

CRWMS/M&O

Design Analysis Cover Sheet

Complete only applicable items.

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1. Purpose

The purpose of this design analysis is to determine the accuracy of the SAS2H module of SCALE 4.3 in predicting isotopic concentrations of spent fuel assemblies. The objective is to develop a methodology for modeling assemblies similar to those evaluated within this analysis and to establish the consistency of SAS2H predictions. The results of this analysis may then be applied to future depletion calculations using SAS2H in which no measurements are available.

2. Quality Assurance

The Quality Assurance (QA) program applies to this analysis. The work reported in this document is part of the Waste Package Design analysis that will eventually support the License Application Design phase. This activity, when appropriately confirmed, can impact the proper functioning of the Mined Geologic Disposal System (MGDS) waste package; the waste package has been identified as an MGDS Q-List item important to safety and waste isolation (pp. 4, 15, Reference 5.1). The waste package is on the Q-List by direct inclusion by the Department of Energy (DOE), without conducting a QAP-2-3 evaluation. The Waste Package Development Department (WPDD) responsible manager has evaluated this activity in accordance with QAP-2-0, *Conduct of Activities*. The *Perform Criticality, Thermal, Structural, and Shielding Analyses* (Reference 5.2) evaluation has determined the preparation and review of this design analysis is subject to *Quality Assurance Requirements and Description* (Reference 5.3) requirements. As specified in NLP-3-18, this activity is subject to QA controls.

The analysis described in this document supports development of the disposal criticality analysis methodology. No designs were analyzed in this document. This document will not directly support any construction, fabrication, or procurement activity and therefore is not required to be procedurally controlled as TBV (to be verified). The calculation design inputs or information used in this document comes from data accepted by the Nuclear Regulatory Commission and by the scientific and engineering community as established fact. The specific references are listed in Section 5 and identified in Section 7. The information is therefore not treated as unqualified data.

3. Method

The analytical model employed for this analysis was the SAS2H module of the SCALE sequence. Based upon fuel design, power history, and operating data for specific assemblies in the Calvert Cliffs pressurized water reactor (PWR), a computational model was developed for use with the SAS2H module of SCALE. The SAS2H module is used to perform a fuel depletion analysis to predict the isotopic concentrations in localized areas of assembly pins (pellet samples) subsequent to irradiation and cooling time. The isotopic concentrations predicted by the SAS2H module are then compared with measured concentrations of the same localized areas (axial locations) of the assembly pins to determine the accuracy of the developed model. The measured isotopic concentrations used for comparisons in the analysis are obtained from a separate report (Reference 5.6).

4. Design Inputs

The sources for the design parameters are References 5.4 through 5.11. References 5.4 and 5.5 provide information on molar masses and half-lives; the assembly design, power history and operating parameters are obtained from References 5.6 through 5.9; the cladding composition from Reference 5.10; and a list of trace elements in the fuel is derived from Reference 5.11.

4.1 Design Parameters

The half-lives of selected isotopes and molar masses of selected elements are obtained from Reference 5.4, while molar masses for selected isotopes are obtained from Reference 5.5. The half-life and molar masses are provided below within three significant figures. Precision beyond three significant figures is not necessary since the calculated isotopic concentrations from SCALE are only to three significant figures. Also, the weight per mole of enriched uranium is approximated by the weight per mole of natural uranium since the weight percent of enrichment is small.

Mole of natural uranium = 238 g,
Half-Life of ^{99}Tc = 2.13×10^5 years,
Half-Life of ^{237}Np = 2.14×10^6 years,
Half-Life of ^{241}Am = 432.7 years,
 6.02×10^{23} atoms per mole. (Reference 5.4)
Mole of ^{99}Tc = 98.9 g,
Mole of ^{237}Np = 237 g,
Mole of ^{241}Am = 241 g. (Reference 5.5)

General spent fuel characteristics for each pellet sample are presented in Table 4-1 and include the initial ^{235}U enrichment, final burnup and the cooling time (Table 2, Reference 5.6). The initial enrichment ranges from 2.453 to 3.038 wt% ^{235}U and the burnup ranges from 18.68 to 46.46 GWd/MTU. The cooling time for the samples from assembly D047 is 1,870 days, for assembly

D101 is 2,374 days, and for assembly BT03 is 2,447 days.

Assembly design parameters are presented in Table 4-2 (Table 3, Reference 5.6; and Table 4.0-1, Reference 5.7). The design is a Combustion Engineering 14 x 14 assembly with 5 guide tube positions. Assembly BT03 was used for testing materials and contains four non-fuel rods, one in each corner, and 12 poison rods in place of 16 fuel rods. The non-fuel rod dimensions and the burnable poison rod composition and dimensions for Assembly BT03 are included in Tables 4-3 through 4-4 (Table 5.0-1, Reference 5.8; Table 2.1-23, Reference 5.9). A cross section of the assemblies are presented in Figures 4-1 through 4-3 (Figures 5 through 6, Reference 5.6). The initial enrichment of ^{234}U , ^{235}U , ^{236}U and ^{238}U for each assembly type is given in Table 4-5 (Table 4, Reference 5.6).

The operating parameters in Table 4-7 include the cumulative burnups, average specific powers, average cycle boron concentrations and the fuel temperatures (Table 5, Reference 5.6). Assembly D047 was irradiated for cycles 2 through 5, D101 for cycles 2 through 4 and BT03 for cycles 1 through 4. Power history, in the form of linear heat generation rates (LHGRs), is only available for assembly D047, Table 4-6, which is used to determine the cycle cumulative burnup, Table 4-7, (Table 6, Reference 5.6). The LHGRs are used to sum the interval linear burnups over the entire cycle and are then normalized to the final burnup to produce the cumulative burnups. Assembly D101 resided in the reactor three cycles in which assembly D047 was present, and the axial locations of samples from D101 are approximately the same as those for samples from assembly D047. Therefore, the same methodology was applied for determining cumulative burnups for assembly D101 as that used for assembly D047, using the LHGRs of assembly D047 from cycles 2 through 4 (p. 19, Reference 5.6). For assembly BT03 the cumulative burnup for the entire rod was known and evaluated against the rod's final burnup. Then the cycle burnup fraction was applied to the sample's final burnup to determine the cumulative burnups (p. 19, Reference 5.6). The specific powers for each sample in Table 4-7 were determined from the cycle lengths and cumulative burnups. Fuel temperatures were known only for assembly D047 and are also included in Table 4-7 (Table 6, Reference 5.6).

Table 4-8 includes the moderator temperature and density (Table 7, Reference 5.6). The moderator temperatures obtained were based on a sinusoidal function of position, and inlet and outlet moderator temperatures of 543.2°F and 593.6°F, respectively. The moderator density was determined from the moderator temperature and the nominal pressure of 2247 psia (p. 23, Reference 5.6). The boron concentration for cycles 2 through 5 was determined by taking the first and last interval boron concentrations from the LHGR tables to linearly extrapolate the boron concentrations at the beginning and end of the cycle, which were used to calculate the cycle average boron concentration. It was assumed that the boron concentration for cycle 1 was the same as the concentration in cycle 2 (p. 19, Reference 5.6).

The composition of the cladding, Zircaloy-4, is presented in Table 4-9, and has a density of 6.56 g/cm³ (Reference 5.10). A list of trace elements in the fuel used in updating cross sections during

the depletion analysis is presented in Table 4-10 and developed with consideration of elements used in (Table 1, Reference 5.11). A generic set of light element weights for PWRs that is typically used in depletion analyses is included in Table 4-11 (Table 17, Reference 5.6). Variations in light element masses per unit fuel in different PWRs are small when compared to this generic set (p. 2-2, Reference 5.9). This data is provided in units of kg/MTUO₂ or kg/MTU depending on the units required in the analysis.

Measured isotopic concentrations are presented in Tables 4-12 and 4-13 and are given in g/gUO₂ and Ci/gUO₂, respectively (Tables 19 through 24, Reference 5.6). The measurements were performed at the Materials Characterization Center at Pacific Northwest Laboratory for fuel pellets at different axial positions in rod MKP-109 of assembly D047, rod MLA-098 of assembly D101, and rod NBD-107 of assembly BT03. Measured isotopic data is more complete for assembly D047; however, isotopic concentrations for assemblies D101 and BT03 do include the major actinides. The measurement uncertainty was obtained for assembly BT03 and is as follows: atom % burnup uncertainty of $\pm 2.5\%$, Pu uncertainty of $\pm 1.6\%$, U uncertainty of $\pm 1.6\%$, ⁹⁹Tc uncertainty of $\pm 3.5\%$ and ²³⁷Np uncertainty of $\pm 1.9\%$ (Table 4.15, Reference 5.12).

Table 4-1. Spent Fuel Characteristic Parameters for Calvert Cliffs PWR

Assembly	Rod	Axial Location from Bottom of Assembly, cm	Enrichment, wt % ²³⁵ U	Burnup, GWD/MTU	Cooling Time, days
D047	MKP109	13.20	3.038	27.35	1870
		27.70	3.038	37.12	1870
		165.22	3.038	44.34	1870
D101	MLA098	8.90	2.72	18.68	2374
		24.30	2.72	26.62	2374
		161.70	2.72	33.17	2374
BT03	NBD107	11.28	2.453	31.40	2447
		19.92	2.453	37.27	2447
		161.21	2.453	46.46	2447

Reference 5.6

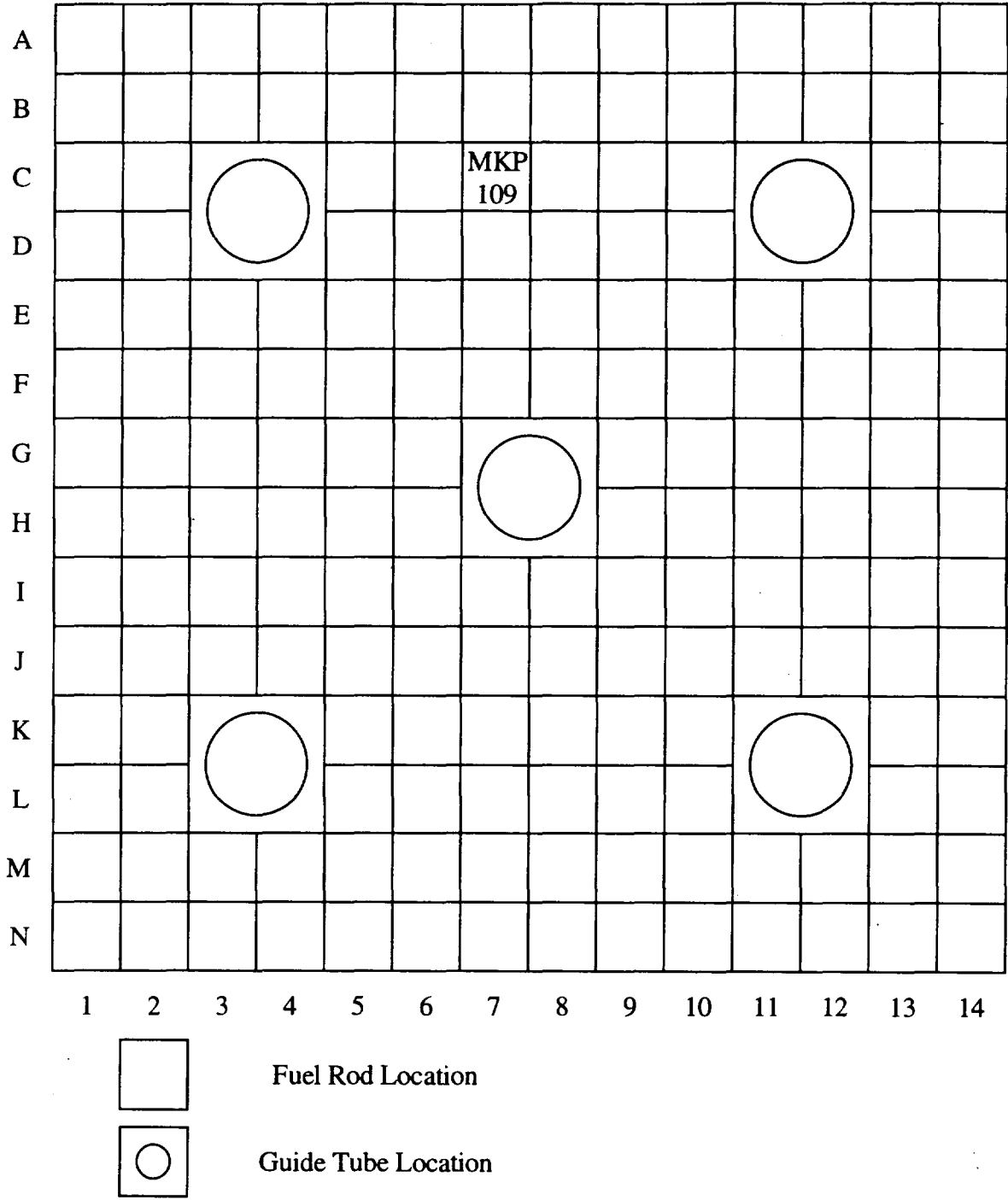
Table 4-2. Assembly Design Parameters for Calvert Cliffs PWR

Parameter	Data	
	D047 and D101	BT03
Assembly general data:		
Designer	Combustion Engineering	Combustion Engineering
Lattice	14 x 14	14 x 14
Number of Fuel Rods	176	160
Number of Guide Tubes	5	5
Number of Non-Fuel Rods	0	4
Number of Poison Rods	0	12
Assembly Pitch, cm	20.78	20.78
Fuel Rod Data:		
Type of Fuel Pellet	UO ₂	UO ₂
UO ₂ Density, % Theoretical (g/cm ³)	94.75 (10.385 ^a)	93.0 (10.193 ^a)
UO ₂ Stack Height Density, g/cm ³	10.018	10.054
Rod Pitch, cm	1.4732	1.4732
Rod Outside Diameter (OD), cm	1.1176	1.1176
Rod Inside Diameter (ID), cm	0.9855	0.9754
Pellet Diameter, cm	0.9563	0.9639
Active Fuel Length, cm	347.22	347.22
Clad Material	Zircaloy-4	Zircaloy-4
Guide Tube Data:		
Inner Radius, cm	1.314	1.314
Outer Radius, cm	1.416	1.416
Tube Material	Zircaloy-4	Zircaloy-4

^aUO₂ density is based on a theoretical density of 10.96 g/cm³.

