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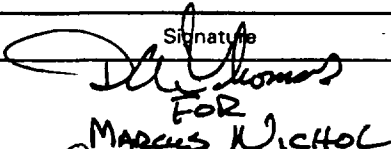
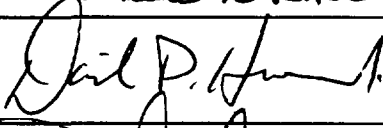
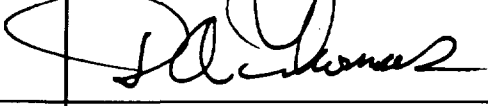
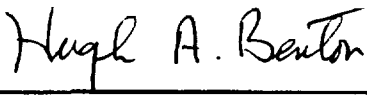
# Design Analysis Cover Sheet

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### **1. Purpose**

The purpose of this design analysis is to determine the accuracy of the SAS2H module of SCALE 4.3 in predicting isotopic concentrations of spent fuel assemblies. The objective is to develop a methodology for modeling assemblies similar to those evaluated within this analysis and to establish the consistency of SAS2H predictions. The results of this analysis may then be applied to future depletion calculations using SAS2H in which no measurements are available.

### **2. Quality Assurance**

The Quality Assurance (QA) program applies to this analysis. The work reported in this document is part of the Waste Package Design analysis that will eventually support the License Application Design phase. This activity, when appropriately confirmed, can impact the proper functioning of the Mined Geologic Disposal System (MGDS) waste package; the waste package has been identified as an MGDS Q-List item important to safety and waste isolation (pp. 4, 15, Reference 5.1). The waste package is on the Q-List by direct inclusion by the Department of Energy (DOE), without conducting a QAP-2-3 evaluation. The Waste Package Development Department (WPDD) responsible manager has evaluated this activity in accordance with QAP-2-0, *Conduct of Activities*. The *Perform Criticality, Thermal, Structural, and Shielding Analyses* (Reference 5.2) evaluation has determined the preparation and review of this design analysis is subject to *Quality Assurance Requirements and Description* (Reference 5.3) requirements. As specified in NLP-3-18, this activity is subject to QA controls.

The analysis described in this document supports development of the disposal criticality analysis methodology. No designs were analyzed in this document. This document will not directly support any construction, fabrication, or procurement activity and therefore is not required to be procedurally controlled as TBV (to be verified). The calculation design inputs or information used in this document come from data accepted by the Nuclear Regulatory Commission and by the scientific and engineering community as established fact. The specific references are listed in Section 5 and identified in Section 7. The information is therefore not treated as unqualified data.

### **3. Method**

The analytical model employed for this analysis was the SAS2H module of the SCALE sequence. Based upon fuel design, power history, and operating data for specific assemblies in the Obrigheim pressurized water reactor (PWR), a computational model was developed for use with the SAS2H module of SCALE. The SAS2H module is used to perform a fuel depletion analysis to predict the isotopic concentrations in localized areas of assembly pins (pellet samples) subsequent to irradiation and cooling time. The isotopic concentrations predicted by the SAS2H module are then compared with measured concentrations of the same localized areas (axial locations) of the assembly pins to determine the accuracy of the developed model. The measured isotopic concentrations used for comparisons in the analysis are obtained from a separate report (Reference 5.5).

#### 4. Design Inputs

The sources for the design parameters are References 5.4 through 5.9. Reference 5.4 provides information on the molar masses; the assembly design, power history and operating parameters are obtained from References 5.5 through 5.7; cladding composition from Reference 5.8; and a list of trace elements in the fuel is derived from Reference 5.9.

##### 4.1 Design Parameters

The molar masses of selected elements are obtained from Reference 5.4 and are provided below within three significant figures. Precision beyond three significant figures is not necessary since the calculated isotopic concentrations from SCALE are only to three significant figures. Also, the weight per mole of enriched uranium is approximated by the weight per mole of natural uranium since the weight percent of enrichment is small.

Mole of natural uranium = 238 g, (Reference 5.4)

General spent fuel characteristics for each test assembly are presented in Table 4-1 and include the initial  $^{235}\text{U}$  enrichment, final burnup and the cooling time (Table 2, Reference 5.5). The initial enrichment of all assemblies is 3.13 wt%  $^{235}\text{U}$  and the burnup ranges from 25.93 to 29.52 GWd/MTU. Reference 5.5 is unclear as to whether the measurements are corrected to the time of shutdown or discharge. However, since Table 32 in Reference 5.5 contains the measured data and states that concentrations are relative to the time of unloading, a cooling time consistent with the time of discharge is used. Unfortunately, the time between shutdown and discharge is unknown, therefore, a cooling time of 10 days is assumed. This is assumed since a longer decay period would not significantly effect the isotopic composition; however, a shorter decay period would effect isotopes that come in part from the decay of short lived parent isotopes (pp. 7 and 10, Reference 5.6). Most notable is the decay of  $^{239}\text{U}$  ( $T_{1/2} = 23.5$  m) and  $^{239}\text{Np}$  ( $T_{1/2} = 2.35$  d) to form  $^{239}\text{Pu}$ , which increases by roughly 1% during the first 10 days (pp. 7 and 10, Reference 5.6). Therefore, the predicted concentration of  $^{239}\text{Pu}$  relative to that which is measured, may be used as an indication as to whether the use of a 10 day cooling time is appropriate.

Assembly design parameters are presented in Table 4-2 (Table 13, Reference 5.5; Table 1, Reference 5.7). The assembly is a Siemens 14 x 14 with 16 guide tube positions that were empty throughout each of the three cycles of irradiation. A cross section of a Siemens 14 x 14 assembly is presented in Figure 4-1 (Section 2.1.7, Reference 5.8). The guide tube dimensions were unknown and therefore the dimensions for a guide tube from a Westinghouse 14 x 14 assembly were assumed (p. 13, Reference 5.5). Values for fuel pellet stack density, pellet diameter, and cladding inside and outside diameters are presented in Reference 5.5 while hot (i.e., in operating reactor.) However, the dimensions prior to irradiation are obtained from Reference 5.7 and used to maintain consistency in modeling from one reactor to the next. The initial enrichment of  $^{234}\text{U}$  and  $^{236}\text{U}$  are not known and

are approximated by: wt %  $^{234}\text{U} = 0.0089 \times ^{235}\text{U}$  %, and wt %  $^{236}\text{U} = 0.0046 \times ^{235}\text{U}$  wt % (p. 13, Reference 5.5).

