990	·	10,300	5,800	293	1,282	17,675
1991		20,338	11,407	565	2,484	34,794
1992	0	30,342	16,991	824	3,761	51,918
1993	0	30,342	16,991	824	3,761	51,918
1994	0	30,342	16,991	824	3,761	51,918
1995	0	30,342	16,991	824	3,761	51,918
1996	0	30,342	16,991	824	3,761	51,918
1997	0	30,342	16,991	824	3,761	51,918
1998	0	0	0	0	0	0
1999	0	0	0	0	0	0
2000	0	0	0	0	<i>,</i> 0	0
2001	0		0	0	0	
2002	0	0	0	0	0	0
2003	0	0	0	0	0	0
2004	0	0	0	0	0	0
2005	0	0	0	0	0	0
2006	0	0	0	0	0	0
2007	0	0	0	0	0	0
2008	0	0	0	0	0	0
2009	0	0	0	0	0	0
2010	0	0	0	0	0	0
2011	0	20,338	1,213	65	313	21,929
2012	0	10,300	0	0	0	10,300
2013	0	18,205	6,796	336	1,561	26,898
2014	0	30,342	6,796	336	1,561	39,035
2015	0	0	0	0	0	0
2016	0	0	0	0	0	0
2017	0	0	0	0	0	0
2018	0	0	0	0	0	0
2019	0	0	0	0	0	0
2020	<u>_0</u>	0 291,875	0 133,958	$\frac{0}{6,539}$	$\frac{0}{29,767}$	0 462,139

TABLE C.27. Annual Transportation Costs for Each Waste Form and the Total Transportation Costs for the MRS/IS Facility - Reference Scenario (\$1000's)

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	Spent	Fuel	High- Level	RH-TRU Special	RH-TRII	CH-TRU Drums
Year	2500 mi.	<u>2000 mi.</u>	Wastes	Canisters	Drums	and Boxes
1990	40,097	32,816	0	0	0	0
1991	45,893	. 37,548	0	0	0	0
1992	56,140	46.151	0	0	0	0
1993	58,091	47.166	0	0	0	0
1994	87,039	71,308	0	0	0	0
1995	108,416	88,816	0	0	0	0
1996	130,202	106,462	0	0	0	0
1997	130,340	106,665	0	0	0	0
1998	0	0	0	0	0	0
1999	0	0	0	0	0	0
2000	0	0	0	0	0	0
2001	0	0	0	0	0	0
2002	0	0	0	0	0	0
2003	0	0	0	0	0	0
2004	0	0	0	0	0	0
2005	0	0	0	0	0	0
2006	0	0	0	0	0	0
2007	0	0	0	0	0	0
2008	0	0	0	0	0	0
2009	0	0	0	0	0	0
2010	0	0	0	0	0	0
2011	0	0	0	0	0	0
2012	54,267	0	0	0	0	0
2013	42,779	0	0	0	0	0
2014	76,229	0	0	0	0	0
2015	155,783	0	0	0	0	0
2016	238,458	0	0	0	0	0
2017	88,851	0	0	0	0	0
2018	0	0	0	0	0	0
2019	0	0	0	0	0	0
2020	0	00	<u>0</u>	<u>0</u>	<u>0</u>	<u>0</u>
	1312,600	1193,139	0	0	0	0

TABLE C.28. Annual Transportation Costs for Each Waste Form - Delayed Reprocessing Scenario (\$1000's)