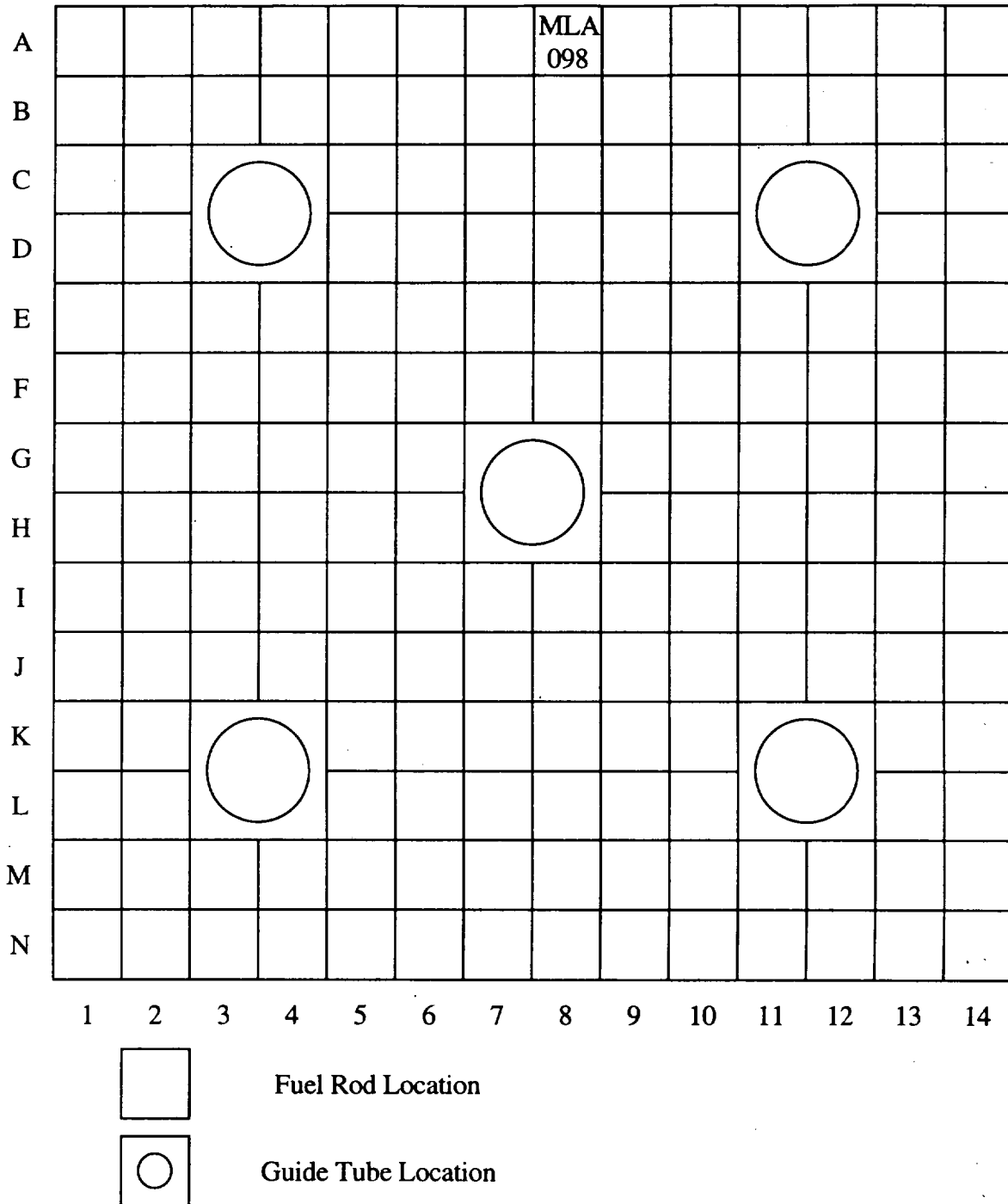
References 5.6 and 5.7

Figure 4-1. Location of Fuel Rod MKP109 in Assembly D047



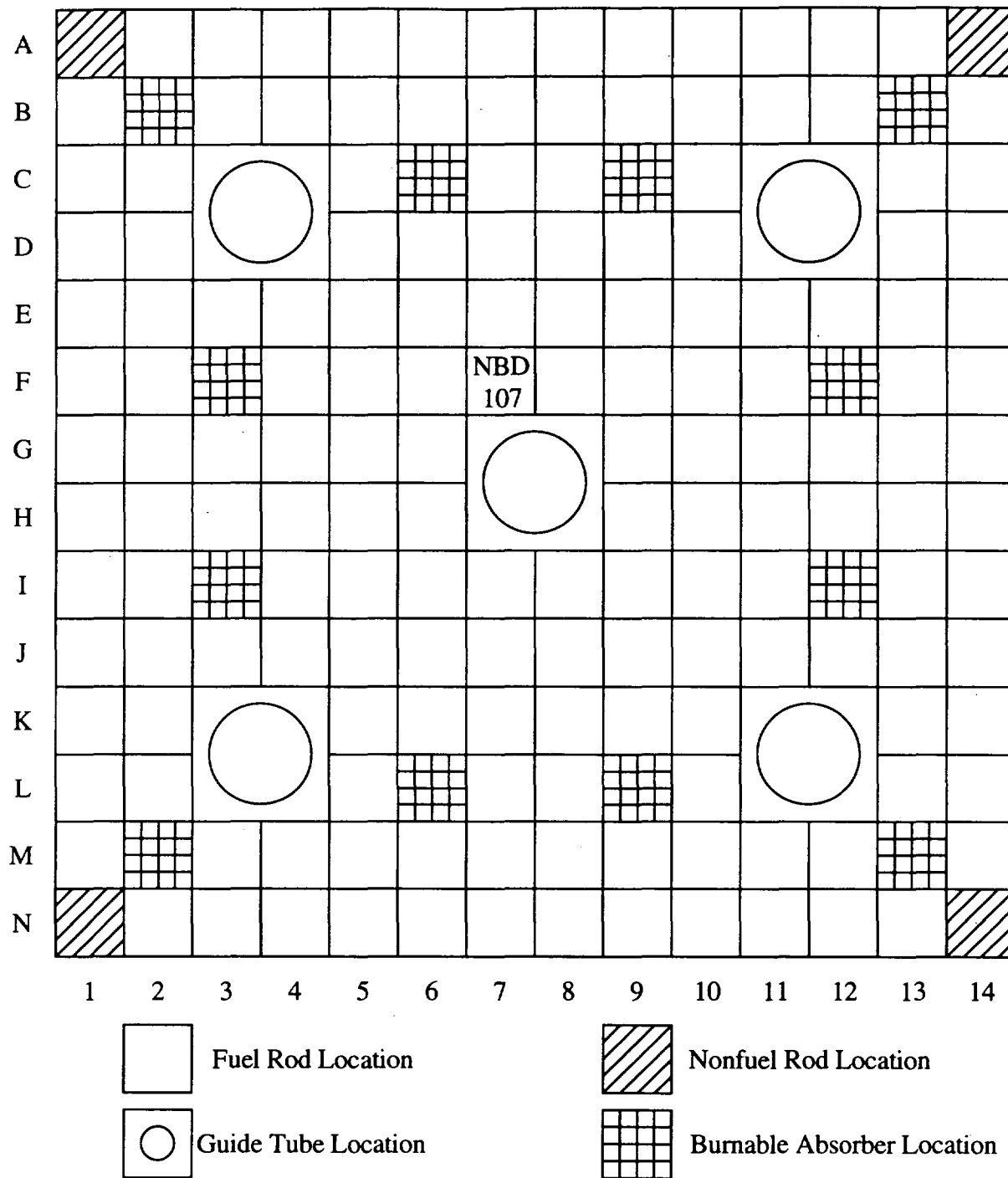
Reference 5.6

Figure 4-2. Location of Fuel Rod MLA098 in Assembly D101



Reference 5.6

Figure 4-3. Location of Fuel Rod NBD107 in Assembly BT03



Reference 5.6

Table 4-3. Burnable Absorber and Test Rod Description for Assembly BT03

Burnable Absorber Rod	
Pellet Outside Diameter, cm	0.955
Clad Inside Diameter, cm	0.9855
Clad Outside Diameter, cm	1.1176
Pellet Material	B ₄ C- Al ₂ O ₃
Absorber Clad Material	Zircaloy-4
Test Rod	
(Voids are dry gas)	
Stainless Steel Tube Inner Diameter, cm	0.660
Stainless Steel Tube Outer Diameter, cm	0.945
Clad Inner Diameter, cm	0.9855
Clad Outer Diameter, cm	1.1176
Clad Material	Zircaloy-4

References 5.8 and 5.9

Table 4-4. Burnable Absorber Atom Densities

Element/Isotope	Density, atoms/barn-cm
Al	0.039
O	0.058
C	0.00107
B-10	0.000859
B-11	0.00344

Reference 5.9

Table 4-5. Fuel Composition by Assembly

Parameter	D047	D101	BT03
Enrichment, wt % ²³⁵ U	3.038	2.72	2.453
wt % ²³⁴ U	0.027	0.024	0.022
wt % ²³⁶ U	0.014	0.013	0.011
wt % ²³⁸ U	96.921	97.243	97.514

Reference 5.6

Table 4-6. Power History and Boron Concentrations for Assembly D047

Interval (days)	Average Soluble Boron, ppm	LHGR, kW/ft		
		Axial Height of 13.20 cm	Axial Height of 27.70 cm	Axial Height of 165.22 cm
Cycle No. 2 (3-22-77 to 1-22-78)				
7.0	654	2.0	3.04	5.42
30.8	614	2.73	4.08	6.64
16.3	563	2.80	4.18	6.60
11.4	533	2.86	4.26	6.60
12.5	507	2.94	4.34	6.56
23.7	468	3.01	4.43	6.41
22.8	418	3.16	4.61	6.44
23.2	368	3.27	4.73	6.37
8.1	333	3.30	4.75	6.34
31.4	290	3.48	4.95	6.34
34.3	218	3.59	5.05	6.53
16.4	162	3.75	5.25	6.38
19.2	122	3.75	5.21	6.26
12.8	86	3.81	5.28	6.30
34.2	36	3.63	4.98	5.95
1.9	0	3.64	4.98	5.96
71.0	0	0	0	0

Table 4-6. Power History and Boron Concentrations for Assembly D047

Interval (days)	Average Soluble Boron, ppm	LHGR, kW/ft		
		Axial Height of 13.20 cm	Axial Height of 27.70 cm	Axial Height of 165.22 cm
Cycle No. 3 (4-3-78 to 4-20-79)				
7.9	883	2.63	3.85	7.47
14.4	862	2.71	3.95	7.20
19.7	837	2.14	3.11	5.04
16.8	808	3.18	4.58	7.79
16.3	775	3.35	4.81	7.78
15.4	741	3.74	5.33	8.16
39.1	684	3.71	5.23	7.45
31.2	611	3.95	5.50	7.37
31.8	545	4.08	5.64	7.20
31.8	478	4.20	5.75	7.02
44.3	368	4.38	5.93	6.93
25.0	291	0	0	0
59.1	224	4.67	6.20	6.89
28.9	120	4.95	6.52	7.12
81.0	83	0	0	0
Cycle No. 4 (7-10-79 to 10-18-80)				
46.1	960	2.79	3.97	6.59
24.0	889	2.91	4.11	6.54
22.6	827	3.07	4.29	6.43
25.7	759	3.29	4.56	6.33
30.2	706	1.58	2.17	3.05
41.2	788	1.79	2.46	3.18
50.3	720	1.72	2.35	3.00
11.0	673	3.18	4.33	5.23

Table 4-6. Power History and Boron Concentrations for Assembly D047

Interval (days)	Average Soluble Boron, ppm	LHGR, kW/ft		
		Axial Height of 13.20 cm	Axial Height of 27.70 cm	Axial Height of 165.22 cm
32.8	527	3.93	5.31	6.17
23.5	460	4.07	5.42	6.12
29.4	370	4.05	5.35	5.95
28.1	301	4.25	5.56	6.07
65.4	191	4.42	5.67	5.98
35.7	73	4.62	5.87	6.02
85.0	31	0	0	0
Cycle No. 5 (1-11-81 to 4-17-82)				
5.5	911	2.15	2.91	4.80
6.6	896	2.20	2.98	4.80
28.6	854	2.36	3.15	4.79
31.2	784	2.54	3.36	4.72
27.0	715	2.66	3.52	4.73
22.7	655	2.77	3.63	4.71
27.1	603	2.46	3.22	4.05
55.2	521	2.81	3.64	4.34
20.9	434	3.17	4.08	4.75
41.9	356	3.32	4.24	4.79
21.6	281	3.38	4.30	4.80
27.6	226	3.21	4.04	4.49
19.0	173	3.57	4.49	4.87
61.2	79	3.05	3.79	4.00

Reference 5.6

Table 4-7. Operating Data for Calvert Cliffs PWR

	Sample	Cycle 1	Cycle 2	Cycle 3	Cycle 4	Cycle 5
Uptime, days		816.0	306.0	381.7	466.0	461.1
Downtime, days		81.0	71.0	81.3	85.0	See Table 4-1
Cumulative Burnup, GWd/MTU	D047, 13.20 cm	-	5.28	12.69	20.63	27.35
	D047, 27.70 cm	-	7.56	17.78	28.42	37.12
	D047, 165.22 cm	-	9.52	21.93	34.14	44.34
	D101, 9.10 cm	-	4.78	11.49	18.68	-
	D101, 24.50 cm	-	7.08	16.65	26.62	-
	D101, 161.90 cm	-	9.25	21.31	33.17	-
	BT03, 11.28 cm	14.59	20.31	25.29	31.40	-
	BT03, 19.92 cm	17.32	24.10	31.02	37.27	-
	BT03, 161.21 cm	21.59	30.05	37.42	46.46	-
Specific Power, MW/MTU	D047, 13.20 cm	-	17.24	19.43	17.04	14.57
	D047, 27.70 cm	-	24.72	26.76	22.84	18.87
	D047, 165.22 cm	-	31.12	32.51	26.20	22.12
	D101, 9.10 cm	-	15.61	17.59	15.43	-
	D101, 24.50 cm	-	23.15	25.06	21.39	-
	D101, 161.90 cm	-	30.24	31.58	25.46	-
	BT03, 11.28 cm	17.88	18.67	13.06	13.10	-
	BT03, 19.92 cm	21.22	22.16	15.51	15.55	-
	BT03, 161.21 cm	26.46	27.62	19.33	19.39	-
Fuel Temperature, K	D047, 13.20 cm	-	829	850	775	709
	D047, 27.70 cm	-	940	927	793	712
	D047, 165.22 cm	-	997	958	794	747
Boron Concentration, ppm		330.8	330.8	469.4	503.7	492.1

Reference 5.6

Table 4-8. Moderator Conditions for Calvert Cliffs PWR

Assembly	Axial Location, cm	Total Burnup, GWd/MTU	Moderator Temperature		Density of Moderator, g/cm ³
			°F	K	
D047	13.20	27.35	543.4	557	0.7575
	27.70	37.12	544.0	558	0.7569
	165.22	44.34	566.5	570	0.7332
D101	9.10	18.68	543.3	557	0.7576
	24.50	26.62	543.8	558	0.7571
	161.90	33.17	565.7	570	0.7341
BT03	11.28	31.40	543.3	557	0.7576
	19.92	37.27	543.6	557	0.7573
	161.21	46.46	565.6	570	0.7342

Reference 5.6

Table 4-9. Composition of Zircaloy-4

Material	Weight Percent
O	0.12
Cr	0.10
Fe	0.20
Sn	1.40
Zr	98.18
Density = 6.56 g/cm ³	

Reference 5.10

Table 4-10. Nuclides Updated in SAS2H

⁸³ Kr	⁸⁵ Kr	⁸⁹ Y	⁹⁰ Sr	⁹⁵ Mo	⁹³ Zr
⁹⁴ Zr	⁹⁴ Nb	⁹⁵ Zr	⁹⁹ Tc	¹⁰¹ Ru	¹⁰³ Rh
¹⁰⁵ Rh	¹⁰⁶ Ru	¹⁰⁵ Pd	¹⁰⁸ Pd	¹⁰⁹ Ag	¹²⁴ Sb
¹³¹ Xe	¹³² Xe	¹³⁴ Cs	¹³⁵ Xe	¹³⁵ Cs	¹³⁶ Xe
¹³⁶ Ba	¹³⁷ Cs	¹³⁹ La	¹⁴¹ Pr	¹⁴³ Pr	¹⁴³ Nd
¹⁴⁴ Ce	¹⁴⁵ Nd	¹⁴⁷ Nd	¹⁴⁷ Pm	¹⁴⁷ Sm	¹⁴⁸ Pm
¹⁴⁹ Sm	¹⁵⁰ Sm	¹⁵¹ Sm	¹⁵² Sm	¹⁵³ Eu	¹⁵⁴ Eu
¹⁵⁵ Gd	¹⁵⁵ Eu				