Power histories for the core during the pertinent cycles of irradiation are presented in Table 4-3 (Table 2, Reference 5.7). The assemblies were irradiated for a total of 3 cycles during cycles 3, 4 and 6 and were not loaded during cycle 5. The zero load days from each of the three operating cycles are summed for each cycle and modeled as a total shutdown period subsequent to the cycle of irradiation. Consequently the sum of the full load days for a particular cycle is used as that cycle's burn time. It is expected that approximating the cycle length by summing the full load days will not significantly alter the isotopic concentrations because the relative number of zero load days to full load days is small.

The operating parameters in Table 4-4 include the cumulative burnups, specific powers and fuel temperatures for each assembly over the operating cycles (Table 15, Reference 5.5). Moderator temperature, density and boron concentration, as well as the fuel cladding temperature are also included in Table 4-4 (Table 13, Reference 5.7). The cumulative burnups and specific powers were based upon data reported by the reactor operating utility (p. 29, Reference 5.5). Fuel temperatures were derived from the fuel temperature versus rod power diagram, Figure 4-1, and the boron concentration was assumed to be 450 ppm (p. 5 and Figure 2, Reference 5.7).

The composition of the cladding, Zircaloy-4, is presented in Table 4-5, and has a density of  $6.56 \text{ g/cm}^3$  (Reference 5.9). A list of trace elements in the fuel used in updating cross sections during the depletion analysis is presented in Table 4-6 and is developed with consideration of elements used in (Table 1, Reference 5.10). A generic set of light element weights for PWRs that is typically used in depletion analyses is included in Table 4-7 (Table 17, Reference 5.5). Variations in light element masses per unit fuel in different PWRs are small when compared to this generic set (p. 2-2, Reference 5.9). This data is provided in units of kg/MTUO<sub>2</sub> or kg/MTU depending on the units required in the analysis.

Measured isotopic concentrations are presented in Table 4-8 and are given in g/MTU (Table 32, Reference 5.5). The measurements were performed at the Karlsruhe Reprocessing Plant in Germany by cutting each assembly lengthwise and dissolving each half separately. The radiochemical analyses were performed independently by laboratories of the European Institute for Transuranic Elements, the Institute for Radiochemistry, the Karlsruhe Reprocessing Plant and the International Atomic Energy Agency, and are averaged to obtain the values in Table 4-8. Included in Table 4-9 is a listing of the measurement uncertainty for each of the isotopes examined (Table 8, Reference 5.7).

Table 4-1. Spent Fuel Characteristic Parameters for Obrigheim PWR

Test Assembly	Enrichment, wt % <sup>235</sup> U	Burnup, GWd/MTU	Cooling Time, days
168	3.13	28.40	10
170	3.13	25.93	10
171	3.13	29.04	10
172	3.13	26.54	10
176, batch 90	3.13	29.52	10
176, batch 91	3.13	27.99	10

Reference 5.5

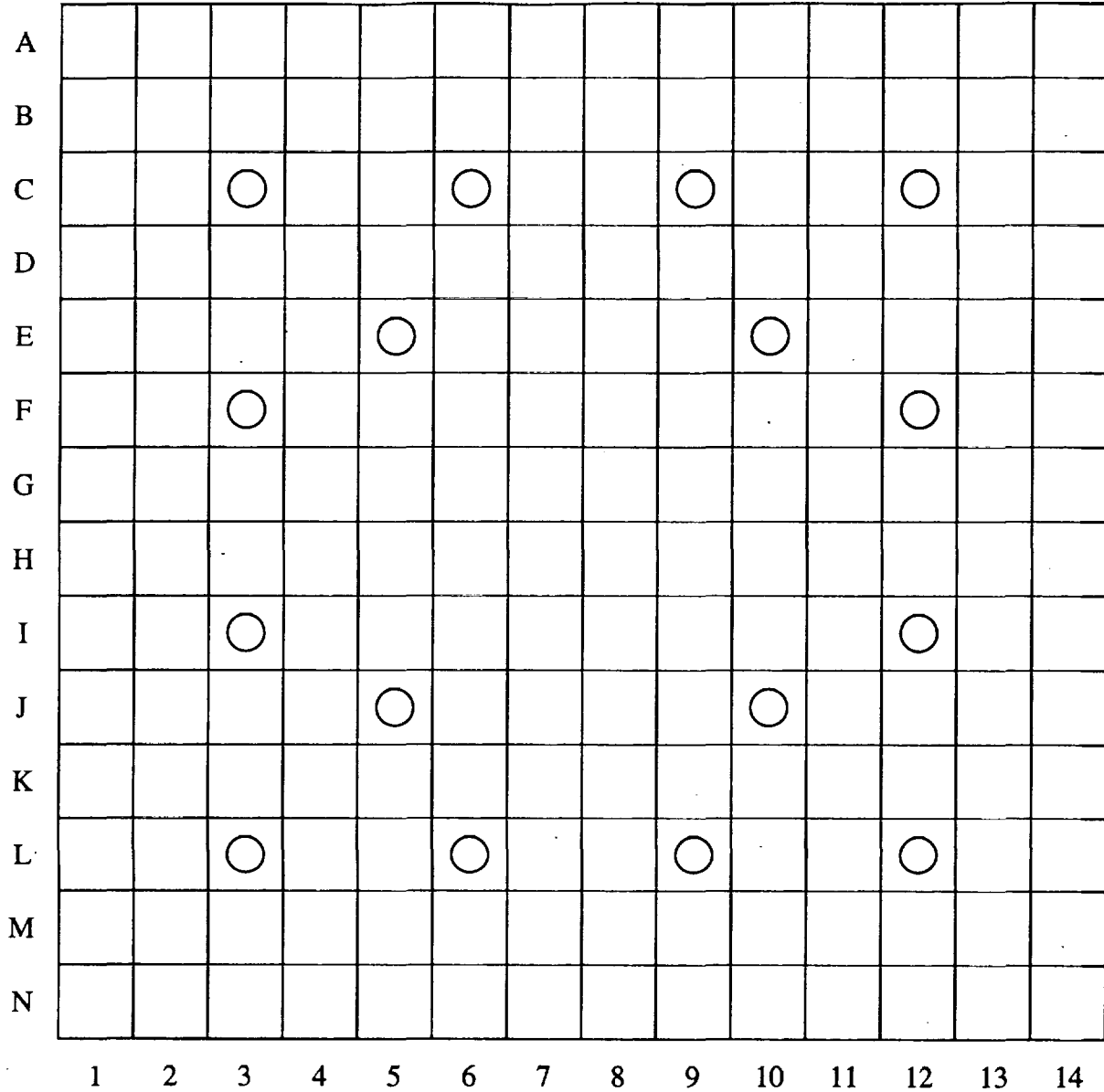
Table 4-2. Assembly Design Parameters for Obrigheim PWR