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YEAR	Spent Fuel	High- Level Wastes	RH-TRU Special Canisters	RH-TRU Drums	CH-TRU Drums and Boxes	TOTAL
1990		10,300	5,800	293	1,292	17,675
1991		20,338	11,407	565	2,484	34,794
1992	٥	30,342	16,991	824		51 019
1993	0	30,342	16,991	824	3,761	51,918
1994	0	30,342	16,991	824	3,761	51,918
1995	0	30,342	16,991	824	3,761	51,918
1996	0	30,342	16,991	824	3,761	51,918
1997	0	30,342	16,991	824	3,761	51,918
1998	0	30,342	16,991	824	3,761	51,918
1999	0	30,342	16,991	824	3,761	51,918
2000	0	30,342	16,991	824	3,761	51,918
2001	0	40,506	22,676	1,096	4,954	69,232
2002	0	50,612	28,227	1,389	6,217	86,445
2003	0	60,684	33,935	1,626	6,614	102,8 59
2004	0	60,684	33,935	1,626	6,614	102,85 9
2005	0	60,684	33,935	1,626	6,614	102,859
2006	0	80,954	45,273	2,180	9,949	138,356
2007	0	101,224	56,532	2,722	12,363	172,841
2008	0	84,958	44,438	2,047	9,723	141,166
2009	0	84,958	44,438	2,047	9,723	141,166
2010	0	84,958	44,438	2,047	9,723	141,166
2011	0	105,228	55,799	2,700	12,193	175,920
2012	0	58,746	26,636	1,279	5,890	92,551
2013	0	32,806	7,084	1,085	4,925	45,900
2014	0	54,616	7,084	1,085	4,925	67,710
2015	0	7,300	0	0	0	7,300
2016	0	10,996	0	0	0	10,996
2017	0	0	0	0	0	0
2018	0	0	0	0	0	0
2019	0	0	0	0	0	0
2020	· <u> </u>	0	0	0	0	0
	0	1283,630	654,556	32,829	148,043	2119,058

TABLE C.29. Annual Transportation Costs for Each Waste Form - Delayed Disposal Scenario (\$1000's)

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2.30. Annual Transportation Costs for Each Waste Form – Early Disposal Scenario (\$1000's)

YEAR	Spent Fuel	High- Level Wastes	RH-TRU Special Canisters	RH-TRU Drums	CH-TRU Drums and Boxes	TOTAL
1990		10,300	5,800	293	1,292	17,685
1991		20,338	11,407	565	2,484	34,794
1992	0	30,342	16,991	824	3,761	51,918
1993	0	0	0	0	0	0
1994	0	0	0	0	0	0
1995	0	0	0	0	0	0
1996	0	0	0	0	0	0
1997	0	0	0	0	0	0
1998	0	0	0	0	0	0
1999	0	0	0	0	0	0
2000	0	0	0	0	0	0
2001	0	0	0	0	0	0
2002	0	0	0	0	0	0
2003	0	0	0	0	0	0
2004	0	0	0	0	0	0
2005	0	0	0	0	0	0
2006	0	0	0	0	0	0
2007	0	0	0	0	0	0
2008	0	0	0	0	0	0
2009	0	0	0	0	0	0
2010	0	0	0	0	0	0
2011	0	0	0	0	0	0
2012	0	0	0	0	0	0
2013	0	0	0	0	0	0
2014	0	0	0	0	0	0
2015	0	0	0	0	0	0
2016	0	0	0	0	0	0
2017	0	0	0	0	0	0
2018	0	0	0	· 0	0	0
2019	0	0	0	0	0	0
2020	0	0	0	0	0	0
	0	60,980	34,198	1,682	7,537	104,397

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YEAR	Spont Fuel	High- Level Wastes	RH-TRU Special Canisters	RH-TRU Drums	CH-TRU Drums and Boxes
1990	40,166	0	0	0	0
1991	46,186	0	0	0	0
1992	56,487	0	0	0	0
1993	57,725	0	0	0	0
1994	87,282	0	0	0	0
1995	108,694	0	0	0	0
1996	130,306	0	0	0	0
1997	130,564	0	0	0	0
1998	149,835	0	0	0	0
1999	170,002	0	0	0	0
2000	181,683	0	0	. 0	0
2001	204,525	0	0	0	0
2002	238,490	0	0	0	0
2003	231,795	0	0	0	0
2004	264,823	0	0	0	0
2005	252,470	0	0	0	0
2006	255,378	0	0	0	0
2007	282,660	0	0	0	0
2008	76,850	0	0	0	0
2009	119,828	0	0	0	0
2010	88,312	0	0	0	0
2011	66,522	0	0	0	0
2012	0	0	0	0	0
2013	0	0	0	0	0
2014	0	0	0	0	0
2015	0	0	. 0	0	0
2016	0	0	0	0	0
2017	0	0	0	0	0
2018	0	0	0	0	0
2019	0	0	· 0	0	0
2020	0	0	0		0
	3,240,583	0	0	0	0