Reference 5.11

Table 4-11. Light Element Mass per Unit of Fuel for a Typical PWR

Element	kg/MTUO ₂
O	119.0
Cr	5.2
Mn	0.29
Fe	11.0
Co	0.066
Ni	8.7
Zr	195.0
Nb	0.63
Sn	3.2

Reference 5.6

Table 4-12. Measured Concentrations of Actinides and Fission Products (g/gUO₂)

Assembly	D047	D047	D047	D101	D101	D101	BT03	BT03	BT03
Axial Height	13.20 cm	27.70 cm	165.22 cm	8.90 cm	24.30 cm	161.70 cm	11.28 cm	19.92 cm	161.21 cm
²³⁴ U	1.6E-4	1.4E-4	1.2E-4	1.400E-4	1.210E-4	1.200E-4	1.53E-4	1.27E-4	7.49E-5
²³⁵ U	8.47E-3	5.17E-3	3.54E-3	1.025E-2	6.940E-3	4.780E-3	3.86E-3	2.71E-3	1.406E-3
²³⁶ U	3.14E-3	3.53E-3	3.69E-3	2.500E-3	2.990E-3	3.260E-3	2.86E-3	3.03E-3	3.04E-3
²³⁸ U	8.425E-1	8.327E-1	8.2486E-1	8.551E-1	8.538E-1	8.422E-1	8.446E-1	8.438E-1	8.272E-1
²³⁷ Np	2.68E-4	3.56E-4	4.68E-4	-	-	-	-	-	-
²³⁸ Pu	1.01E-4	1.89E-4	2.69E-4	4.850E-5	9.690E-5	1.483E-4	1.426E-4	1.947E-4	2.842E-4
²³⁹ Pu	4.264E-3	4.357E-3	4.357E-3	3.954E-3	4.252E-3	4.187E-3	3.814E-3	3.835E-3	3.766E-3
²⁴⁰ Pu	1.719E-3	2.239E-3	2.543E-3	1.243E-3	1.766E-3	2.111E-3	2.067E-3	2.321E-3	2.599E-3
²⁴¹ Pu	6.81E-4	9.03E-4	1.020E-3	4.543E-4	6.822E-4	8.125E-4	7.260E-4	8.130E-4	8.862E-4
²⁴² Pu	2.89E-4	5.76E-4	8.40E-4	1.394E-4	3.301E-4	5.474E-4	5.463E-4	7.753E-4	1.169E-3
¹⁴³ Nd	6.13E-4	7.16E-4	7.63E-4	-	-	-	-	-	-
¹⁴⁵ Nd	5.10E-4	6.53E-4	7.44E-4	-	-	-	-	-	-
¹⁴⁹ Sm	2.9E-6	3.0E-6	4.7E-6	-	-	-	-	-	-
¹⁵⁰ Sm	2.07E-4	2.71E-4	3.61E-4	-	-	-	-	-	-
¹⁵² Sm	8.7E-5	1.04E-4	1.21E-4	-	-	-	-	-	-
¹⁵³ Eu	7.9E-5	1.09E-4	1.48E-4	-	-	-	-	-	-

Reference 5.6

Table 4-13. Measured Concentrations of Fission Products (Ci/gUO₂)

Assembly	D047	D047	D047	D101	D101	D101	BT03	BT03	BT03
Axial Height	13.20 cm	27.70 cm	165.22 cm	8.90 cm	24.30 cm	161.70 cm	11.28 cm	19.92 cm	161.21 cm
⁹⁹ Tc	9.59E-6	1.23E-5	1.35E-5	7.07E-6	9.37E-6	1.13E-5	7.70E-6	8.96E-6	1.09E-5
²³⁷ Np	-	-	-	1.23E-7	2.11E-7	2.41E-7	1.84E-7	2.26E-7	2.66E-7
²⁴¹ Am	8.56E-4	1.18E-3	1.31E-3	6.67E-4	9.91E-4	1.20E-3	1.18E-3	1.46E-3	2.18E-3

Reference 5.6

4.2 Criteria

The design of the waste package will depend on waste package configuration criticality analyses performed using an acceptable disposal criticality analysis methodology. Criteria that relate to the development and design of repository and engineered barrier components are derived from the applicable requirements and planning documents. The Engineered Barrier Design Requirements Document (EBDRD, Reference 5.15) provides requirements for engineered barrier segment design. The Repository Design Requirements Document (RDRD, Reference 5.16) provides requirements for repository design. The Controlled Design Assumptions Document (Reference 5.17) provides guidance for requirements listed in the EBDRD and RDRD which have unqualified or unconfirmed data associated with the requirement.

This analysis supports the disposal criticality analysis methodology by providing input, in the form of fuel depletion results, to benchmark calculations which address the prediction of both spent fuel isotopic compositions and their associated reactivity. These benchmark calculations will contribute to the determination of bias values in the method of critical multiplication factor calculation that is implemented by the analytic tools to be used in the disposal criticality methodology. The requirements for utilizing the bias in the method of calculation of the critical multiplication factor for disposal configurations containing spent nuclear fuel are located in Section 3.2.2.5 of the RDRD and Section 3.2.2.6 of the EBDRD. This analysis does not satisfy these requirements, but the results from this analysis will be used as input to subsequent analyses which will satisfy these requirements.

4.3 Assumptions

- 4.3.1 Due to lack of data, the boron concentration in cycle 1 is assumed to be equal to the concentration in cycle 2. The basis for this assumption originates in Reference 5.6 and is used because average boron concentrations do not typically vary greatly from cycle to cycle. This assumption is used in Section 7.2.
- 4.3.2 The cladding temperature could not be obtained, therefore, a cladding temperature of 620 K is assumed for each sample. The basis for this assumption is that the value is consistent with the expectation that the cladding temperature is closer to the moderator temperature than it is to the fuel temperature. Furthermore, it is expected that the cladding temperature will not significantly effect the resulting isotopic concentrations, since the composition contains no nuclides that are strong neutron absorbers. This assumption is used in Section 7.2.

4.4 Codes and Standards

There are no applicable codes or standards for this design analysis.

5. References

- 5.1 *Yucca Mountain Site Characterization Project Q-List*, YMP/90-55Q REV 4, Yucca Mountain Site Characterization Project.
- 5.2 *QAP-2-0 Activity Evaluations: ID #WP-20, Perform Criticality, Thermal, Structural, and Shielding Analyses*, Civilian Radioactive Waste Management System (CRWMS) Management and Operating Contractor (M&O), August 3, 1997.
- 5.3 *Quality Assurance Requirements and Description*, DOE/RW-0333P REV 7, U.S. Department of Energy (DOE) Office of Civilian Radioactive Waste Management (OCRWM).
- 5.4 *Nuclides and Isotopes*, General Electric Company, 14ed., 1989.
- 5.5 G. Audi and A. H. Wapstra, *Atomic Mass Adjustments: 'The 1995 Update to the Atomic Mass Evaluation'*, Nuclear Physics A595 Vol. 4, p. 409-480.
- 5.6 *Validation of the Scale System for PWR Spent Fuel Isotopic Composition Analyses*, ORNL/TM-12667, Oak Ridge National Laboratory, March 1995.
- 5.7 *Calvert Cliffs Nuclear Power Plant, Unit 1. Licence No. DPR-53 amendment 21: TS changes re termination of interim restrictions on peak linear heat generation rate; authorization use of Cycle 2 test assemblies; incorporation of ECCs model evaluation limits*, DOCKET-50-317-848, Baltimore Gas and Electric Co., MD, 1977.
- 5.8 *Startup Test Report*, DOCKET-50-317-463, Baltimore Gas and Electric Co., MD, 1975.
- 5.9 *Isotopic and Criticality Validation for PWR Actinide-Only Burnup Credit*, DOE/RW-0497, DOE OCRWM.
- 5.10 *Material Compositions and Number Densities for Neutronics Calculations*, Document Identification (DI) Number: BBA000000-01717-0200-00002 REV 00, CRWMS M&O.
- 5.11 *SCALE-4 Analysis of Pressurized Water Reactor Critical Configurations: Volume 2- Sequoyah Unit 2 Cycle 3*, ORNL/TM-12294/V2, March 1995.
- 5.12 *Characterization of Spent Fuel Approved Testing Material-ATM-106*, PNL-5109-106, Pacific Northwest Laboratory, October 1988.

- 5.13 *SCALE 4.3, A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation for Workstations and Personal Computers*, NUREG/CR-0200 REV 5, ORNL/NUREG/CSD-2/R5, Volumes 1-3, Oak Ridge National Laboratory.
- 5.14 *Software Qualification Report for the SCALE Modular Code System*, DI Number: 30011-2002 REV 01, CRWMS M&O.
- 5.15 *Engineered Barrier Design Requirements Document*, YMP/CM-0024, REV 00, ICN 01, DOE OCRWM.
- 5.16 *Repository Design Requirements Document*, YMP/CM-0023, REV 00, ICN 01, DOE OCRWM.
- 5.17 *Controlled Design Assumptions Document*, DI#: B00000000-01717-4600-00032 REV 04, ICN 01, CRWMS M&O.

6. Use of Computer Software

- A.** Reference 5.13 describes the SAS2H module of SCALE 4.3 that is used with the 44GROUPNDF5 cross section library to calculate the isotopic concentrations for the specified burnup and cooling time. The computer code's spatially independent point depletion model is appropriate for comparison with pellet sample measurements, and is used within the range of validation, as described in Reference 5.14, in accordance with the QAP-SI series procedures. SCALE is obtained from the Software Configuration Management in accordance with appropriate procedures. SCALE's CSCI number is 30011 V4.3 and is installed on the WPDD HP 9000, 700 Workstation with CRWMS M&O tag number 110433.

- B.** *Lotus 1-2-3 Release 5 for Windows 95* is an Acquired Software spreadsheet program as defined in QAP-SI-0. User defined formulas and/or algorithms, inputs and results, are documented in the appropriate sections.

7. Design Analysis

The SAS2H module of SCALE 4.3 is used to perform one-dimensional (1-D) neutron transport and point depletion analyses on the Calvert Cliffs samples using the preferred 44GROUPNDF5 cross-section library. To properly model the neutron flux spectrum and the nuclide composition changes, it is necessary to define the compositions, temperatures, and geometry of the fuel assembly. This is accomplished with the use of data blocks in which similar parameters are grouped together.

7.1 SCALE Input Data Blocks 1, 2, and 3

Data blocks 1 through 3 define the SCALE module to be used, the title of the input file, the cross section library to be used, and the lattice type to be modeled. The module used is SAS2H and the cross sectional library is 44GROUPNDF5, abbreviated as 44GROUP. The 44GROUP cross section library is recommended by Oak Ridge National Laboratory. Since SAS2H is only to be used for isotopic depletion/generation, the 'parm=skipshipdata' option is used so that a shipping cask shielding analysis is not performed. The title is arbitrary and should contain information that is sample specific, while the lattice type is "latticecell" to reflect the array characteristic of the assembly.

7.2 SCALE Input Data Block 4

Data block 4 defines the material compositions present in the assembly. A unique mixture number is assigned to each composition, and follows the form of mixture 1 for fuel, mixture 2 for cladding and mixture 3 for moderator.

The fuel mixture is specified as UO_2 using the stack density and isotopic weight percentages from Tables 4-2 and 4-5, respectively. Fuel temperatures for the samples from assembly D047 are presented in Table 4-7; however, no fuel temperatures for samples from the other assemblies could be obtained. Therefore, these temperatures are approximated by performing a regression analysis, based on specific power, on the available temperatures. The resulting temperatures are reported in Table 7-1. The temperature used during the first cycle of irradiation is input in data block 4. The other cycle temperatures are input in data block 9. Isotopes which are selected as needing their cross sections updated during the depletion analysis are included in the fuel mixture. A standard list of trace fuel elements is given in Table 4-10 and defined in the fuel mixture to have a concentration of 10^{-20} atoms/barn·cm.

Table 7-1. Fuel Temperatures (K) for Assemblies D101 and BT03

	Regression Slope		Regression Intercept		
	13.79207 K/(MW/MTU)		521.6644 K		
	Cycle 1	Cycle 2	Cycle 3	Cycle 4	Cycle 5
D101, 9.10 cm	-	737	764	734	-
D101, 24.50 cm	-	841	867	817	-
D101, 161.90 cm	-	939	957	873	-
BT03, 11.28 cm	768	779	702	702	-
BT03, 19.92 cm	814	827	736	736	-
BT03, 161.21 cm	887	903	788	789	-

The cladding material of Zircaloy-4 is not contained within the Standard Composition Library in SCALE 4.3 and must be defined as an arbitrary material. The cladding is defined with a density and isotopic weight percentages from Table 4-9. The cladding temperature could not be obtained, therefore, a cladding temperature of 620 K is assumed for each sample. This value is consistent with the expectation that the cladding temperature is closer to the moderator temperature than the fuel temperature. Furthermore, it is expected that the cladding temperature will not significantly effect the resulting isotopic concentrations.

The moderator temperature, density and boron concentration are given in Tables 4-7 and 4-8, and is composed of H₂O and boron. The boron is defined as an arbitrary material with the moderator density and temperature, a volume fraction equal to the average boron concentration of the first cycle irradiated, and a standard boron composition of from the Standard Composition Library designated as 5000.

Three additional mixtures must be specified. These are the Zircaloy-4 cladding of the poison rod, the composition of the poison rod and the air in between the poison rod and cladding. The air between the poison rod and the cladding is given the mixture number of 4, and is defined as nitrogen with an atom density of 5×10^{-5} atoms/barn-cm, and a temperature equal to the moderator temperature. The poison rod cladding of Zircaloy-4 is given the mixture number of 5 with a temperature also equal to the moderator temperature. Finally, the poison rod composition is given a mixture number of 6 with atom densities from Table 4-4 and a temperature equal to the moderator temperature.

7.3 SCALE Input Data Blocks 5 Through 7

The unit fuel rod cell geometry is defined in data block 5. The 'squarepitch' designation for the type of lattice is appropriate since the fuel assembly consists of a square array of fuel rods. Fuel rod, cladding and pitch dimensions are given in Table 4-2 with the mixture number for each composition defined in Section 7.2. The gap mixture is defined as 0.

Data block 6 allows the user to specify such parameters as the spatial mesh, angular quadrature and the convergence criteria. It is determined that the default values are sufficient and such options are not used in this design model.

In data block 7 the user defines general assembly data and determines the level of detail in which the assembly is to be modeled. The number of fuel rods per assembly is given in Table 4-2 and the length is calculated so that an assembly contains 1 Metric Ton of Uranium Dioxide ($MTUO_2$), using the following equation:

$$Length = \frac{1}{\frac{\pi}{4}(POD)^2(PDen)(NFR)} * \frac{10^6 g UO_2}{1 MTUO_2} \quad \text{Equation 7-1}$$

Where:

- Length = Length Required for an Assembly to Contain 1 $MTUO_2$ (cm)
- POD = Fuel Pellet Diameter (cm)
- PDen = Fuel Pellet Density (gUO_2/cm^3)
- NFR = Number of Fuel Rods

Since measured isotopic concentrations are presented in grams of isotope per gram UO_2 and SCALE presents concentrations in grams of isotope per assembly, it is possible to alter the length so that the assembly contains 1 $MTUO_2$. This is possible since the 1-D transport calculation is axially independent. Consequently, the length of the assembly does not impact the neutron flux spectrum nor the nuclide cross sections. The resulting calculated lengths for the Calvert Cliffs assemblies are 789.64 cm for assemblies D047 and D101, and 851.90 cm for assembly BT03.

Assembly D047 was irradiated for 4 cycles, D101 for 3 cycles and BT03 for 4 cycles. It is determined that approximately 80 days per cross section library is sufficient to accurately model the change in nuclide cross sections with increasing burnup, without over-burdening the SAS2H code. Therefore, the number of libraries per cycle are specified as five. To obtain the concentrations of all interested nuclides, a print level of 5 is chosen, while an input level of 2 is defined so that a Path B model may be utilized. The number of light elements are nine and are determined from Table 4-11, while the number of zones are five for assemblies D047 and D101, and six for assembly BT03, which are determined by the Path B model described in Section 7.4.