Parameter	Data
Assembly general data:	
Designer	Siemens
Lattice	14 x 14
Number of Fuel Rods	180
Number of Guide Tubes	16
Assembly Pitch, cm	20.12
Fuel Rod Data:	
Type of Fuel Pellet	UO <sub>2</sub>
Enrichment,	
wt % <sup>235</sup> U	3.13
wt % <sup>234</sup> U	0.028
wt % <sup>236</sup> U	0.014
Pellet Stack Density, g/cm <sup>3</sup>	10.05
Rod Pitch, cm	1.430
Rod Outside Diameter (OD), cm	1.074
Rod Inside Diameter (ID), cm	0.930
Pellet Diameter, cm	0.913
Active Fuel Length, cm	295.6
Clad Material	Zircaloy-4
Guide Tube Data:	
Inner Radius, cm	0.6413
Outer Radius, cm	0.6845
Tube Material	Zircaloy-4

*References 5.5 and 5.7*



Figure 4-1. Cross Section of Obrigheim Assembly



□ Fuel Rod Location

○ Guide Tube Location

Reference 5.8

Table 4-3. Power History of Obrigheim PWR

Cycle 3, days	Operating Condition	Cycle 4, days	Operating Condition	Cycle 5, days	Operating Condition	Cycle 6, days	Operating Condition
4.9	FL <sup>a</sup>	124.2	FL	377	ZL	127.8	FL
2.4	ZL <sup>b</sup>	8.5	ZL			2.4	ZL
79.1	FL	90.1	FL			54.8	FL
3.7	ZL	2.4	ZL			1.2	ZL
18.3	FL	9.7	FL			65.7	FL
1.2	ZL	1.2	ZL				
12.2	FL	13.4	FL				
37.7	ZL	4.9	ZL				
136.5	FL	1.2	FL				
6.8	ZL	2.4	ZL				
37.0	FL	70.6	FL				
29.2	ZL						
<b>Cycle Length, days</b>							
369		328		377		252	
<b>Uptime, days</b>							
288		309		0		248	
<b>Downtime, days</b>							
81		19		377		4	

<sup>a</sup>Full Load

<sup>b</sup>Zero Load

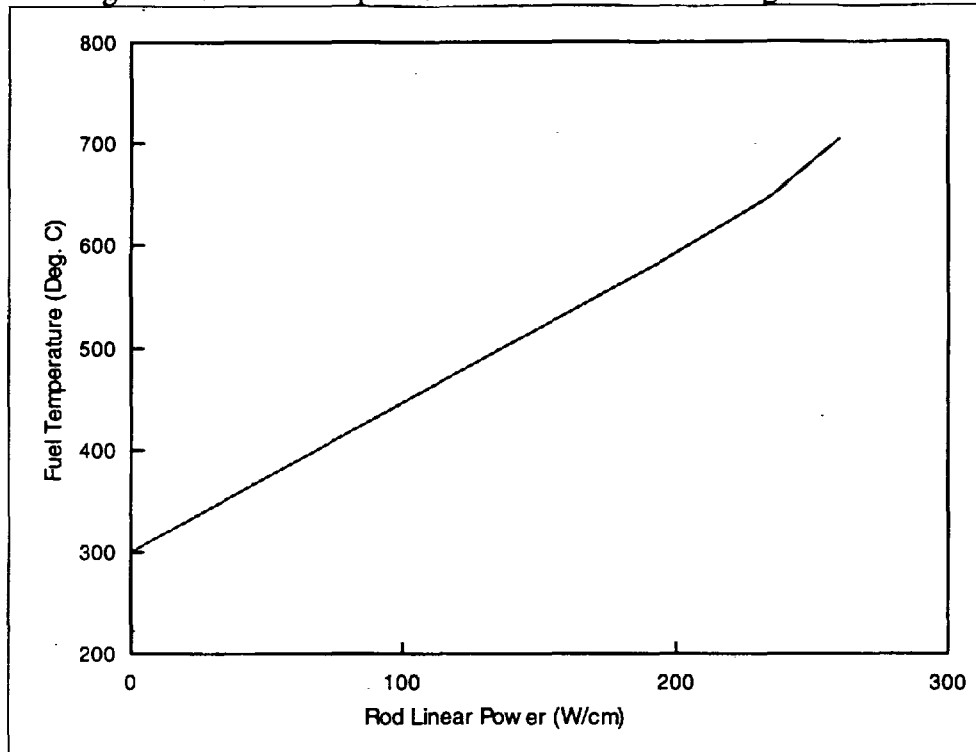
Reference 5.7

Table 4-4. Operating Data for Obrigheim PWR

	Test Assembly	Batch	Cycle 3	Cycle 4	Cycle 5	Cycle 6
Cumulative Burnup, GWd/MTU	168	86	8.16	19.90	-	28.40
	170	94	6.03	17.61	-	25.93
	171	89	8.39	20.42	-	29.04
	172	92	10.03	17.77	-	26.54
	176	90	9.25	20.62	-	29.52
	176	91	8.77	19.55	-	27.99
Specific Power, MW/MTU	168	86	28.336	38.005	-	34.249
	170	94	20.929	37.468	-	33.564
	171	89	29.124	38.952	-	34.748
	172	92	34.883	25.035	-	35.374
	176	90	32.121	36.801	-	35.875
	176	91	30.457	34.894	-	34.016
Effective Fuel Temperature, K	168	86	807	895	-	860
	170	94	743	896	-	851
	171	89	813	905	-	865
	172	92	865	778	-	870
	176	90	840	883	-	875
	176	91	825	865	-	855
Water Temperature, K	all	all	572			
Water Density, g/cm <sup>3</sup>	all	all	0.7283			
Soluble Boron, ppm	all	all	450			
Clad Temperature, K	all	all	605			