TABLE C.31. Annual Transportation Costs for Each Waste Form - Delayed Disposal, No Reprocessing (\$1000's)

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APPENDIX D

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GENERAL CRITERIA AND STANDARDS

APPENDIX D

GENERAL CRITERIA AND STANDARDS

Design and construction of the facilities described in Section 4 of this report will be in accordance with the applicable sections of the following regulations, codes, standards, and guides, as well as their applicable references. Other codes and standards may be selected and used during the subsequent design phases.

D.1 U.S. GOVERNMENT STANDARDS, REGULATIONS, AND GUIDES

National Environmental Policy Act (NEPA)

40 CFR 1500-1508

Occupational Safety and Health Administration (OSHA)

Code of Federal Regulations (CFR)

10 CFR 20, Standards for Protection Against Radiation

10 CFR 30, Rules of General Applicability to Domestic Licensing of By-Product Material

10 CFR 50, Domestic Licensing of Production and Utilization Facilities

10 CFR 51, Licensing and Regulatory Policy and Procedures for Environmental Protection

10 CFR 55, Operators' Licenses

10 CFR 60, Disposal of High-Level Radioactive Wastes in Geologic Repositories (Proposed)

10 CFR 70, Domestic Licensing of Special Nuclear Material

10 CFR 71, Packaging of Radioactive Material for Transport and Transportation of Radioative Material under Certain Conditions

10 CFR 72, Licensing Requirements for the Storage of Spent Fuel in an Independent Spent Fuel Storage Installation (ISFSI)

10 CFR 73, Physical Protection of Plants and Materials

10 CFR 75, Safeguard of Nuclear Material (when issued)

D.1

10 CFR 95, Security Facility Approval and Safeguarding of National Security Information and Restricted Data

10 CFR 100, Reactor Site Criteria

10 CFR 150, Exemptions and Continued Regulatory Authority in Agreement States under Section 274

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10 CFR 170, Fees for Facilities and Materials Licenses and Other Regulatory Services under the Atomic Energy Act of 1954, as Amended

10 CFR 1022, Compliance with Floodplain/Wetland Environmental Review Requirements

29 CFR 1910, Occupational Safety and Health Standards

40 CFR, Protection of the Environment

49 CFR 127, 191.179, Hazardous Materials Regulations

49 CFR 173.393, General Packaging and Shipment Requirements

U.S. Nuclear Regulatory Commission (NRC) Regulatory Guides

1.12, Fire Protection Guidelines for Nuclear Power Plants

1.21, Measuring, Evaluating, and Reporting Radioactivity in Solid Wastes and Releases of Radioactive Materials in Liquid and Gaseous Effluents from Light-Water-Cooled Nuclear Power Plants

1.23, Radiation Protection Design Features

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Manual Chapters (MC)

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SDC 5.1, Standard Design Criteria for Heating, Ventilating, and Air Conditioning

SDC 7.2, Standard Electrical Design Criteria for Outside Lighting and Aerial Distribution Systems

SDC 7.4, Standard Electrical Design Criteria for Underground Power Distribution Systems

SDC 7.5, Standard Electrical Design Criteria for Interior Power and Lighting Systems

SDC 7.7, Standard Electrical Design Criteria for Communication, Signaling, and Low-Voltage Systems