7.4 SCALE Input Data Block 8

Two different Path B models are required for Calvert Cliffs assemblies. For assemblies D047 and D101, the Path B model centralizes the guide tube with a surrounding homogenized fuel and moderator mixture which is further surrounded by the moderator between assemblies. Assembly BT03 with burnable poison and test rods, uses a Path B model with a central poison rod, a surrounding homogenized fuel and moderator mixture and further surrounded by the moderator between assemblies. The neutron flux in the samples is assumed to not be effected by the test rods because samples are taken from a rod next to the guide tube in the center of the assembly and the test rods are at the corners of the assembly. Therefore, the test rod material is not included in the Path B model.

For assemblies D047 and D101, the equations below are used to determine the number of fuel unit cells that surround the guide tube for the Path B model, by conserving the fuel to moderator volume ratio. All of the following equations used to calculate the Path B model dimensions are derived. The results of the fuel-unit-cell calculations are presented in Table 7-2, and the resulting Path B model dimensions are presented in Table 7-3.

$$x = \frac{\left(\frac{F}{M}\right)(CUCMV)}{\left(FV\right) - \left(\frac{F}{M}\right)(MV)} \quad \text{Equation 7-2}$$

$$\frac{F}{M} = \frac{(NFR)\left(\frac{\pi}{4}\right)(POD)^2}{(NFR)\left[RP^2 - \left(\frac{\pi}{4}\right)(COD)^2\right] + (NGT)\left[(2*RP)^2 - \left(\frac{\pi}{4}\right)(GTOD)^2 + \left(\frac{\pi}{4}\right)(GTID)^2\right]} \quad \text{Equation 7-3}$$

$$CUCMV = (2*RP)^2 - \left(\frac{\pi}{4}\right)(GTOD)^2 + \left(\frac{\pi}{4}\right)(GTID)^2 \quad \text{Equation 7-4}$$

$$FV = \left(\frac{\pi}{4}\right)(POD)^2 \quad \text{Equation 7-5}$$

$$MV = RP^2 - \left(\frac{\pi}{4}\right)(COD)^2 \quad \text{Equation 7-6}$$

Where:

x = Number of Unit Fuel Cells per Centralized Guide Tube

F/M = Fuel to Moderator Volume Ratio

NFR = Number of Fuel Rods

POD = Fuel Pellet Outer Diameter

RP = Rod Pitch

COD = Cladding Outer Diameter

NGT = Number of Guide Tubes

GTOD = Guide Tube Outer Diameter

GTID = Guide Tube Inner Diameter

CUCMV = Central Unit Cell Moderator Volume

FV = Fuel Volume of One Fuel Unit Cell

MV = Moderator Volume of One Fuel Unit Cell

Once the number of fuel cells per guide tube is determined the geometry of the Path B model is calculated. Since the guide tube is centralized, the dimensions of the guide tube are the same as those presented in Table 4-2.

The radius for the moderator surrounding the guide tube but still within the guide tube's 2 x 2 cell, is calculated with the following equation:

$$R_3 = \sqrt{\left(\frac{1}{\pi}\right)(2*RP)^2} \quad \text{Equation 7-7}$$

Where:

R_3 = Radius of Moderator Surrounding Guide Tube

The area of an annular region is calculated by the difference between the outer circular area and the inner circular area. Equation 7-8 is the basis for the Equations 7-9 and 7-10 which determine the radii of the homogenized fuel zone and the outer moderator zone.

$$ARA = \pi(ORAR^2 - IRAR^2) \quad \text{Equation 7-8}$$

Where:

ARA = Annular Region Area

ORAR = Outer Radius of Annular Region

IRAR = Inner Radius of Annular Region

The area of the homogenized fuel zone surrounding the guide tube's 2 x 2 cell is equal to the number of fuel unit cells surrounding the guide tube multiplied by the area of a fuel unit cell. Consequently, the radius of the homogenized fuel zone is computed with the following equation:

$$R_4 = \sqrt{\left(\frac{x}{\pi}\right)RP^2 + R_3^2} \quad \text{Equation 7-9}$$

Where:

R_4 = Radius of Homogenized Fuel and Moderator Zone

The mixture number of the homogenized fuel and moderator mixture must be specified as 500. The code then determines the composition of the region using cell averages or homogenized densities of the fuel-pin-cell.

The moderator in the channel between assemblies is determined by calculating the total moderator volume and multiplying by the fraction of unit cells in the larger unit cell of the Path B model. The total moderator volume between assemblies is determined by the assembly pitch and the fuel cell pitch multiplied by the number of unit cells. The radius of the moderator between assemblies is calculated from the following equation:

$$R_5 = \sqrt{\frac{(x+4)}{\pi * N_{Cell}} [AP^2 - (N_{Cell})(RP^2)] + R_4^2} \quad \text{Equation 7-10}$$

Where:

R_5 = Radius of Moderator Surrounding Assembly Zone

N_{Cell} = Number of Cells in Assembly

AP = Assembly Pitch

For assembly BT03, the poison rod is centralized and the Path B model dimension for zones 1 through 3 are the poison rod pellet radius, poison rod inner cladding radius and poison rod outer cladding radius, with compositions of poison rod, air and cladding, respectively. These dimensions and compositions are obtained from Tables 4-3 and 4-4.

The number of fuel unit cells needed for each centralized burnable absorber unit cell is calculated by Equation 7-2 with an exception to Equations 7-3 and 7-4. Since the centralized unit cell is different, Equations 7-3, 7-4, 7-7 and 7-10 are modified to reflect such conditions and are shown below:

$$\frac{F}{M} = \frac{(NFR)(\frac{\pi}{4})(POD)^2}{(NFR)[RP^2 - (\frac{\pi}{4})(COD)^2] + (NGT)[(2 * RP)^2 - (\frac{\pi}{4})(GTOD)^2 + (\frac{\pi}{4})(GTID)^2] + (NBPR)[RP^2 - (\frac{\pi}{4})(COD)^2] + (NNFR)[RP^2 - (\frac{\pi}{4})(COD)^2]} \quad \text{Equation 7-11}$$

$$CUCMV = (RP)^2 - (\frac{\pi}{4})(COD)^2 \quad \text{Equation 7-12}$$

$$R_3 = \sqrt{(\frac{1}{\pi})RP^2} \quad \text{Equation 7-13}$$

$$R_6 = \sqrt{\frac{(x+1)}{\pi * N_{Cell}} [AP^2 - (N_{Cell})(RP^2)] + R_5^2} \quad \text{Equation 7-14}$$

Where:

$NNFR$ = Number of Non-Fuel Rods

$NBPR$ = Number of Burnable Poison Rods

Equations 7-5, 7-6, and 7-8 are used without modification and Equation 7-9 is used to determine the radius of zone 5 of the Path B model.

Table 7-2. Calculation of Fuel Unit Cell per Guide Tube Unit Cell

Assembly	F/M	CUCMV, cm ²	FV, cm ²	MV, cm ²	x
D047 and D101	0.5090	7.8065	0.7183	1.1893	35.2000
BT03	0.4701	1.1893	0.7297	1.1893	3.2774

Table 7-3. Path B Model Dimensions

	D047 and D101		BT03	
	Radius, cm	Composition	Radius, cm	Composition
R ₁	1.3140	Moderator	0.4775	Poison Rod
R ₂	1.4160	Cladding	0.4928	Air
R ₃	1.6623	Moderator	0.5588	Cladding
R ₄	5.2039	Fuel	0.8312	Moderator
R ₅	5.2431	Moderator	1.7190	Fuel
R ₆	NA	NA	1.7319	Moderator

7.5 SCALE Input Data Blocks 9 Through 16

Data block 9 is used to describe the power history of the reactor. The specific power, fuel irradiation period, the length of downtime, the fraction of boron and moderator density, and the temperature during the cycle may all be defined. The specific power is specified in units of MW/MTUO₂ and must be converted from the average specific powers given in Table 4-7 with the relation of 238 g U is equal to 270 g UO₂, Table 7-4. The irradiation period and length of downtime are both defined in days with values presented in Table 4-7. The moderator density is constant over all cycles and the boron fraction is determined by dividing the cycle average boron concentration by the boron concentration specified in data block 4, Section 7.2. The individual cycle temperatures are calculated as described in Section 7.2 with values given in Table 7-1. The boron fraction is specified with the command 'bfrac=' and the temperature with 'temkyc='. Values for the specific power and boron fraction are presented in Table 7-4.

Table 7-4. Specific Power and Boron Fractions

	Cycle 1	Cycle 2	Cycle 3	Cycle 4	Cycle 5
Boron Fraction	1	1	1.419	1.523	1.488
Specific Power, MW/MTUO₂					
D047 MKP109, 13.20 cm	-	15.197	17.127	15.020	12.843
D047 MKP109, 27.70 cm	-	21.790	23.588	20.133	16.634
D047 MKP109, 165.22 cm	-	27.432	28.657	23.095	19.498
D101 MLA098, 9.10 cm	-	13.760	15.505	13.601	-
D101 MLA098, 24.50 cm	-	20.406	22.090	18.855	-
D101 MLA098, 161.90 cm	-	26.656	27.837	22.443	-
BT03 NBD107, 11.28 cm	15.761	16.457	11.512	11.547	-
BT03 NBD107, 19.92 cm	18.705	19.534	13.672	13.707	-
BT03 NBD107, 161.21 cm	23.324	24.347	17.039	17.092	-

Light elements and their effective weight, in kg per assembly, are entered in data block 10. Table 4-11 provides a generic set of light elements and their weights, in kg per MTUO₂. Since the fuel length is altered so that there is 1 MTUO₂ per assembly the use of light elements with weights of kg per MTUO₂ is appropriate.

Data blocks 11 through 15 describe parameters used in the radial shielding analysis of a shipping cask and are not necessary in performing the depletion analysis. Data block 16 denotes the end of the SCALE input.

7.6 Comparison of Calculated and Measured Concentrations

Comparisons of corresponding calculated and measured concentrations are performed on a percent difference basis. The difference between the measured and the calculated value is divided by the measured value to determine the accuracy of the SAS2H calculation. A positive percent difference represents an over-prediction by the code, while a negative percent difference represents an under-prediction by the code.

Measured concentrations presented in Table 4-12 have units of g of isotope per g of UO₂, while calculated concentrations presented in Table 7-5 have units of g of isotope per Metric Ton of UO₂. Therefore, the measured concentrations must be multiplied by 10⁶ gUO₂/MTUO₂ to obtain similar units. Included in Table 7-6 are the total Uranium and total Plutonium concentrations, which are determined by summing the concentrations for all reported isotopes of the particular element.

Measured concentrations are presented in Table 4-13 with units of Curies per g UO₂. The activity of a particular isotope per gram UO₂ is converted to grams of that isotope per gram UO₂ using the half-life and molar mass presented in Section 4.1 and the following equation:

$$\left(\frac{Yg}{gUO_2}\right) = \left(\frac{XCi}{gUO_2}\right) \left(\frac{3.7 \times 10^{10} Bq}{Ci}\right) \left(\frac{1}{\lambda}\right) \left(\frac{3.16 \times 10^7 s}{1yr}\right) \left(\frac{1mole}{6.02 \times 10^{23} atoms}\right) \left(\frac{Mass}{1mole}\right) \tag{Equation 7-15}$$

Where:

Y = Measured Value Used in Comparison (g isotope/g UO₂)

X = Measured Value from SAS2H (Ci isotope/g UO₂)

$$\lambda = \frac{\ln(2)}{T_{1/2}} \text{ (yr}^{-1}\text{)}$$

T_{1/2} = Half-life of Isotope (yr)

Mass = Molar Mass of Isotope

Percent differences for the actinides and fission products are presented in Table 7-7.

7.7 Results

SAS2H predicted isotopic concentrations are presented in Table 7-5. The calculated concentrations are obtained through the methodology described in Sections 7.1 through 7.5, and with the input parameters defined in Section 4.1. Included in Table 7-6 are the total Plutonium and total Uranium measured concentrations. Calculated concentrations are compared with measured concentrations as described in Section 7.6 to determine the accuracy of the SAS2H code. Results of the comparison, in the form of percent differences, are presented in Table 7-7.

Table 7-5. Calculated Concentrations (g/MTUO₂)

Assembly	D047	D047	D047	D101	D101	D101	BT03	BT03	BT03
Axial Height	13.20 cm	27.70 cm	165.22 cm	8.90 cm	24.30 cm	161.70 cm	11.28 cm	19.92 cm	161.21 cm
⁹⁹ Tc	5.96E2	7.74E2	8.93E2	4.20E2	5.78E2	6.98E2	6.56E2	7.59E2	9.05E2
²³⁴ U	1.59E2	1.38E2	1.22E2	1.58E2	1.40E2	1.28E2	1.18E2	1.09E2	9.76E1
²³⁵ U	8.33E3	5.06E3	3.30E3	1.03E4	7.05E3	5.16E3	4.66E3	3.29E3	1.95E3
²³⁶ U	3.23E3	3.65E3	3.75E3	2.44E3	2.93E3	3.18E3	2.91E3	3.05E3	3.13E3
²³⁸ U	8.37E5	8.30E5	8.24E5	8.46E5	8.40E5	8.35E5	8.37E5	8.33E5	8.25E5
²³⁷ Np	2.78E2	4.00E2	5.01E2	1.67E2	2.64E2	3.46E2	3.10E2	3.67E2	4.48E2
²³⁸ Pu	9.56E1	1.83E2	2.48E2	3.81E1	8.88E1	1.48E2	1.48E2	2.00E2	2.90E2
²³⁹ Pu	3.67E3	3.71E3	4.52E3	3.38E3	3.42E3	3.46E3	3.52E3	3.38E3	3.32E3
²⁴⁰ Pu	1.80E3	2.28E3	2.53E3	1.32E3	1.89E3	2.25E3	2.26E3	2.49E3	2.75E3
²⁴¹ Pu	6.66E2	8.51E2	9.95E2	4.25E2	6.48E2	7.99E2	7.23E2	7.95E2	8.82E2
²⁴² Pu	3.37E2	6.67E2	8.44E2	1.50E2	3.74E2	6.16E2	5.73E2	8.13E2	1.21E3
²⁴¹ Am	2.37E2	2.95E2	3.42E2	1.80E2	2.71E2	3.30E2	3.47E2	3.71E2	3.96E2
¹⁴³ Nd	6.24E2	7.29E2	7.75E2	-	-	-	-	-	-
¹⁴⁵ Nd	5.09E2	6.48E2	7.38E2	-	-	-	-	-	-
¹⁴⁹ Sm	1.87E0	2.03E0	2.23E0	-	-	-	-	-	-
¹⁵⁰ Sm	2.07E2	2.98E2	3.67E2	-	-	-	-	-	-
¹⁵² Sm	1.00E2	1.30E2	1.51E2	-	-	-	-	-	-

Table 7-5. Calculated Concentrations (g/MTUO₂)

Assembly	D047	D047	D047	D101	D101	D101	BT03	BT03	BT03
Axial Height	13.20 cm	27.70 cm	165.22 cm	8.90 cm	24.30 cm	161.70 cm	11.28 cm	19.92 cm	161.21 cm
¹⁵³ Eu	7.96E1	1.21E2	1.51E2	-	-	-	-	-	-
Total U	8.49E+05	8.39E+05	8.31E+05	8.59E+05	8.50E+05	8.43E+05	8.45E+05	8.39E+05	8.30E+05
Total Pu	6.57E+03	7.69E+03	9.14E+03	5.31E+03	6.42E+03	7.27E+03	7.55E+03	7.68E+03	8.45E+03