Reference 5.5

Figure 4-1. Fuel Temperature vs Rod Power for Obrigheim PWR



Reference 5.7

Table 4-5. Composition of Zircaloy-4

Material	Weight Percent
O	0.12
Cr	0.10
Fe	0.20
Sn	1.40
Zr	98.18
Density = 6.56 g/cm <sup>3</sup>	

Reference 5.9

Table 4-6. Nuclides Updated in SAS2H

<sup>83</sup> Kr	<sup>85</sup> Kr	<sup>89</sup> Y	<sup>90</sup> Sr	<sup>95</sup> Mo	<sup>93</sup> Zr
<sup>94</sup> Zr	<sup>94</sup> Nb	<sup>95</sup> Zr	<sup>99</sup> Tc	<sup>101</sup> Ru	<sup>103</sup> Rh
<sup>105</sup> Rh	<sup>106</sup> Ru	<sup>105</sup> Pd	<sup>108</sup> Pd	<sup>109</sup> Ag	<sup>124</sup> Sb
<sup>131</sup> Xe	<sup>132</sup> Xe	<sup>134</sup> Cs	<sup>135</sup> Xe	<sup>135</sup> Cs	<sup>136</sup> Xe
<sup>136</sup> Ba	<sup>137</sup> Cs	<sup>139</sup> La	<sup>141</sup> Pr	<sup>143</sup> Pr	<sup>143</sup> Nd
<sup>144</sup> Ce	<sup>145</sup> Nd	<sup>147</sup> Nd	<sup>147</sup> Pm	<sup>147</sup> Sm	<sup>148</sup> Pm
<sup>149</sup> Sm	<sup>150</sup> Sm	<sup>151</sup> Sm	<sup>152</sup> Sm	<sup>153</sup> Eu	<sup>154</sup> Eu
<sup>155</sup> Gd	<sup>155</sup> Eu				

Reference 5.10

Table 4-7. Light Element Mass per Unit of Fuel for Typical PWR

Element	kg/MTU
O	135.0
Cr	5.9
Mn	0.33
Fe	13.0
Co	0.075
Ni	9.9
Zr	221.0
Nb	0.71
Sn	3.6

Reference 5.5

Table 4-8. Average Measured Isotopic Concentrations (g/MTU)

Batch	86	94	89	92	90	91
Assembly	168	170	171	172	176	176
Burnup, GWd/MTU	28.40	25.93	29.04	26.54	29.52	27.99
<sup>235</sup> U	9680	10950	9580	10580	9180	9850
<sup>236</sup> U	3730	3590	3750	3620	3810	3700
<sup>238</sup> Pu	105.4	80.1	101.3	88.9	107.1	94.8
<sup>239</sup> Pu	5013	4805	4957	4713	4943	4925
<sup>240</sup> Pu	2020	1800	2000	1830	2040	1920
<sup>241</sup> Pu	1103	978	1107	978	1128	1058
<sup>242</sup> Pu	407	312	405	328	438	372

Reference 5.5

Table 4-9. Measurement Uncertainty

<sup>235</sup> U	± 2 %
<sup>236</sup> U	± 1 %
<sup>238</sup> Pu	± 15 %
<sup>239</sup> Pu	± 3 %
<sup>240</sup> Pu	± 3 %
<sup>241</sup> Pu	± 4 %
<sup>242</sup> Pu	± 4 %

Reference 5.7

#### 4.2 Criteria

The design of the waste package will depend on waste package configuration criticality analyses performed using an acceptable disposal criticality analysis methodology. Criteria that relate to the development and design of repository and engineered barrier components are derived from the applicable requirements and planning documents. The Engineered Barrier Design Requirements Document (EBDRD, Reference 5.13) provides requirements for engineered barrier segment design. The Repository Design Requirements Document (RDRD, Reference 5.14) provides requirements

for repository design. The Controlled Design Assumptions Document (Reference 5.15) provides guidance for requirements listed in the EBDRD and RDRD which have unqualified or unconfirmed data associated with the requirement.

This analysis supports the disposal criticality analysis methodology by providing input, in the form of fuel depletion results, to benchmark calculations which address the prediction of both spent fuel isotopic compositions and their associated reactivity. These benchmark calculations will contribute to the determination of bias values in the method of critical multiplication factor calculation that is implemented by the analytic tools to be used in the disposal criticality methodology. The requirements for utilizing the bias in the method of calculation of the critical multiplication factor for disposal configurations containing spent nuclear fuel are located in Section 3.2.2.5 of the RDRD and Section 3.2.2.6 of the EBDRD. This analysis does not satisfy these requirements, but the results from this analysis will be used as input to subsequent analyses which will satisfy these requirements.

#### **4.3 Assumptions**

4.3.1 Measured isotopic concentrations from Reference 5.5 are calculated and corrected to the time of discharge; however, the time between shutdown and discharge is not specified. Therefore, a cooling time of 10 days is assumed. The basis for this assumption is that a longer decay period does not significantly effect isotopic concentrations, but a shorter decay period effects concentrations of those isotopes with short lived parents. This assumption is used in Section 7.5.

4.3.2 The cycle average boron concentrations are assumed to be 450 ppm. The basis for this assumption is that the value is an average of typical cycle average boron concentrations, and was obtained from Reference 5.7. This assumption is used in Section 7.2.

#### **4.4 Codes and Standards**

There are no applicable codes or standards for this design analysis.