SDC 7.8, Standard Electrical Design Criteria for Fire Alarm Systems

SCC 7.10, Standard Electrical Design Criteria for Corrosion Protection Systems

E-11, Cathodic Protection Standards

E-12, Building Grounding

D.2 STATE OF WASHINGTON PUBLICATIONS

Washington Administrative Code

Chapter 296-52, Safety Standards for the Possession and Handling of Explosives

Chapter 296-155, Construction Standards

State of Washington High Manual

State of Washington Grid System

D.3 INDUSTRIAL AND PROFESSIONAL SOCIETY PUBLICATIONS

In general, applicable "national concensus" codes and standards as developed by such organizations as the American Society of Mechanical Engineer, American Concrete Institute, American National Standards Institute and the Institute of Electrical and Electronic Engineers shall also be followed.

American Conference of Governmental Industry Hygienists (ACGIH)

Threshold Limit Values for Chemical Substances and Physical Agents in the Workroom Environment

Industrial Ventilation, 14th Edition

American Concrete Institute (ACI)

American National Standards Institute (ANSI)

A58.1-72, Building Code Requirements for Minimum Design Loads in Buildings and Other Structures

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B30.3-75, Hammerhead Tower Cranes, Partial Revision of B30.2-43 (R 1952)

B30.4-73, Portal, Towe, and Pillar Cranes, Safety Code for

B30-9-71, Slings, Safety Code for (partial revision of B30.2-43)

B30.10-75, Hooks, Safety Standards for Cableways, Cranes, Hoists Hooks, Jacks, and Slings.

B30.11-73, Monorail Systems and Under-Hung Cranes

B30.13, Controlled Mechanical Storage Crane

B30.16-73, Overhead Hoists

B56.1, Lowered Industrial Trucks, Low Lift and High Lift Trucks, Safety Standards for (ISO/R1074); Design, Operation, Maintenance of Lowered Industrial Trucks (ISO/R1074)

C2-77, National Electrical Code

N13.1-69, Guide to Sampling Airborne Radioactive Materials in Nuclear Facilities

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N13.10-74, Onsite Instrumentation for Continuously Monitoring Radioactivity in Effluents, Specification, and Performance of

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S1.6-67, Preferred Frequencies and Band Numbers for Acoustical Measurement

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American Society of Civil Engineers (ASCE)

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1977 Fundamentals Handbook

American Society of Mechanical Engineers (ASME)

Boiler and Pressure Vessel Code, Section VII, Division 1, Pressure Vessels

American Society for Testing and Materials (ASTM)

American Water Works Association (AWWA)

Manual M-14, Backflow Prevention and Cross Connection Control

Standard C-506-69, Backflow Prevention Devices, Reduced Pressure Principle and Double Check Valve Types

Factory Mutual Research Corporation Manual (FMRC)

7-88 Storage Tanks for Flammable Liquids

Government-Industry Data Exchange Program (GIDEP)

Institute of Electrical and Electronics Engineers (IEEE)

279-71, Criteria for Protection, Systems for Nuclear Power Generating Stations

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308-74, Standard Criteria for Class IE Power Systems for Nuclear Power Generating Stations

380-75, Definition of Terms used in IEEE Nuclear Power Generating Station Standard

383-74, IEEE Standard for Type Test of Class IE Electric Cables, Field Splices, and Connections for Nuclear Power Generating Stations

384-77, Criteria for Separation of Class IE Equipment and Circuits

422-77, Design and Installation of Cable Systems in Power Generating Stations

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72B, Installation, Maintenance, and Use of Auxiliary Protective Signaling Systems for Fire Alarm Service, Standard NFPA No. 72-B-1975

72E, Automatic Fire Detectors, Standard for NFPA No. 72E-1974

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78, Lightning Protection Code

Underwriters' Laboratories, Inc. (UL)

586, Test Performance of High-Efficiency Particulate Air Filter Unit

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