Table 7-6. Measured Concentrations of Total Pu and U (g/gUO₂)

Assembly	D047	D047	D047	D101	D101	D101	BT03	BT03	BT03
Axial Height	13.20 cm	27.70 cm	165.22 cm	8.90 cm	24.30 cm	161.70 cm	11.28 cm	19.92 cm	161.21 cm
Total U	8.54E-01	8.42E-01	8.32E-01	8.68E-01	8.64E-01	8.50E-01	8.51E-01	8.50E-01	8.32E-01
Total Pu	7.05E-03	8.26E-03	9.03E-03	5.84E-03	7.13E-03	7.81E-03	7.30E-03	7.94E-03	8.70E-03

Table 7-7. Percent Difference Between Measured and Calculated $[(C/M-1)*100]$

Assembly	D047	D047	D047	D101	D101	D101	BT03	BT03	BT03
Axial Height	13.20 cm	27.70 cm	165.22 cm	8.90 cm	24.30 cm	161.70 cm	11.28 cm	19.92 cm	161.21 cm
⁹⁹ Tc	5.27	6.59	12.04	0.62	4.48	4.63	44.30	43.48	40.63
²³⁴ U	-0.63	-1.43	1.67	12.86	15.70	6.67	-22.88	-14.17	30.31
²³⁵ U	-1.65	-2.13	-6.78	0.49	1.59	7.95	20.73	21.40	38.69
²³⁶ U	2.87	3.40	1.63	-2.40	-2.01	-2.45	1.75	0.66	2.96
²³⁸ U	-0.65	-0.32	-0.10	-1.06	-1.62	-0.85	-0.90	-1.28	-0.27

Table 7-7. Percent Difference Between Measured and Calculated [(C/M-1)*100]

Assembly	D047	D047	D047	D101	D101	D101	BT03	BT03	BT03
Axial Height	13.20 cm	27.70 cm	165.22 cm	8.90 cm	24.30 cm	161.70 cm	11.28 cm	19.92 cm	161.21 cm
²³⁷ Np	3.73	12.36	7.05	-4.48	-11.98	1.00	18.53	14.24	18.49
²³⁸ Pu	-5.35	-3.17	-7.81	-21.44	-8.36	-0.20	3.79	2.72	2.04
²³⁹ Pu	-13.93	-14.85	3.74	-14.52	-19.57	-17.36	-7.71	-11.86	-11.84
²⁴⁰ Pu	4.71	1.83	-0.51	6.19	7.02	6.58	9.34	7.28	5.81
²⁴¹ Pu	-2.20	-5.76	-2.45	-6.45	-5.01	-1.66	-0.41	-2.21	-0.47
²⁴² Pu	16.61	15.80	0.48	7.60	13.30	12.53	4.89	4.86	3.51
²⁴¹ Am	-5.26	-14.46	-10.67	-7.66	-6.43	-5.90	0.62	-13.05	-37.85
¹⁴³ Nd	1.79	1.82	1.57	-	-	-	-	-	-
¹⁴⁵ Nd	-0.20	-0.77	-0.81	-	-	-	-	-	-
¹⁴⁹ Sm	-35.52	-32.33	-52.55	-	-	-	-	-	-
¹⁵⁰ Sm	0.00	9.96	1.66	-	-	-	-	-	-
¹⁵² Sm	14.94	25.00	24.79	-	-	-	-	-	-
¹⁵³ Eu	0.76	11.01	2.03	-	-	-	-	-	-
Total U	-0.65	-0.32	-0.12	-1.05	-1.59	-0.81	-0.80	-1.20	-0.19
Total Pu	-6.88	-6.93	1.20	-9.01	-9.91	-6.83	-0.99	-3.29	-2.90

8. Conclusions

The accuracy in which the SAS2H module is able to predict isotopic concentrations is indicated by the percent differences presented in Table 7-7. Inspection of such results reveals that the code has a tendency to over-predict ^{99}Tc , ^{240}Pu , and ^{242}Pu , while it tends to under-predict ^{239}Pu , ^{241}Am , and ^{149}Sm . Furthermore, some calculated concentrations vary widely from the measured concentration, for example, ^{234}U ranges from -22.88% to 30.31%. Percent differences from this analysis are compared with results from Reference 5.6, in which similar calculations were performed with a previous version of SCALE and the 27burnuplib cross section library. The concentrations calculated in Reference 5.6 for the most part agree with the concentrations calculated in this analysis; however, significant differences are seen for the plutonium isotopes. Since there are few differences between the models of assemblies D047 and D101 in Reference 5.6 and the models for those assemblies contained within, it is believed that the discrepancy between calculated concentrations for plutonium isotopes is caused by a change in the cross section library. However, since there is a significant difference in the Path B model for assembly BT03 from Reference 5.6 and the model for that assembly contained within, it cannot be determined what is responsible for the differences between calculated concentrations.

Uncertainty in the measured concentration of each isotope helps to explain the deviation of the calculated concentrations from the measured concentrations. For example, the calculated concentration of total U is always within the $\pm 1.6\%$ measurement uncertainty. However, such is not always the case for the total Pu, ^{99}Tc or ^{237}Np , which generally deviate only slightly more than the measurement uncertainty. For these, the deviation (not accounted for by the measurement uncertainty) may be explained by the lack of detailed operating data. For instance, calculated concentrations for samples from assembly BT03 deviate much more than the calculated concentrations for samples from the other assemblies for the isotopes of ^{99}Tc , ^{234}U , and ^{241}Am . This may be a result of the Path B model containing an effective infinite array of BT03 assemblies, while in reality there were few BT03 assemblies in the core. Therefore, the neutron spectrum calculated by SAS2H would be slightly different than the actual spectrum effecting the calculated concentrations.

The SAS2H code normally predicts isotopic concentrations as a radial assembly average; however, measurements are performed on individual pellet samples. Therefore, local pellet conditions are modeled as closely as possible in this analysis so that a more realistic pellet composition can be determined. However, approximations made to obtain local pellet conditions will influence the calculated isotopic concentrations.

In general, the SAS2H module of SCALE is adequate in predicting isotopic concentrations for samples from Calvert Cliffs, using the methodology presented. While over-prediction or under-prediction is significant for a few isotopes, the majority of calculated concentrations are very close to the measured concentrations. The measurement uncertainty does account for some deviation between measured and calculated concentrations. More detailed operating data would be expected to improve the accuracy of the calculated concentrations in relation to the corresponding measurements. It is recommended that future analyses use more detailed data if possible.

9. Attachments

Attachment I includes nine pages and contains the input files used in the modeling of the Calvert Cliffs samples. A description of the parameters contained within the input files is found in Sections 7.1 through 7.5.

Included in Attachment II is an extraction from each of the output files, containing the following information:

- echo of the SAS2H input deck,
- time/date stamp for when the SAS2H depletion calculation was performed,
- the output extraction of information pertinent to the Radiochemical Assay evaluations from the final ORIGEN calculation of the SAS2H depletion calculation.

ccd047g27.input

=sas2h parm=skipshipdata
calvert cliffs 1 pwr, d047, rod mkp109, 13.200 cm, 27.35/mtu June 97

mixtures of fuel-pin-unit-cell:

44group latticecell
uo2 1 den=10.018 1 829
92234 0.027 92235 3.038 92236 0.014 92238 96.921 end
kr-83 1 0 1-20 829 end
kr-85 1 0 1-20 829 end
y-89 1 0 1-20 829 end
sr-90 1 0 1-20 829 end
zr-93 1 0 1-20 829 end
zr-94 1 0 1-20 829 end
zr-95 1 0 1-20 829 end
nb-94 1 0 1-20 829 end
mo-95 1 0 1-20 829 end
tc-99 1 0 1-20 829 end
ru-101 1 0 1-20 829 end
ru-106 1 0 1-20 829 end
rh-103 1 0 1-20 829 end
rh-105 1 0 1-20 829 end
pd-105 1 0 1-20 829 end
pd-108 1 0 1-20 829 end
ag-109 1 0 1-20 829 end
sb-124 1 0 1-20 829 end
xe-131 1 0 1-20 829 end
xe-132 1 0 1-20 829 end
xe-135 1 0 1-20 829 end
xe-136 1 0 1-20 829 end
cs-134 1 0 1-20 829 end
cs-135 1 0 1-20 829 end
cs-137 1 0 1-20 829 end
ba-136 1 0 1-20 829 end
la-139 1 0 1-20 829 end
pr-141 1 0 1-20 829 end
pr-143 1 0 1-20 829 end
ce-144 1 0 1-20 829 end
nd-143 1 0 1-20 829 end
nd-145 1 0 1-20 829 end
nd-147 1 0 1-20 829 end
pm-147 1 0 1-20 829 end
pm-148 1 0 1-20 829 end
sm-147 1 0 1-20 829 end
sm-149 1 0 1-20 829 end
sm-150 1 0 1-20 829 end
sm-151 1 0 1-20 829 end
sm-152 1 0 1-20 829 end
eu-153 1 0 1-20 829 end
eu-154 1 0 1-20 829 end
eu-155 1 0 1-20 829 end
gd-155 1 0 1-20 829 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 620 end
h2o 3 den=0.7575 1 557 end
arbm-bormod 0.7575 1 1 0 0 5000 100 3 330.8e-6 557 end

331 ppm boron (wt) in moderator

end comp

fuel-pin-cell geometry:

squarepitch 1.4732 0.9563 1 3 1.1176 2 0.9855 0 end

assembly and cycle parameters:

npin/assm=176 fuelnght=789.64 ncycles=4 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 1.3140 2 1.4160 3 1.6623 500 5.2039 3 5.2431
power=15.197 burn=306.0 down=71 end
power=17.127 burn=381.7 down=81.3 bfrac=1.419
temkcyc=850 end
power=15.020 burn=466.0 down=85 bfrac=1.523
temkcyc=775 end
power=12.843 burn=461.1 down=1870 bfrac=1.488
temkcyc=709 end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2

end

ccd047g37.input

=sas2h parm=skipshipdata
calvert cliffs 1 pwr, d047, rod mkp109, 27.700 cm, 37.12/mtu June 97

mixtures of fuel-pin-unit-cell:

44group latticecell
uo2 1 den=10.018 1 940
92234 0.027 92235 3.038 92236 0.014 92238 96.921 end
kr-83 1 0 1-20 940 end
kr-85 1 0 1-20 940 end
y-89 1 0 1-20 940 end
sr-90 1 0 1-20 940 end
zr-93 1 0 1-20 940 end
zr-94 1 0 1-20 940 end
zr-95 1 0 1-20 940 end
nb-94 1 0 1-20 940 end
mo-95 1 0 1-20 940 end
tc-99 1 0 1-20 940 end
ru-101 1 0 1-20 940 end
ru-106 1 0 1-20 940 end
rh-103 1 0 1-20 940 end
rh-105 1 0 1-20 940 end
pd-105 1 0 1-20 940 end
pd-108 1 0 1-20 940 end
ag-109 1 0 1-20 940 end
sb-124 1 0 1-20 940 end
xe-131 1 0 1-20 940 end
xe-132 1 0 1-20 940 end
xe-135 1 0 1-20 940 end
xe-136 1 0 1-20 940 end
cs-134 1 0 1-20 940 end
cs-135 1 0 1-20 940 end
cs-137 1 0 1-20 940 end
ba-136 1 0 1-20 940 end
la-139 1 0 1-20 940 end
pr-141 1 0 1-20 940 end
pr-143 1 0 1-20 940 end
ce-144 1 0 1-20 940 end
nd-143 1 0 1-20 940 end
nd-145 1 0 1-20 940 end
nd-147 1 0 1-20 940 end
pm-147 1 0 1-20 940 end
pm-148 1 0 1-20 940 end
sm-147 1 0 1-20 940 end
sm-149 1 0 1-20 940 end
sm-150 1 0 1-20 940 end
sm-151 1 0 1-20 940 end
sm-152 1 0 1-20 940 end
eu-153 1 0 1-20 940 end
eu-154 1 0 1-20 940 end
eu-155 1 0 1-20 940 end
gd-155 1 0 1-20 940 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 620 end
h2o 3 den=0.7569 1 558 end
arbm-bormod 0.7569 1 1 0 0 5000 100 3 330.8e-6 558 end

331 ppm boron (wt) in moderator

end comp

fuel-pin-cell geometry:

squarepitch 1.4732 0.9563 1 3 1.1176 2 0.9855 0 end

assembly and cycle parameters:

npin/assm=176 fuelnght=789.64 ncycles=4 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 1.3140 2 1.4160 3 1.6623 500 5.2039 3 5.2431
power=21.790 burn=306.0 down=71 end
power=23.588 burn=381.7 down=81.3 bfrac=1.419
temkcyc=927 end
power=20.133 burn=466.0 down=85 bfrac=1.523
temkcyc=793 end
power=16.634 burn=461.1 down=1870 bfrac=1.488
temkcyc=712 end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2

end

ccd047g44.input

=sas2h parm=skipshipdata
calvert cliffs 1 pwr, d047, rod mkp109, 165.22 cm, 44.34/mtu June 97

mixtures of fuel-pin-unit-cell:

44group latticecell
uo2 1 den=10.018 1 997
92234 0.027 92235 3.038 92236 0.014 92238 96.921 end
kr-83 1 0 1-20 997 end
kr-85 1 0 1-20 997 end
y-89 1 0 1-20 997 end
sr-90 1 0 1-20 997 end
zr-93 1 0 1-20 997 end
zr-94 1 0 1-20 997 end
zr-95 1 0 1-20 997 end
nb-94 1 0 1-20 997 end
mo-95 1 0 1-20 997 end
tc-99 1 0 1-20 997 end
ru-101 1 0 1-20 997 end
ru-106 1 0 1-20 997 end
rh-103 1 0 1-20 997 end
rh-105 1 0 1-20 997 end
pd-105 1 0 1-20 997 end
pd-108 1 0 1-20 997 end
ag-109 1 0 1-20 997 end
sb-124 1 0 1-20 997 end
xe-131 1 0 1-20 997 end
xe-132 1 0 1-20 997 end
xe-135 1 0 1-20 997 end
xe-136 1 0 1-20 997 end
cs-134 1 0 1-20 997 end
cs-135 1 0 1-20 997 end
cs-137 1 0 1-20 997 end
ba-136 1 0 1-20 997 end
la-139 1 0 1-20 997 end
pr-141 1 0 1-20 997 end
pr-143 1 0 1-20 997 end
ce-144 1 0 1-20 997 end
nd-143 1 0 1-20 997 end
nd-145 1 0 1-20 997 end
nd-147 1 0 1-20 997 end
pm-147 1 0 1-20 997 end
pm-148 1 0 1-20 997 end
sm-147 1 0 1-20 997 end
sm-149 1 0 1-20 997 end
sm-150 1 0 1-20 997 end
sm-151 1 0 1-20 997 end
sm-152 1 0 1-20 997 end
eu-153 1 0 1-20 997 end
eu-154 1 0 1-20 997 end
eu-155 1 0 1-20 997 end
gd-155 1 0 1-20 997 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 620 end
h2o 3 den=0.7332 1 570 end
arbm-bormod 0.7332 1 1 0 0 5000 100 3 330.8e-6 570 end