## 5. References

- 5.1 *Yucca Mountain Site Characterization Project Q-List*, YMP/90-55Q REV 4, Yucca Mountain Site Characterization Project.
- 5.2 *QAP-2-0 Activity Evaluations: ID #WP-20, Perform Criticality, Thermal, Structural, and Shielding Analyses*, Civilian Radioactive Waste Management System (CRWMS) Management and Operating Contractor (M&O), August 3, 1997.
- 5.3 *Quality Assurance Requirements and Description*, DOE/RW-0333P REV 7, U.S. Department of Energy (DOE) Office of Civilian Radioactive Waste Management (OCRWM).
- 5.4 *Nuclides and Isotopes*, General Electric Company, 14ed., 1989.
- 5.5 *Validation of the Scale System for PWR Spent Fuel Isotopic Composition Analyses*. ORNL/TM-12667, Oak Ridge National Laboratory, March 1995.
- 5.6 *An Extension of the Validation of SCALE (SAS2H) Isotopic Predictions for PWR Spent Fuel*, ORNL/TM-13317, Oak Ridge National Laboratory, September 1996.
- 5.7 U. Hesse, *Verification of the OREST (HAMMER-ORIGEN) Depletion Program System Using Post-Irradiation Analyses of Fuel Assemblies 168, 170, 171, and 176 from the Obrigheim Reactor*, (ORNL-TR-88/20), GRS-A-962, Gesellschaft für Reaktorsicherheit (GRS) mbH, 1984.
- 5.8 *Isotopic and Criticality Validation for PWR-Actinide Only Burnup Credit*, DOE/RW-0497, DOE OCRWM.
- 5.9 *Material Compositions and Number Densities for Neutronics Calculations*, Document Identifier (DI) Number: BBA000000-01717-0200-00002 REV 00, CRWMS M&O.
- 5.10 *SCALE-4 Analysis of Pressurized Water Reactor Critical Configurations: Volume 2- Sequoyah Unit 2 Cycle 3*, ORNL/TM-12294/V2, March 1995.
- 5.11 *SCALE 4.3, A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation for Workstations and Personal Computers*, NUREG/CR-0200 REV 5, ORNL/NUREG/CSD-2/R5, Volumes 1-3, Oak Ridge National Laboratory.
- 5.12 *Software Qualification Report for the SCALE Modular Code System*, DI Number: 30011-2002 REV 01, CRWMS M&O.



- 5.13 *Engineered Barrier Design Requirements Document*, YMP/CM-0024, REV 00, ICN 01, DOE OCRWM.
- 5.14 *Repository Design Requirements Document*, YMP/CM-0023, REV 00, ICN 01, DOE OCRWM.
- 5.15 *Controlled Design Assumptions Document*, DI#: B00000000-01717-4600-00032 REV 04, ICN 01, CRWMS M&O.

### **6. Use of Computer Programs**

- A.** Reference 5.11 describes the SAS2H module of SCALE 4.3 that is used with the 44GROUPNDF5 cross section library to calculate the isotopic concentrations for the specified burnup and cooling time. The computer code's spatially independent point depletion model is appropriate for comparison with assembly average measurements, and is used within the range of validation, as described in Reference 5.12, in accordance with the QAP-SI series procedures. SCALE is obtained from the Software Configuration Management in accordance with appropriate procedures. SCALE's CSCI number is 30011 V4.3 and is installed on the WPDD HP 9000, 700 Workstation with CRWMS M&O tag number 110433.
  
- B.** *Lotus 1-2-3* Release 5 for Windows 95 is an Acquired Software spreadsheet program as defined in QAP-SI-0. User defined formulas and/or algorithms, inputs and results, are documented in the appropriate sections.

## 7. Design Analysis

The SAS2H module of SCALE 4.3 is used to perform one-dimensional (1-D) neutron transport and point depletion analyses on the Obrigheim assemblies using the preferred 44GROUPNDF5 cross-section library. To properly model the neutron flux spectrum and the nuclide composition changes, it is necessary to define the materials, geometry, and operating parameters of the fuel assembly. This is accomplished with the use of data blocks in which similar parameters are grouped together.

### 7.1 SCALE Input Data Blocks 1, 2, and 3

Data blocks 1 through 3 define the SCALE module to be used, the title of the input file, the cross sectional library to be used, and the lattice type to be modeled. The module used is SAS2H and the cross sectional library is 44GROUPNDF5, abbreviated as 44GROUP. The 44GROUP cross section library is recommended by Oak Ridge National Laboratory. Since SAS2H is only to be used for isotopic depletion/generation, the option 'parm=skipshipdata' is used so that a shipping cask shielding analysis is not performed. The title is arbitrary and should contain information that is assembly specific, while the lattice type is "latticecell" to reflect the array characteristic of the assembly.

### 7.2 SCALE Input Data Block 4

Data block 4 defines the material compositions present in the assembly. A unique mixture number is assigned to each composition, and follows the form of mixture 1 for fuel, mixture 2 for cladding and mixture 3 for moderator.

The fuel mixture is specified as  $\text{UO}_2$  with a density and isotopic weight percentages from Table 4-2. Fuel temperatures for the assemblies during each cycle are presented in Table 4-4 and the temperature during cycle 3 is input for the fuel temperature specification in data block 4. The other cycle fuel temperatures are input in data block 9. Isotopes which are selected as needing their cross sections updated during the depletion analysis are included in the fuel mixture. A standard list of trace fuel elements is given in Table 4-6 and defined in the fuel mixture to have a concentration of  $10^{-20}$  atoms/barn-cm.

The cladding material of Zircaloy-4 is not contained within the Standard Composition Library in SCALE 4.3 and must be defined as an arbitrary material. The cladding is defined with a density and isotopic weight percentages from Table 4-5 and temperature given in Table 4-4.

The moderator temperature, density and boron concentration are given in Table 4-4 and is composed of  $\text{H}_2\text{O}$  and boron. The boron is defined as an arbitrary material with the moderator density and temperature, a volume fraction equal to the cycle average boron concentration, and a standard boron composition from the Standard Composition Library designated as 5000.

### 7.3 SCALE Input Data Blocks 5 Through 7

The unit fuel rod cell geometry is defined in data block 5. The 'squarepitch' designation for the type of lattice is appropriate since the fuel assembly consists of a square array of fuel rods. Fuel rod, cladding and pitch dimensions are given in Table 4-2 with the mixture number for each composition defined in Section 7.2. The gap mixture is defined as 0.

Data block 6 allows the user to specify such parameters as the spatial mesh, angular quadrature and convergence criteria. It is determined that the default values are sufficient and such options are not used in this design model.

In data block 7 the user defines general assembly data and determines the level of detail in which the assembly is to be modeled. The number of fuel rods per assembly is given in Table 4-2 and the length is calculated so that an assemble contains 1 MTU, using the following equation:

$$Length = \frac{1}{\frac{\pi}{4}(POD)^2(PDen)(NFR)} * \frac{270gUO_2}{238gU} * \frac{10^6gU}{1MTU} \quad \text{Equation 7-1}$$

Where:

- Length = Length Required for an Assembly to Contain 1 MTU (cm)
- POD = Fuel Pellet Diameter (cm)
- PDen = Fuel Pellet Density (g UO<sub>2</sub>/cm<sup>3</sup>)
- NFR = Number of Fuel Rods

Since measured isotopic concentrations are presented in grams of isotope per Metric Ton Uranium (MTU) and SCALE presents concentrations in grams of isotope per assembly, it is convenient to alter the length so that the assembly contains 1 MTU. This is possible since the 1-D transport calculation is axially independent. Consequently, the length of the assembly does not impact the neutron flux spectrum nor the nuclide cross sections. The resulting length for Obrigheim assemblies is 957.89 cm.

Each assembly was irradiated for three cycles. It is determined that approximately 80 days per cross section library is sufficient to accurately model the change in nuclide cross sections with increasing burnup, without over-burdening the SAS2H code. Therefore, the number of libraries per cycle are specified as five. To obtain the concentrations of all interested nuclides, a print level of 5 is chosen, while an input level of 2 is defined so that a Path B model may be utilized. The number of light elements are nine and are determined from Table 4-5, while the number of zones are five which is determined by the Path B model described in Section 7.4.

## 7.4 SCALE Input Data Block 8

The Path B model for Obrigheim is a centralized guide tube unit cell surrounded by an homogenized fuel and moderator mixture that conserves the fuel to moderator volume ratio, and is further surrounded by moderator between assemblies. The equation below is used to determine the number of fuel unit cells that surround the central guide tube. All of the following equations used to calculate the Path B model dimensions are derived. The results of the fuel-unit-cell calculations are presented in Table 7-1, and the resulting Path B model dimensions are presented in Table 7-2.

$$x = \frac{\left(\frac{F}{M}\right)(CUCMV)}{(FV) - \left(\frac{F}{M}\right)(MV)} \quad \text{Equation 7-2}$$

$$\frac{F}{M} = \frac{(NFR)\left(\frac{\pi}{4}\right)(POD)^2}{(NFR)\left[RP^2 - \left(\frac{\pi}{4}\right)(COD)^2\right] + (NGT)\left[RP^2 - \left(\frac{\pi}{4}\right)(GTOD)^2 + \left(\frac{\pi}{4}\right)(GTID)^2\right]} \quad \text{Equation 7-3}$$

$$CUCMV = RP^2 - \left(\frac{\pi}{4}\right)(GTOD)^2 + \left(\frac{\pi}{4}\right)(GTID)^2 \quad \text{Equation 7-4}$$

$$FV = \left(\frac{\pi}{4}\right)(POD)^2 \quad \text{Equation 7-5}$$

$$MV = RP^2 - \left(\frac{\pi}{4}\right)(COD)^2 \quad \text{Equation 7-6}$$

Where:

- x = Number of Unit Fuel Cells per Central Guide Tube
- F/M = Fuel to Moderator Volume Ratio
- NFR = Number of Fuel Rods
- POD = Fuel Pellet Outer Diameter
- RP = Rod Pitch
- COD = Cladding Outer Diameter
- NGT = Number of Guide Tubes
- GTOD = Guide Tube Outer Diameter
- GTID = Guide Tube Inner Diameter
- CUCMV = Central Unit Cell Moderator Volume
- FV = Fuel Volume of One Fuel Unit Cell
- MV = Moderator Volume of One Fuel Unit Cell

Once the number of fuel cells per central guide tube is determined the geometry of the Path B model is calculated. Since the guide tube cell is centralized, the dimensions of the first two zones are the same as the guide tube inner and outer radii, these are presented in Table 7-2. The mixtures are moderator for zone 1 and zircaloy for zone 2.

The radius for the moderator surrounding the guide tube, but still within the guide tube cell, conserves volume and is calculated with the following equation:

$$R_3 = \sqrt{\left(\frac{1}{\pi}\right)RP^2} \quad \text{Equation 7-7}$$

Where:

$R_3$  = Radius of Moderator Surrounding Guide Tube

The area of an annular region is calculated by the difference between the outer circular area and the inner circular area. Equation 7-8 is the basis for the Equations 7-9 and 7-10 which determine the radii of the homogenized fuel zone and the outer moderator zone, respectively.

$$ARA = \pi(ORAR^2 - IRAR^2) \quad \text{Equation 7-8}$$

Where:

ARA = Annular Region Area

ORAR = Outer Radius of Annular Region

IRAR = Inner Radius of Annular Region

The area of the homogenized fuel zone surrounding the guide tube unit cell is equal to the number of fuel unit cells surrounding the guide tube multiplied by the area of a fuel unit cell. Consequently, the radius of the homogenized fuel zone is computed with the following equation:

$$R_4 = \sqrt{\left(\frac{x}{\pi}\right)RP^2 + R_3^2} \quad \text{Equation 7-9}$$

Where:

$R_4$  = Radius of Homogenized Fuel and Moderator Zone

The mixture number of the homogenized fuel and moderator mixture must be specified as 500. The code then determines the composition of the region using cell averages or homogenized densities of the fuel-pin-cell.

The moderator in the channel between assemblies is determined by calculating the total moderator volume and multiplying by the fraction of unit cells in the larger unit cell of the Path B model. The total moderator volume between assemblies is determined by the assembly pitch and the fuel cell

pitch multiplied by the number of unit cells. The radius of the moderator between assemblies is calculated from the following equation:

$$R_5 = \sqrt{\frac{(x+1)}{\pi * N_{Cell}} [AP^2 - (N_{Cell})(RP^2)] + R_4^2} \tag{Equation 7-10}$$

Where:

$R_5$  = Radius of Moderator Surrounding Assembly Zone

$N_{cell}$  = Number of Cells in Assembly

AP = Assembly Pitch

Table 7-1. Calculation of Fuel Unit Cell per Guide Tube Unit Cell

F/M	CUCMV, cm <sup>2</sup>	FV, cm <sup>2</sup>	MV, cm <sup>2</sup>	x
0.5018	1.8650	0.6547	1.1390	11.2500

Table 7-2. Path B Model Dimensions

	$R_1$	$R_2$	$R_3$	$R_4$	$R_5$
Radius, cm	0.6413	0.6845	0.8068	2.8238	2.8379
Composition	Moderator	Cladding	Moderator	Fuel/Moderator	Moderator

### 7.5 SCALE Input Data Blocks 9 Through 16

Data block 9 is used to describe the power history of the reactor. The specific power, fuel irradiation period, length of downtime, fraction of boron and moderator density, and the temperature during the cycle may all be defined. The specific power is in units of MW/MTU while the irradiation period and length of downtime are both defined in days. Table 4-4 contains values for the specific powers and the resulting uptime and downtime for each cycle are presented in Table 7-3. The power used for the intervals is the same and equal to the power for cycle 1 from Table 4-4. The boron and moderator density fractions are not used in modeling the Obrigheim assemblies because data provided are not in sufficient detail to determine cycle specific values. The individual cycle temperatures are provided in Table 4-4, and are specified with the command 'temkyc='.