331 ppm boron (wt) in moderator

end comp

fuel-pin-cell geometry:

squarepitch 1.4732 0.9563 1 3 1.1176 2 0.9855 0 end

assembly and cycle parameters:

npin/assm=176 fuelnght=789.64 ncycles=4 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 1.3140 2 1.4160 3 1.6623 500 5.2039 3 5.2431
power=27.432 burn=306.0 down=71 end
power=28.657 burn=381.7 down=81.3 bfrac=1.419 end
power=23.095 burn=466.0 down=85 bfrac=1.523 end
power=19.498 burn=461.1 down=1870 bfrac=1.488 end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2

end

ccd101g18.input

```
=sas2h parm=skipshipdata
calvert cliffs 1 pwr, d101, rod mla098, 8.9 cm 18.68gwd/mtu June 97
```

```
mixtures of fuel-pin-unit-cell:
```

```
This model uses the temperature that was derived by ORNL.
```

```
44group latticecell
uo2 1 den=10.018 1 816
  92234 0.024 92235 2.72 92236 0.013 92238 97.243 end
kr-83 1 0 1-20 816 end
kr-85 1 0 1-20 816 end
y-89 1 0 1-20 816 end
sr-90 1 0 1-20 816 end
zr-93 1 0 1-20 816 end
zr-94 1 0 1-20 816 end
zr-95 1 0 1-20 816 end
nb-94 1 0 1-20 816 end
mo-95 1 0 1-20 816 end
tc-99 1 0 1-20 816 end
ru-101 1 0 1-20 816 end
ru-106 1 0 1-20 816 end
rh-103 1 0 1-20 816 end
rh-105 1 0 1-20 816 end
pd-105 1 0 1-20 816 end
pd-108 1 0 1-20 816 end
ag-109 1 0 1-20 816 end
sb-124 1 0 1-20 816 end
xe-131 1 0 1-20 816 end
xe-132 1 0 1-20 816 end
xe-135 1 0 1-20 816 end
xe-136 1 0 1-20 816 end
cs-134 1 0 1-20 816 end
cs-135 1 0 1-20 816 end
cs-137 1 0 1-20 816 end
ba-136 1 0 1-20 816 end
la-139 1 0 1-20 816 end
pr-141 1 0 1-20 816 end
pr-143 1 0 1-20 816 end
ce-144 1 0 1-20 816 end
nd-143 1 0 1-20 816 end
nd-145 1 0 1-20 816 end
nd-147 1 0 1-20 816 end
pm-147 1 0 1-20 816 end
pm-148 1 0 1-20 816 end
sm-147 1 0 1-20 816 end
sm-149 1 0 1-20 816 end
sm-150 1 0 1-20 816 end
sm-151 1 0 1-20 816 end
sm-152 1 0 1-20 816 end
eu-153 1 0 1-20 816 end
eu-154 1 0 1-20 816 end
eu-155 1 0 1-20 816 end
gd-155 1 0 1-20 816 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 620 end
h2o 3 den=0.7576 1 557 end
arbm-bormod 0.7576 1 1 0 0 5000 100 3 330.8e-6 557 end
```

```
331 ppm boron (wt) in moderator
```

```
end comp
```

```
fuel-pin-cell geometry:
```

```
squarepitch 1.4732 0.9563 1 3 1.1176 2 0.9855 0 end
```

```
assembly and cycle parameters:
```

```
npin/assm=176 fuelnght=789.64 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 1.3140 2 1.4160 3 1.6623 500 5.2039 3 5.2431
power=13.760 burn=306.0 down=71 end
power=15.505 burn=381.7 down=81.3 bfrac=1.419 end
power=13.601 burn=466.0 down=2374 bfrac=1.523 end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2
```

```
end
```

ccd101g26.input

```
=sas2h parm=skipshipdata
calvert cliffs 1 pwr, d101, rod mla098, 24.5 cm 26.62gwd/mtu June 97
```

```
mixtures of fuel-pin-unit-cell:
```

```
44group latticecell
uo2 1 den=10.018 1 841
  92234 0.024 92235 2.72 92236 0.013 92238 97.243 end
kr-83 1 0 1-20 841 end
kr-85 1 0 1-20 841 end
y-89 1 0 1-20 841 end
sr-90 1 0 1-20 841 end
zr-93 1 0 1-20 841 end
zr-94 1 0 1-20 841 end
zr-95 1 0 1-20 841 end
nb-94 1 0 1-20 841 end
mo-95 1 0 1-20 841 end
tc-99 1 0 1-20 841 end
ru-101 1 0 1-20 841 end
ru-106 1 0 1-20 841 end
rh-103 1 0 1-20 841 end
rh-105 1 0 1-20 841 end
pd-105 1 0 1-20 841 end
pd-108 1 0 1-20 841 end
ag-109 1 0 1-20 841 end
sb-124 1 0 1-20 841 end
xe-131 1 0 1-20 841 end
xe-132 1 0 1-20 841 end
xe-135 1 0 1-20 841 end
xe-136 1 0 1-20 841 end
cs-134 1 0 1-20 841 end
cs-135 1 0 1-20 841 end
cs-137 1 0 1-20 841 end
ba-136 1 0 1-20 841 end
la-139 1 0 1-20 841 end
pr-141 1 0 1-20 841 end
pr-143 1 0 1-20 841 end
ce-144 1 0 1-20 841 end
nd-143 1 0 1-20 841 end
nd-145 1 0 1-20 841 end
nd-147 1 0 1-20 841 end
pm-147 1 0 1-20 841 end
pm-148 1 0 1-20 841 end
sm-147 1 0 1-20 841 end
sm-149 1 0 1-20 841 end
sm-150 1 0 1-20 841 end
sm-151 1 0 1-20 841 end
sm-152 1 0 1-20 841 end
eu-153 1 0 1-20 841 end
eu-154 1 0 1-20 841 end
eu-155 1 0 1-20 841 end
gd-155 1 0 1-20 841 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 620 end
h2o 3 den=0.7571 1 558 end
arbm-bormod 0.7571 1 1 0 0 5000 100 3 330.8e-6 558 end
```

```
331 ppm boron (wt) in moderator
```

```
end comp
```

```
fuel-pin-cell geometry:
```

```
squarepitch 1.4732 0.9563 1 3 1.1176 2 0.9855 0 end
```

```
assembly and cycle parameters:
```

```
npin/assm=176 fuelnght=789.64 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 1.3140 2 1.4160 3 1.6623 500 5.2039 3 5.2431
power=20.406 burn=306.0 down=71 end
power=22.090 burn=381.7 down=81.3 bfrac=1.419
temkcy=867 end
power=18.855 burn=466.0 down=2374 bfrac=1.523
temkcy=817 end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2
```

```
end
```

ccd101g33.input

=sas2h parm=skipshipdata
calvert cliffs 1 pwr, d101, rod mla098, 161.7 cm 33.17gwd/mtu June 97

mixtures of fuel-pin-unit-cell:

```
44group latticecell
uo2 1 den=10.018 1 939
  92234 0.024 92235 2.72 92236 0.013 92238 97.243 end
kr-83 1 0 1-20 939 end
kr-85 1 0 1-20 939 end
y-89 1 0 1-20 939 end
sr-90 1 0 1-20 939 end
zr-93 1 0 1-20 939 end
zr-94 1 0 1-20 939 end
zr-95 1 0 1-20 939 end
nb-94 1 0 1-20 939 end
mo-95 1 0 1-20 939 end
tc-99 1 0 1-20 939 end
ru-101 1 0 1-20 939 end
ru-106 1 0 1-20 939 end
rh-103 1 0 1-20 939 end
rh-105 1 0 1-20 939 end
pd-105 1 0 1-20 939 end
pd-108 1 0 1-20 939 end
ag-109 1 0 1-20 939 end
sb-124 1 0 1-20 939 end
xe-131 1 0 1-20 939 end
xe-132 1 0 1-20 939 end
xe-135 1 0 1-20 939 end
xe-136 1 0 1-20 939 end
cs-134 1 0 1-20 939 end
cs-135 1 0 1-20 939 end
cs-137 1 0 1-20 939 end
ba-136 1 0 1-20 939 end
la-139 1 0 1-20 939 end
pr-141 1 0 1-20 939 end
pr-143 1 0 1-20 939 end
ce-144 1 0 1-20 939 end
nd-143 1 0 1-20 939 end
nd-145 1 0 1-20 939 end
nd-147 1 0 1-20 939 end
pm-147 1 0 1-20 939 end
pm-148 1 0 1-20 939 end
sm-147 1 0 1-20 939 end
sm-149 1 0 1-20 939 end
sm-150 1 0 1-20 939 end
sm-151 1 0 1-20 939 end
sm-152 1 0 1-20 939 end
eu-153 1 0 1-20 939 end
eu-154 1 0 1-20 939 end
eu-155 1 0 1-20 939 end
gd-155 1 0 1-20 939 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 620 end
h2o 3 den=0.7341 1 570 end
arbm-bormod 0.7341 1 1 0 0 5000 100 3 330.8e-6 570 end
```

331 ppm boron (wt) in moderator

end comp

fuel-pin-cell geometry:

```
squarepitch 1.4732 0.9563 1 3 1.1176 2 0.9855 0 end
```

assembly and cycle parameters:

```
npin/assm=176 fuelnght=789.64 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 1.3140 2 1.4160 3 1.6623 500 5.2039 3 5.2431
power=26.656 burn=306.0 down=71 end
power=27.837 burn=381.7 down=81.3 bfrac=1.419
temkcy=957 end
power=22.443 burn=466.0 down=2374 bfrac=1.523
temkcy=873 end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2
```

end

ccbt03g31.input

```
=sas2h parm=skipshipdata
calvert cliffs 1 pwr, bt03, rod nbd107, 11.28 cm 31.40gwd June 97
```

```
' mixtures of fuel-pin-unit-cell:
```

```
44group latticecell
uo2 1 den=10.054 1 768
  92234 0.022 92235 2.453 92236 0.011 92238 97.514 end
kr-83 1 0 1-20 768 end
kr-85 1 0 1-20 768 end
y-89 1 0 1-20 768 end
sr-90 1 0 1-20 768 end
zr-93 1 0 1-20 768 end
zr-94 1 0 1-20 768 end
zr-95 1 0 1-20 768 end
nb-94 1 0 1-20 768 end
mo-95 1 0 1-20 768 end
tc-99 1 0 1-20 768 end
ru-101 1 0 1-20 768 end
ru-106 1 0 1-20 768 end
rh-103 1 0 1-20 768 end
rh-105 1 0 1-20 768 end
pd-105 1 0 1-20 768 end
pd-108 1 0 1-20 768 end
ag-109 1 0 1-20 768 end
sb-124 1 0 1-20 768 end
xe-131 1 0 1-20 768 end
xe-132 1 0 1-20 768 end
xe-135 1 0 1-20 768 end
xe-136 1 0 1-20 768 end
cs-134 1 0 1-20 768 end
cs-135 1 0 1-20 768 end
cs-137 1 0 1-20 768 end
ba-136 1 0 1-20 768 end
la-139 1 0 1-20 768 end
pr-141 1 0 1-20 768 end
pr-143 1 0 1-20 768 end
ce-144 1 0 1-20 768 end
nd-143 1 0 1-20 768 end
nd-145 1 0 1-20 768 end
nd-147 1 0 1-20 768 end
pm-147 1 0 1-20 768 end
pm-148 1 0 1-20 768 end
sm-147 1 0 1-20 768 end
sm-149 1 0 1-20 768 end
sm-150 1 0 1-20 768 end
sm-151 1 0 1-20 768 end
sm-152 1 0 1-20 768 end
eu-153 1 0 1-20 768 end
eu-154 1 0 1-20 768 end
eu-155 1 0 1-20 768 end
gd-155 1 0 1-20 768 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 620 end
h2o 3 den=0.7576 1 557 end
arbm-bormod 0.7576 1 1 0 0 5000 100 3 330.8e-6 557 end
n 4 0 5-5 557 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 5 1.0 557 end
o 6 0 0.058 557 end
al 6 0 0.039 557 end
c 6 0 0.00107 557 end
b-10 6 0 0.000859 557 end
b-11 6 0 0.0034 557 end
```

```
' 331 ppm boron (wt) in moderator
```

```
end comp
```

```
fuel-pin-cell geometry:
```

```
squarepitch 1.4732 0.9639 1 3 1.1176 2 0.9754 0 end
```

```
assembly and cycle parameters:
```

```
npin/assm=160 fuelnht=851.90 ncycles=4 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=6 end
6 0.4775 4 0.4928 5 0.5588 3 0.8312 500 1.7190 3 1.7319
power=15.761 burn=816.0 down=81 end
power=16.457 burn=306.0 down=71 temkcy=779 end
power=11.512 burn=381.7 down=81.3 bfrac=1.419
temkcy=702 end
power=11.547 burn=466.0 down=2447 bfrac=1.523
temkcy=702 end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2
```

```
end
```


ccbt03g37.input

```
=sas2h parm=skipshipdata
calvert cliffs 1 pwr, bt03, rod nbd107, 19.92 cm 37.27gwd June 97
```

```
-----
mixtures of fuel-pin-unit-cell:
```

```
44group latticecell
uo2 1 den=10.054 1 814
  92234 0.022 92235 2.453 92236 0.011 92238 97.514 end
kr-83 1 0 1-20 814 end
kr-85 1 0 1-20 814 end
y-89 1 0 1-20 814 end
sr-90 1 0 1-20 814 end
zr-93 1 0 1-20 814 end
zr-94 1 0 1-20 814 end
zr-95 1 0 1-20 814 end
nb-94 1 0 1-20 814 end
mo-95 1 0 1-20 814 end
tc-99 1 0 1-20 814 end
ru-101 1 0 1-20 814 end
ru-106 1 0 1-20 814 end
rh-103 1 0 1-20 814 end
rh-105 1 0 1-20 814 end
pd-105 1 0 1-20 814 end
pd-108 1 0 1-20 814 end
ag-109 1 0 1-20 814 end
sb-124 1 0 1-20 814 end
xe-131 1 0 1-20 814 end
xe-132 1 0 1-20 814 end
xe-135 1 0 1-20 814 end
xe-136 1 0 1-20 814 end
cs-134 1 0 1-20 814 end
cs-135 1 0 1-20 814 end
cs-137 1 0 1-20 814 end
ba-136 1 0 1-20 814 end
la-139 1 0 1-20 814 end
pr-141 1 0 1-20 814 end
pr-143 1 0 1-20 814 end
ce-144 1 0 1-20 814 end
nd-143 1 0 1-20 814 end
nd-145 1 0 1-20 814 end
nd-147 1 0 1-20 814 end
pm-147 1 0 1-20 814 end
pm-148 1 0 1-20 814 end
sm-147 1 0 1-20 814 end
sm-149 1 0 1-20 814 end
sm-150 1 0 1-20 814 end
sm-151 1 0 1-20 814 end
sm-152 1 0 1-20 814 end
eu-153 1 0 1-20 814 end
eu-154 1 0 1-20 814 end
eu-155 1 0 1-20 814 end
gd-155 1 0 1-20 814 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 620 end
h2o 3 den=0.7573 1 557 end
arbm-bormod 0.7573 1 1 0 0 5000 100 3 330.8e-6 557 end

n 4 0 5-5 557 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 5 1.0 557 end
o 6 0 0.058 557 end
al 6 0 0.039 557 end
c 6 0 0.00107 557 end
b-10 6 0 0.000859 557 end
b-11 6 0 0.0034 557 end
```

```
-----
331 ppm boron (wt) in moderator
```

```
end comp
```

```
-----
fuel-pin-cell geometry:
```

```
squarepitch 1.4732 0.9639 1 3 1.1176 2 0.9754 0 end
```

```
-----
assembly and cycle parameters:
```

```
npin/assm=160 fuelngth=851.90 ncycles=4 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=6 end
6 0.4775 4 0.4928 5 0.5588 3 0.8312 500 1.7190 3 1.7319
power=18.705 burn=816.0 down=81 end
power=19.534 burn=306.0 down=71 temkcyc=827 end
power=13.672 burn=381.7 down=81.3 bfrac=1.419
temkcyc=736 end
power=13.707 burn=466.0 down=2447 bfrac=1.523
temkcyc=736 end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2
```

```
-----
end
```

ccbt03g46.input

sas2h parm=skipshipdata

calvert cliffs 1 pwr, br03, rod nbd107, 161.21 cm 46.46gwd June 97

```

-----
' mixtures of fuel-pin-unit-cell:

```

44group latticecell

uo2 1 den=10.054 1 887

92234 0.022 92235 2.453 92236 0.011 92238 97.514 end

kr-83 1 0 1-20 887 end

kr-85 1 0 1-20 887 end

y-89 1 0 1-20 887 end

sr-90 1 0 1-20 887 end

zr-93 1 0 1-20 887 end

zr-94 1 0 1-20 887 end

zr-95 1 0 1-20 887 end

nb-94 1 0 1-20 887 end

mo-95 1 0 1-20 887 end

tc-99 1 0 1-20 887 end

ru-101 1 0 1-20 887 end

ru-106 1 0 1-20 887 end

rh-103 1 0 1-20 887 end

rh-105 1 0 1-20 887 end

pd-105 1 0 1-20 887 end

pd-108 1 0 1-20 887 end

ag-109 1 0 1-20 887 end

sb-124 1 0 1-20 887 end

xe-131 1 0 1-20 887 end

xe-132 1 0 1-20 887 end

xe-135 1 0 1-20 887 end

xe-136 1 0 1-20 887 end

cs-134 1 0 1-20 887 end

cs-135 1 0 1-20 887 end

cs-137 1 0 1-20 887 end

ba-136 1 0 1-20 887 end

la-139 1 0 1-20 887 end

pr-141 1 0 1-20 887 end

pr-143 1 0 1-20 887 end

ce-144 1 0 1-20 887 end

nd-143 1 0 1-20 887 end

nd-145 1 0 1-20 887 end

nd-147 1 0 1-20 887 end

pm-147 1 0 1-20 887 end

pm-148 1 0 1-20 887 end

sm-147 1 0 1-20 887 end

sm-149 1 0 1-20 887 end

sm-150 1 0 1-20 887 end

sm-151 1 0 1-20 887 end

sm-152 1 0 1-20 887 end

eu-153 1 0 1-20 887 end

eu-154 1 0 1-20 887 end

eu-155 1 0 1-20 887 end

gd-155 1 0 1-20 887 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40

40000 98.18 2 1.0 620 end

h2o 3 den=0.7342 1 570 end

arbm-bormod 0.7342 1 1 0 0 5000 100 3 330.8e-6 570 end

n 4 0 5-5 570 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40

40000 98.18 5 1.0 570 end

o 6 0 0.058 570 end

al 6 0 0.039 570 end

c 6 0 0.00107 570 end

b-10 6 0 0.000859 570 end

b-11 6 0 0.0034 570 end

```

' 331 ppm boron (wt) in moderator
-----

```

end comp

```

-----
' fuel-pin-cell geometry:

```

squarepitch 1.4732 0.9639 1 3 1.1176 2 0.9754 0 end

```

-----
' assembly and cycle parameters:

```

npin/assm=160 fuelngth=851.90 ncycles=4 nlib/cyc=5

printlevel=5 lightel=9 inplevel=2 numztotal=6 end

6 0.4775 4 0.4928 5 0.5588 3 0.8312 500 1.7190 3 1.7319

power=23.324 burn=816.0 down=81 end

power=24.347 burn=306.0 down=71 temkyc=903 end

power=17.039 burn=381.7 down=81.3 bfrac=1.419

temkyc=788 end

power=17.092 burn=466.0 down=2447 bfrac=1.523

temkyc=789 end

o 119 cr 5.2 mn 0.29

fe 11.0 co 0.066 ni 8.7

zr 195 nb 0.63 sn 3.2

```

-----
end

```

d047g27.sum

```

0.....
.
.          SCALE4.3  Bulletin Board
.          -----
.          Welcome to SCALE-4.3.
.
.
1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  calvert cliffs 1 pwr. d047, rod mkp109, 13.200 cm, 27.35/mtu June 97
.
.   mixtures of fuel-pin-unit-cell:
.
.   44group          latticecell
.   uo2 1 den=10.018 1 829
.       92234 0.027 92235 3.038 92236 0.014 92238 96.921 end
.   kr-83 1 0 1-20 829 end
.   kr-85 1 0 1-20 829 end
.   y-89 1 0 1-20 829 end
.   sr-90 1 0 1-20 829 end
.   zr-93 1 0 1-20 829 end
.   zr-94 1 0 1-20 829 end
.   zr-95 1 0 1-20 829 end
.   nb-94 1 0 1-20 829 end
.   mo-95 1 0 1-20 829 end
.   tc-99 1 0 1-20 829 end
.   ru-101 1 0 1-20 829 end
.   ru-106 1 0 1-20 829 end
.   rh-103 1 0 1-20 829 end
.   rh-105 1 0 1-20 829 end
.   pd-105 1 0 1-20 829 end
.   pd-108 1 0 1-20 829 end
.   ag-109 1 0 1-20 829 end
.   sb-124 1 0 1-20 829 end
.   xe-131 1 0 1-20 829 end
.   xe-132 1 0 1-20 829 end
.   xe-135 1 0 1-20 829 end
.   xe-136 1 0 1-20 829 end
.   cs-134 1 0 1-20 829 end
.   cs-135 1 0 1-20 829 end
.   cs-137 1 0 1-20 829 end
.   ba-136 1 0 1-20 829 end
.   la-139 1 0 1-20 829 end
.   pr-141 1 0 1-20 829 end
.   pr-143 1 0 1-20 829 end
.   ce-144 1 0 1-20 829 end
.   nd-143 1 0 1-20 829 end
.   nd-145 1 0 1-20 829 end
.   nd-147 1 0 1-20 829 end
.   pm-147 1 0 1-20 829 end
.   pm-148 1 0 1-20 829 end
.   sm-147 1 0 1-20 829 end
.   sm-149 1 0 1-20 829 end
.   sm-150 1 0 1-20 829 end
.   sm-151 1 0 1-20 829 end
.   sm-152 1 0 1-20 829 end
.   eu-153 1 0 1-20 829 end
.   eu-154 1 0 1-20 829 end
.   eu-155 1 0 1-20 829 end
.   qd-155 1 0 1-20 829 end
.   arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
.               40000 98.18 2 1.0 620 end
.   h2o 3 den=0.7575 1 557 end
.   arbm-bormod 0.7575 1 1 0 0 5000 100 3 330.8e-6 557 end
.
.   331 ppm boron (wt) in moderator
.
.   end comp
.
.
.   fuel-pin-cell geometry:
.
.   squarepitch 1.4732 0.9563 1 3 1.1176 2 0.9855 0 end
.
.
.   assembly and cycle parameters:
.
.   npin/assm=176 fuelnght=789.64 ncycles=4 nlib/cyc=5
.   printlevel=5 lightel=9 inplevel=2 numtotal=5 end
.   3 1.3140 2 1.4160 3 1.6623 500 5.2039 3 5.2431
.   power=15.197 burn=306.0 down=71 end
.   power=17.127 burn=381.7 down=81.3 bfrac=1.419 temkcyc=850 end
.   power=15.020 burn=466.0 down=85 bfrac=1.523 temkcyc=775 end
.   power=12.843 burn=461.1 down=1870 bfrac=1.488 temkcyc=709 end
.   o 119 cr 5.2 mn 0.29
.   fe 11.0 co 0.066 ni 8.7
.   zr 195 nb 0.63 sn 3.2
.
.
.
1  sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
.  sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
.  ss aa aa ss 22 hh hh
.  ss aa aa ss 22 hh hh
.  ss aa aa ss 22 hh hh
.  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
.  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
.  ss aa aa ss 22 hh hh
.  ss aa aa ss 22 hh hh
.  ss aa aa ss 22 hh hh
.  sssssssssss aa aa sssssssssss 2222222222 hh hh
.  sssssssssss aa aa sssssssssss 2222222222 hh hh
0
.
nn nn iiiiiiiiii cccccccccc hh hh oooooooooo 11

```


d047g44.sum

```

0.....
.
.          SCALE4.3  Bulletin  Board
.          -----
.
.          Welcome to SCALE-4.3.
.
.
1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  calvert cliffs 1 pwr, d047, rod mkp109, 165.22 cm, 44.34/mtu June 97
.
.   mixtures of fuel-pin-unit-cell:
.
44group          latticecell
uo2 1 den=10.018 1 997
    92234 0.027 92235 3.038 92236 0.014 92238 96.921 end
kr-83 1 0 1-20 997 end
kr-85 1 0 1-20 997 end
y-89 1 0 1-20 997 end
sr-90 1 0 1-20 997 end
zr-93 1 0 1-20 997 end
zr-94 1 0 1-20 997 end
zr-95 1 0 1-20 997 end
nb-94 1 0 1-20 997 end
mo-95 1 0 1-20 997 end
tc-99 1 0 1-20 997 end
ru-101 1 0 1-20 997 end
ru-106 1 0 1-20 997 end
rh-103 1 0 1-20 997 end
rh-105 1 0 1-20 997 end
pd-105 1 0 1-20 997 end
pd-108 1 0 1-20 997 end
ag-109 1 0 1-20 997 end
sb-124 1 0 1-20 997 end
xe-131 1 0 1-20 997 end
xe-132 1 0 1-20 997 end
xe-135 1 0 1-20 997 end
xe-136 1 0 1-20 997 end
cs-134 1 0 1-20 997 end
cs-135 1 0 1-20 997 end
cs-137 1 0 1-20 997 end
ba-136 1 0 1-20 997 end
la-139 1 0 1-20 997 end
pr-141 1 0 1-20 997 end
pr-143 1 0 1-20 997 end
ce-144 1 0 1-20 997 end
nd-143 1 0 1-20 997 end
nd-145 1 0 1-20 997 end
nd-147 1 0 1-20 997 end
pm-147 1 0 1-20 997 end
pm-148 1 0 1-20 997 end
sm-147 1 0 1-20 997 end
sm-149 1 0 1-20 997 end
sm-150 1 0 1-20 997 end
sm-151 1 0 1-20 997 end
sm-152 1 0 1-20 997 end
eu-153 1 0 1-20 997 end
eu-154 1 0 1-20 997 end
eu-155 1 0 1-20 997 end
gd-155 1 0 1-20 997 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
            40000 98.18 2 1.0 620 end
h2o 3 den=0.7332 1 570 end
arbm-bormod 0.7332 1 1 0 0 5000 100 3 330.8e-6 570 end
.
.   331 ppm boron (wt) in moderator
.
end comp
.
.
.
.
.   fuel-pin-cell geometry:
.
squarepitch 1.4732 0.9563 1 3 1.1176 2 0.9855 0 end
.
.
.
.   assembly and cycle parameters:
.
npin/assm=176 fuelnght=789.64 ncycles=4 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 1.3140 2 1.4160 3 1.6623 500 5.2039 3 5.2431
power=27.432 burn=306.0 down=71 end
power=28.657 burn=381.7 down=81.3 bfrac=1.419 end
power=23.095 burn=466.0 down=85 bfrac=1.523 end
power=19.498 burn=461.1 down=1870 bfrac=1.488 end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2
.
.
.
1 ssssssssssss aaaaaaaaaa ssssssssssss 222222222222 hh hh
  ssssssssssss aaaaaaaaaa ssssssssssss 222222222222 hh hh
  ss ss aa aa ss ss 22 22 hh hh
  ss aa aa aa ss ss 22 22 hh hh
  ss aa aa aa ss ss 22 22 hh hh
  ssssssssssss aaaaaaaaaa ssssssssssss 22 hhhhhhhhhhhh
  ssssssssssss aaaaaaaaaa ssssssssssss 22 hhhhhhhhhhhh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  ssssssssssss aa aa ssssssssssss 222222222222 hh hh
  ssssssssssss aa aa ssssssssssss 222222222222 hh hh
0
nn nn iiiiiiiiii cccccccccc hh hh oooooooooooo 11

```


d101g18.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  calvert cliffs 1 pwr. d101. rod mla098, 8.9 cm 18.68gwd/mtu June 97
  mixtures of fuel-pin-unit-cell:

44group latticecell
uo2 1 den=10.018 1 737
  92234 0.024 92235 2.72 92236 0.013 92238 97.243 end
kr-83 1 0 1-20 737 end
kr-85 1 0 1-20 737 end
y-89 1 0 1-20 737 end
sr-90 1 0 1-20 737 end
zr-93 1 0 1-20 737 end
zr-94 1 0 1-20 737 end
zr-95 1 0 1-20 737 end
nb-94 1 0 1-20 737 end
mo-95 1 0 1-20 737 end
tc-99 1 0 1-20 737 end
ru-101 1 0 1-20 737 end
ru-106 1 0 1-20 737 end
rh-103 1 0 1-20 737 end
rh-105 1 0 1-20 737 end
pd-105 1 0 1-20 737 end
pd-108 1 0 1-20 737 end
ag-109 1 0 1-20 737 end
sb-124 1 0 1-20 737 end
xe-131 1 0 1-20 737 end
xe-132 1 0 1-20 737 end
xe-135 1 0 1-20 737 end
xe-136 1 0 1-20 737 end
cs-134 1 0 1-20 737 end
cs-135 1 0 1-20 737 end
cs-137 1 0 1-20 737 end
ba-136 1 0 1-20 737 end
la-139 1 0 1-20 737 end
pr-141 1 0 1-20 737 end
pr-143 1 0 1-20 737 end
ce-144 1 0 1-20 737 end
nd-143 1 0 1-20 737 end
nd-145 1 0 1-20 737 end
nd-147 1 0 1-20 737 end
pm-147 1 0 1-20 737 end
pm-148 1 0 1-20 737 end
sm-147 1 0 1-20 737 end
sm-149 1 0 1-20 737 end
sm-150 1 0 1-20 737 end
sm-151 1 0 1-20 737 end
sm-152 1 0 1-20 737 end
eu-153 1 0 1-20 737 end
eu-154 1 0 1-20 737 end
eu-155 1 0 1-20 737 end
gd-155 1 0 1-20 737 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 620 end
h2o 3 den=0.7576 1 557 end
arbm-boromod 0.7576 1 1 0 0 5000 100 3 330.8e-6 557 end
  331 ppm boron (wt) in moderator
-----
end comp
-----

fuel-pin-cell geometry:
squarepitch 1.4732 0.9563 1 3 1.1176 2 0.9855 0 end
-----

assembly and cycle parameters:
npin/assm=176 fuelnght=789.64 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 1.3140 2 1.4160 3 1.6623 500 5.2039 3 5.2431
power=13.760 burn=306.0 down=71 end
power=15.505 burn=381.7 down=81.3 bfrac=1.419 temkcy=764 end
power=13.601 burn=466.0 down=2374 bfrac=1.523 temkcy=734 end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2
-----

1 ssssssssss aaaaaaaaaa ssssssssss 2222222222 hh hh
  ssssssssss aaaaaaaaaa ssssssssss 2222222222 hh hh
  ss aa aa ss ss 22 22 hh hh
  ss aa aa ss ss 22 22 hh hh
  ss aa aa ss ss 22 22 hh hh
  ssssssssss aaaaaaaaaa ssssssssss 22 hhhhhhhhhhhh
  ssssssssss aaaaaaaaaa ssssssssss 22 hhhhhhhhhhhh
  ss aa aa ss ss 22 hh hh
  ss aa aa ss ss 22 hh hh
  ss aa aa ss ss 22 hh hh
  ssssssssss aa aa ssssssssss 2222222222 hh hh
  ssssssssss aa aa ssssssssss 2222222222 hh hh

0
nn nn iiiiiiiiii cccccccccc hh hh oooooooooo 11
nnn nn iiiiiiiiii cccccccccc hh hh oooooooooo 11