Table 7-3. Cycle Irradiation Lengths and Downtime Between Cycles

	Cycle 3	Cycle 4	Cycle 5
Uptime, days	288	309	248
Downtime, days	81	396	10

Light elements and their effective weight, in kg per assembly, are entered in data block 10. Table 4-7 provides a generic set of light elements and their weights, in kg per MTU. Since the fuel length is altered so that there is 1 MTU per assembly the use of light elements with weights of kg per MTU is appropriate.

Data blocks 11 through 15 describe parameters used in the radial shielding analysis of a shipping cask and are not necessary in performing the depletion analyses. Data block 16 denotes the end of the SCALE input.

### **7.6 Comparison of Calculated and Measured Concentrations**

Comparisons of corresponding calculated and measured concentrations are performed on a percent difference basis. The difference between the measured and the calculated value is divided by the measured value to determine the accuracy of the SAS2H calculation. A positive percent difference represents an over-prediction by the code, while a negative percent difference represents an under-prediction by the code. The measured concentrations are given in Table 4-8, calculated concentrations in Table 7-4 and the percent differences are presented in Table 7-5.

In an attempt to determine the impact of the assumption of a cycle average boron concentration of 450 ppm for each cycle, a sensitivity analysis is performed. Two assemblies representing low and high burnups, 170 Batch 94 and 176 Batch 90, are used to observe the changes in isotopic concentrations with both a 100 ppm increase in boron concentration. The results are reported in Tables 7-5 and 7-6.

### **7.7 Results**

SAS2H predicted isotopic concentrations are presented in Table 7-3. The calculated concentrations are obtained through the methodology described in Sections 7.1 through 7.5, with the input parameters defined in Section 4.1. Calculated concentrations are then compared with measured concentrations as described in Section 7.6 to determine the accuracy of the SAS2H module. Results of the comparison, in the form of measured percent differences, are presented in Table 7-4. Also the results of the sensitivity analysis are reported in Tables 7-5 and 7-6.



Table 7-3. Calculated Isotopic Concentrations (g/MTU)

Batch	86	94	89	92	90	91
Assembly	168	170	171	172	176	176
<sup>235</sup> U	9.98E3	1.11E4	9.70E3	1.08E4	9.48E3	1.01E4
<sup>236</sup> U	3.76E3	3.60E3	3.80E3	3.64E3	3.83E3	3.74E3
<sup>238</sup> Pu	1.08E2	8.72E1	1.14E2	9.22E1	1.19E2	1.05E2
<sup>239</sup> Pu	4.21E3	4.17E3	4.21E3	4.24E3	4.21E3	4.23E3
<sup>240</sup> Pu	2.17E3	1.99E3	2.21E3	2.06E3	2.25E3	2.14E3
<sup>241</sup> Pu	1.10E3	1.01E3	1.13E3	1.03E3	1.15E3	1.08E3
<sup>242</sup> Pu	4.24E2	3.46E2	4.48E2	3.47E2	4.61E2	4.05E2

Table 7-4. Percent Difference Between Measured and Calculated  $[(C/M-1)*100]$

Batch	86	94	89	92	90	91
Assembly	168	170	171	172	176	176
<sup>235</sup> U	3.10	1.37	1.25	2.08	3.27	2.54
<sup>236</sup> U	0.80	0.28	1.33	0.55	0.52	1.08
<sup>238</sup> Pu	2.47	8.86	12.54	3.71	11.11	10.76
<sup>239</sup> Pu	-16.02	-13.22	-15.07	-10.04	-14.83	-14.11
<sup>240</sup> Pu	7.43	10.56	10.50	12.57	10.29	11.46
<sup>241</sup> Pu	-0.27	3.27	2.08	5.32	1.95	2.08
<sup>242</sup> Pu	4.18	10.90	10.62	5.79	5.25	8.87

Table 7-5. Sensitivity Analysis for Assembly 170 Batch 94

	Calculated Concentration, g/MTU		% Change in Calculated Concentrations
	Modeled Conditions	Boron Concentration Increase of 100 ppm	
<sup>235</sup> U	1.11E4	1.12E4	0.90
<sup>236</sup> U	3.60E3	3.60E3	0.00
<sup>238</sup> Pu	8.72E1	8.80E1	0.92
<sup>239</sup> Pu	4.17E3	4.21E3	0.96
<sup>240</sup> Pu	1.99E3	2.00E3	0.50
<sup>241</sup> Pu	1.01E3	1.01E3	0.00
<sup>242</sup> Pu	3.46E2	3.47E2	0.29

Table 7-6. Sensitivity Analysis for Assembly 176 Batch 90

	Calculated Concentration, g/MTU		% Change in Calculated Concentrations
	Modeled Conditions	Boron Concentration Increase of 100 ppm	
<sup>235</sup> U	9.48E3	9.54E3	0.63
<sup>236</sup> U	3.83E3	3.83E3	0.00
<sup>238</sup> Pu	1.19E2	1.20E2	0.84
<sup>239</sup> Pu	4.21E3	4.26E3	1.19
<sup>240</sup> Pu	2.25E3	2.25E3	0.00
<sup>241</sup> Pu	1.15E3	1.16E3	0.87
<sup>242</sup> Pu	4.61E2	4.61E2	0.00

## 8. Conclusions

The accuracy in which the SAS2H module is able to predict isotopic concentrations is indicated by the percent differences presented in Table 7-4. Inspection of such results reveals that the code consistently under-predicts the concentration of  $^{239}\text{Pu}$ , while it consistently over-predicts the isotopes of  $^{236}\text{U}$ ,  $^{238}\text{Pu}$ ,  $^{240}\text{Pu}$ , and  $^{242}\text{Pu}$ . Percent differences from this analysis are compared with results from Reference 5.5, in which similar calculations were performed with a previous version of SCALE and the 27burnplib cross section library. The concentrations calculated in Reference 5.5 for the most part agree with the concentrations calculated in this analysis; however, significant differences are seen for the plutonium isotopes. Since there are few differences between the model in Reference 5.5 and the model contained within, it is believed that the discrepancy between calculated concentrations for plutonium isotopes is caused by a change in the cross section library.