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d101g26.sum

```

.....
*
*          SCALE4.3  Bulletin  Board
*          -----
*
*          Welcome to SCALE-4.3.
*
*
.....
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
   calvert cliffs 1 pwr, d101, rod mla098, 24.5 cm 26.62gwd/mtu June 97
   :
   :   mixtures of fuel-pin-unit-cell:
   :
   :   44group      latticecell
   :   uo2 1 den=10.018 1 841
   :       92234 0.024 92235 2.72 92236 0.013 92238 97.243 end
   :   kr-83 1 0 1-20 841 end
   :   kr-85 1 0 1-20 841 end
   :   y-89 1 0 1-20 841 end
   :   sr-90 1 0 1-20 841 end
   :   zr-93 1 0 1-20 841 end
   :   zr-94 1 0 1-20 841 end
   :   zr-95 1 0 1-20 841 end
   :   nb-94 1 0 1-20 841 end
   :   mo-95 1 0 1-20 841 end
   :   tc-99 1 0 1-20 841 end
   :   ru-101 1 0 1-20 841 end
   :   ru-106 1 0 1-20 841 end
   :   rh-103 1 0 1-20 841 end
   :   rh-105 1 0 1-20 841 end
   :   pd-105 1 0 1-20 841 end
   :   pd-108 1 0 1-20 841 end
   :   ag-109 1 0 1-20 841 end
   :   sb-124 1 0 1-20 841 end
   :   xe-131 1 0 1-20 841 end
   :   xe-132 1 0 1-20 841 end
   :   xe-135 1 0 1-20 841 end
   :   xe-136 1 0 1-20 841 end
   :   cs-134 1 0 1-20 841 end
   :   cs-135 1 0 1-20 841 end
   :   cs-137 1 0 1-20 841 end
   :   ba-136 1 0 1-20 841 end
   :   la-139 1 0 1-20 841 end
   :   pr-141 1 0 1-20 841 end
   :   pr-143 1 0 1-20 841 end
   :   ce-144 1 0 1-20 841 end
   :   nd-143 1 0 1-20 841 end
   :   nd-145 1 0 1-20 841 end
   :   nd-147 1 0 1-20 841 end
   :   pm-147 1 0 1-20 841 end
   :   pm-148 1 0 1-20 841 end
   :   sm-147 1 0 1-20 841 end
   :   sm-149 1 0 1-20 841 end
   :   sm-150 1 0 1-20 841 end
   :   sm-151 1 0 1-20 841 end
   :   sm-152 1 0 1-20 841 end
   :   eu-153 1 0 1-20 841 end
   :   eu-154 1 0 1-20 841 end
   :   eu-155 1 0 1-20 841 end
   :   gd-155 1 0 1-20 841 end
   :   arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
   :               40000 98.18 2 1.0 620 end
   :   h2o 3 den=0.7571 1 558 end
   :   arbm-bormod 0.7571 1 1 0 0 5000 100 3 330.8e-6 558 end
   :
   :   331 ppm boron (wt) in moderator
   :
   :   -----
   :   end comp
   :
   :
   :   fuel-pin-cell geometry:
   :
   :   squarepitch 1.4732 0.9563 1 3 1.1176 2 0.9855 0 end
   :
   :   -----
   :
   :   assembly and cycle parameters:
   :
   :   npin/assm=176 fuelnght=789.64 ncycles=3 nlib/cyc=5
   :   printlevel=5 lightel=9 inplevel=2 numztotal=5 end
   :   3 1.3140 2 1.4160 3 1.6623 500 5.2039 3 5.2431
   :   power=20.406 burn=306.0 down=71 end
   :   power=22.090 burn=381.7 down=81.3 bfrac=1.419 temkcy=867 end
   :   power=18.855 burn=466.0 down=2374 bfrac=1.523 temkcy=817 end
   :   o 119 cr 5.2 mn 0.29
   :   fe 11.0 co 0.066 ni 8.7
   :   zr 195 nb 0.63 sn 3.2
   :
   :   -----
1  sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
   sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
   ss ss aa aa ss ss 22 22 hh hh
   ss aa aa aa ss 22 hh hh
   ss aa aa aa ss 22 hh hh
   sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhh
   sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhh
   ss aa aa ss ss 22 hh hh
   ss aa aa ss ss 22 hh hh
   ss aa aa ss 22 hh hh
   sssssssssss aa aa sssssssssss 2222222222 hh hh
   sssssssssss aa aa sssssssssss 2222222222 hh hh
0
nn nn iiiiiiiiii cccccccccc hh hh oooooooooo 11
nnn nn iiiiiiiiii cccccccccc hh hh oooooooooo 11

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d101g33.sum

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.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  calvert cliffs 1 pwr, d101, rod mla098, 161.7 cm 33.17gwd/mtu June 97
  mixtures of fuel-pin-unit-cell:
    44group latticecell
    uo2 1 den=10.018 1 939
      92234 0.024 92235 2.72 92236 0.013 92238 97.243 end
    kr-83 1 0 1-20 939 end
    kr-85 1 0 1-20 939 end
    y-89 1 0 1-20 939 end
    sr-90 1 0 1-20 939 end
    zr-93 1 0 1-20 939 end
    zr-94 1 0 1-20 939 end
    zr-95 1 0 1-20 939 end
    nb-94 1 0 1-20 939 end
    mo-95 1 0 1-20 939 end
    tc-99 1 0 1-20 939 end
    ru-101 1 0 1-20 939 end
    ru-106 1 0 1-20 939 end
    rh-103 1 0 1-20 939 end
    rh-105 1 0 1-20 939 end
    pd-105 1 0 1-20 939 end
    pd-108 1 0 1-20 939 end
    ag-109 1 0 1-20 939 end
    sb-124 1 0 1-20 939 end
    xe-131 1 0 1-20 939 end
    xe-132 1 0 1-20 939 end
    xe-135 1 0 1-20 939 end
    xe-136 1 0 1-20 939 end
    cs-134 1 0 1-20 939 end
    cs-135 1 0 1-20 939 end
    cs-137 1 0 1-20 939 end
    ba-136 1 0 1-20 939 end
    la-139 1 0 1-20 939 end
    pr-141 1 0 1-20 939 end
    pr-143 1 0 1-20 939 end
    ce-144 1 0 1-20 939 end
    nd-143 1 0 1-20 939 end
    nd-145 1 0 1-20 939 end
    nd-147 1 0 1-20 939 end
    pm-147 1 0 1-20 939 end
    pm-148 1 0 1-20 939 end
    sm-147 1 0 1-20 939 end
    sm-149 1 0 1-20 939 end
    sm-150 1 0 1-20 939 end
    sm-151 1 0 1-20 939 end
    sm-152 1 0 1-20 939 end
    eu-153 1 0 1-20 939 end
    eu-154 1 0 1-20 939 end
    eu-155 1 0 1-20 939 end
    gd-155 1 0 1-20 939 end
    arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
      40000 98.18 2 1.0 620 end
    h2o 3 den=0.7341 1 570 end
    arbm-bormod 0.7341 1 1 0 0 5000 100 3 330.8e-6 570 end
  331 ppm boron (wt) in moderator
end comp
-----
fuel-pin-cell geometry:
squarepitch 1.4732 0.9563 1 3 1.1176 2 0.9855 0 end
-----
assembly and cycle parameters:
npin/assm=176 fuelnght=789.64 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 1.3140 2 1.4160 3 1.6623 500 5.2039 3 5.2431
power=26.656 burn=306.0 down=71 end
power=27.837 burn=381.7 down=81.3 bfrac=1.419 temkyc=957 end
power=22.443 burn=466.0 down=2374 bfrac=1.523 temkyc=873 end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2
-----
1 ssssssssss aaaaaaaaaa ssssssssss 2222222222 hh hh
  ssssssssssss aaaaaaaaaa ssssssssss 222222222222 hh hh
  ss ss aa aa ss ss 22 22 hh hh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  ssssssssss aaaaaaaaaa ssssssssss 22 hhhhhhhhhhhh
  ssssssssss aaaaaaaaaa ssssssssss 22 hhhhhhhhhhhh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  ssssssssss aa aa ssssssssss 222222222222 hh hh
  ssssssssss aa aa ssssssssss 222222222222 hh hh
0
nn nn iiiiiiiiii cccccccccc hh hh oooooooooo 11
nnn nn iiiiiiiiii cccccccccc hh hh oooooooooo 11

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bt03g37.sum

```

.....
      SCAL4.3 Bulletin Board
      -----
      Welcome to SCALE-4.3.
.....
1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  calvert cliffs 1 pwr, bt03, rod nbd107, 19.92 cm 37.27gwd June 97
.....
  mixtures of fuel-pin-unit-cell:
44group latticecell
uo2 1 den=10.054 1 814
  92234 0.022 92235 2.453 92236 0.011 92238 97.514 end
kr-83 1 0 1-20 814 end
kr-85 1 0 1-20 814 end
y-89 1 0 1-20 814 end
sr-90 1 0 1-20 814 end
zr-93 1 0 1-20 814 end
zr-94 1 0 1-20 814 end
zr-95 1 0 1-20 814 end
nb-94 1 0 1-20 814 end
mo-95 1 0 1-20 814 end
tc-99 1 0 1-20 814 end
ru-101 1 0 1-20 814 end
ru-106 1 0 1-20 814 end
zh-103 1 0 1-20 814 end
zh-105 1 0 1-20 814 end
pd-105 1 0 1-20 814 end
pd-108 1 0 1-20 814 end
ag-109 1 0 1-20 814 end
sb-124 1 0 1-20 814 end
xe-131 1 0 1-20 814 end
xe-132 1 0 1-20 814 end
xe-135 1 0 1-20 814 end
xe-136 1 0 1-20 814 end
cs-134 1 0 1-20 814 end
cs-135 1 0 1-20 814 end
cs-137 1 0 1-20 814 end
ba-136 1 0 1-20 814 end
la-139 1 0 1-20 814 end
pr-141 1 0 1-20 814 end
pr-143 1 0 1-20 814 end
ce-144 1 0 1-20 814 end
nd-143 1 0 1-20 814 end
nd-145 1 0 1-20 814 end
nd-147 1 0 1-20 814 end
pm-147 1 0 1-20 814 end
pm-148 1 0 1-20 814 end
sm-147 1 0 1-20 814 end
sm-149 1 0 1-20 814 end
sm-150 1 0 1-20 814 end
sm-151 1 0 1-20 814 end
sm-152 1 0 1-20 814 end
eu-153 1 0 1-20 814 end
eu-154 1 0 1-20 814 end
eu-155 1 0 1-20 814 end
gd-155 1 0 1-20 814 end
arbm-zirc4 6.56 5 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 620 end
h2o 3 den=0.7573 1 557 end
arbm-bormod 0.7573 1 1 0 0 5000 100 3 330.8e-6 557 end
n 4 0 5-5 557 end
arbm-zirc4 6.56 5 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 5 1.0 557 end
o 6 0 0.058 557 end
al 6 0 0.039 557 end
c 6 0 0.00107 557 end
b-10 6 0 0.000859 557 end
b-11 6 0 0.0034 557 end
.
.
  331 ppm boron (wt) in moderator
.....
end comp
.....
  fuel-pin-cell geometry:
squarepitch 1.4732 0.9639 1 3 1.1176 2 0.9754 0 end
.....
  assembly and cycle parameters:
npin/assm=160 fuelngth=851.90 ncycles=4 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numzttotal=6 end
6 0.4775 4 0.4928 5 0.5588 3 0.8312 500 1.7190 3 1.7319
power=18.705 burn=816.0 down=81 end
power=19.534 burn=306.0 down=71 temkyc=827 end
power=13.672 burn=381.7 down=81.3 bfrac=1.419 temkyc=736 end
power=13.707 burn=466.0 down=2447 bfrac=1.523 temkyc=736 end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2
.....
1 sssssssss aaaaaaaaa sssssssss 2222222222 hh hh
  sssssssss aaaaaaaaa sssssssss 2222222222 hh hh
ss ss aa aa ss ss 22 22 hh hh
ss aa aa ss 22 22 hh hh

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bt03g46.sum

```

.....
.
.          SCALE4.3  Bulletin  Board
.          -----
.
.          Welcome to SCALE-4.3.
.
.....
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
   calvert cliffs 1 pwr, bt03, rod nbd107, 161.21 cm 46.46gwd June 97
.
.  mixtures of fuel-pin-unit-cell:
.
44group          latticecell
uo2 1 den=10.054 1 887
   92234 0.022 92235 2.453 92236 0.011 92238 97.514  end
kr-83 1 0 1-20 887  end
kr-85 1 0 1-20 887  end
y-89 1 0 1-20 887  end
sr-90 1 0 1-20 887  end
zr-93 1 0 1-20 887  end
zr-94 1 0 1-20 887  end
zr-95 1 0 1-20 887  end
nb-94 1 0 1-20 887  end
mo-95 1 0 1-20 887  end
tc-99 1 0 1-20 887  end
ru-101 1 0 1-20 887  end
ru-106 1 0 1-20 887  end
rh-103 1 0 1-20 887  end
rh-105 1 0 1-20 887  end
pd-105 1 0 1-20 887  end
pd-108 1 0 1-20 887  end
ag-109 1 0 1-20 887  end
sb-124 1 0 1-20 887  end
xe-131 1 0 1-20 887  end
xe-132 1 0 1-20 887  end
xe-135 1 0 1-20 887  end
xe-136 1 0 1-20 887  end
cs-134 1 0 1-20 887  end
cs-135 1 0 1-20 887  end
cs-137 1 0 1-20 887  end
ba-136 1 0 1-20 887  end
la-139 1 0 1-20 887  end
pr-141 1 0 1-20 887  end
pr-143 1 0 1-20 887  end
ce-144 1 0 1-20 887  end
nd-143 1 0 1-20 887  end
nd-145 1 0 1-20 887  end
nd-147 1 0 1-20 887  end
pm-147 1 0 1-20 887  end
pm-148 1 0 1-20 887  end
sm-147 1 0 1-20 887  end
sm-149 1 0 1-20 887  end
sm-150 1 0 1-20 887  end
sm-151 1 0 1-20 887  end
sm-152 1 0 1-20 887  end
eu-153 1 0 1-20 887  end
eu-154 1 0 1-20 887  end
eu-155 1 0 1-20 887  end
gd-155 1 0 1-20 887  end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
           40000 98.18 2 1.0 620  end
h2o 3 den=0.7342 1 570 end
arbm-bormod 0.7342 1 1 0 0 5000 100 3 330.8e-6 570  end
.
.  n 4 0 5-5 570  end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
           40000 98.18 5 1.0 570  end
o 6 0 0.058 570  end
al 6 0 0.039 570  end
c 6 0 0.00107 570  end
b-10 6 0 0.000859 570  end
b-11 6 0 0.0034 570  end
.
.  331 ppm boron (wt) in moderator
.
end comp
.
.  fuel-pin-cell geometry:
.
squarepitch 1.4732 0.9639 1 3 1.1176 2 0.9754 0  end
.
.  assembly and cycle parameters:
.
npin/assm=160 fuelngth=851.90 ncycles=4 nlib/cyc=5
printlevel=5 lightel=9 impllevel=2 numztotal=6 end
6 0.4775 4 0.4928 5 0.5588 3 0.8312 500 1.7190 3 1.7319
power=23.324 burn=816.0 down=81  end
power=24.347 burn=306.0 down=71 temkcy=903  end
power=17.039 burn=381.7 down=81.3 bfrac=1.419 temkcy=788  end
power=17.092 burn=466.0 down=2447 bfrac=1.523 temkcy=789  end
o 119 cr 5.2 mn 0.29
fe 11.0 co 0.066 ni 8.7
zr 195 nb 0.63 sn 3.2
.
.....
1  sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
   sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
   ss aa aa ss 22 22 hh hh
   ss aa aa ss 22 22 hh hh

```