Uncertainty in the measured concentration of each isotope helps to explain the deviation of the calculated concentrations from the measured concentrations. For example, the calculated concentration of  $^{235}\text{U}$ ,  $^{236}\text{U}$ ,  $^{238}\text{Pu}$ , and  $^{241}\text{Pu}$  are either within or very close to the measurement uncertainties of  $\pm 2\%$ ,  $\pm 1\%$ ,  $\pm 15\%$  and  $\pm 3\%$ , respectively. However, such is not the case for the isotopes of  $^{238}\text{Pu}$ ,  $^{240}\text{Pu}$  and  $^{242}\text{Pu}$ , which deviate by more than the respective measurement uncertainties.

Results from the sensitivity analysis of the isotopic concentrations with boron concentration reveal that calculated isotopic concentrations increase by around 1% or less with a 100 ppm increase in boron concentration. Although, a slightly lower average boron concentration would improve calculated concentrations for most isotopes, it would also create a larger deviation for  $^{239}\text{Pu}$  which already has some of the largest deviation. However, since the average boron concentration is not expected to deviate more than 250 ppm from the assumed value, it is expected that the assumption of an average boron concentration of 450 ppm does not significantly effect the calculated isotopic concentrations.

It is believed that the 10 day cooling time assumed does not adversely effect any isotopic concentrations since the concentration of  $^{239}\text{Pu}$  is under-predicted and any longer cooling time would not significantly increase the concentration. However, if the concentration of  $^{239}\text{Pu}$  were over-predicted then a shorter cooling time would seem to be more appropriate.

In general the SAS2H module of SCALE does well in predicting isotopic concentrations for Obrigheim assemblies, using the methodology presented. While over-prediction or under-prediction is significant for a few isotopes, the majority of calculated concentrations are very close to the measured concentrations. Although the assumptions for the average boron concentration does effect the resulting isotopic concentrations, the effect is not significant enough to account for all variation between the measured and calculated concentrations. More detailed operating data would be expected to improve the accuracy of the calculated concentrations in relation to the corresponding measurements. It is recommended that future analyses use more detailed data if possible.

### **9. Attachments**

Attachment I includes eight pages and contains the input files used in the modeling of the Obrigheim assemblies. A description of the parameters contained within the input files is found in Sections 7.1 through 7.5.

Included in Attachment II is an extraction from each of the output files, containing the following information:

- echo of the SAS2H input deck,
- time/date stamp for when the SAS2H depletion calculation was performed,
- the output extraction of information pertinent to the Radiochemical Assay evaluations from the final ORIGEN calculation of the SAS2H depletion calculation.

## ob168g28.input

```
=sas2h parm=skipshipdata
obrighiem (kwo) pwr, assm 168, batch 86, 28.40 gwd/mtu 3-cyc June 97
.....used 180 fuel rode, 16 guide tubes.....
```

```
-----
mixtures of fuel-pin-unit-cell:
```

```
44group latticecell
uo2 1 den=10.05 1 807
92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 807 end
kr-85 1 0 1-20 807 end
y-89 1 0 1-20 807 end
sr-90 1 0 1-20 807 end
zr-93 1 0 1-20 807 end
zr-94 1 0 1-20 807 end
zr-95 1 0 1-20 807 end
nb-94 1 0 1-20 807 end
mo-95 1 0 1-20 807 end
tc-99 1 0 1-20 807 end
ru-101 1 0 1-20 807 end
ru-106 1 0 1-20 807 end
rh-103 1 0 1-20 807 end
rh-105 1 0 1-20 807 end
pd-105 1 0 1-20 807 end
pd-108 1 0 1-20 807 end
ag-109 1 0 1-20 807 end
sb-124 1 0 1-20 807 end
xe-131 1 0 1-20 807 end
xe-132 1 0 1-20 807 end
xe-135 1 0 1-20 807 end
xe-136 1 0 1-20 807 end
cs-134 1 0 1-20 807 end
cs-135 1 0 1-20 807 end
cs-137 1 0 1-20 807 end
ba-136 1 0 1-20 807 end
la-139 1 0 1-20 807 end
pr-141 1 0 1-20 807 end
pr-143 1 0 1-20 807 end
ce-144 1 0 1-20 807 end
nd-143 1 0 1-20 807 end
nd-145 1 0 1-20 807 end
nd-147 1 0 1-20 807 end
pm-147 1 0 1-20 807 end
pm-148 1 0 1-20 807 end
sm-147 1 0 1-20 807 end
sm-149 1 0 1-20 807 end
sm-150 1 0 1-20 807 end
sm-151 1 0 1-20 807 end
sm-152 1 0 1-20 807 end
eu-153 1 0 1-20 807 end
eu-154 1 0 1-20 807 end
eu-155 1 0 1-20 807 end
gd-155 1 0 1-20 807 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 450.0e-6 572 end
```

```
450 ppm boron (wt) in moderator
```

```
-----
end comp
```

```
-----
fuel-pin-cell geometry:
```

```
squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end
```

```
assembly and cycle parameters:
```

```
npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
```

```
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
```

```
power=28.336 burn=288 down=81 end
power=38.005 burn=309 down=396 temkyc=895 end
```

```
power=34.249 burn=248 down=10 temkyc=860 end
```

```
o 135 cr 5.9 mn 0.33
```

```
fe 13 co 0.075 ni 9.9
```

```
zr 221 nb 0.71 sn 3.6
```

```
-----
end
```

## ob170g25.input

```
=sas2h parm=skipshipdata
obrighiem (kwo) pwr, assm 170, batch 94, 25.93 gwd/mtu 3-cyc June97
.....used 180 fuel rode, 16 guide tubes.....
```

```
-----
mixtures of fuel-pin-unit-cell:
```

```
44group latticecell
uo2 1 den=10.05 1 743
  92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 743 end
kr-85 1 0 1-20 743 end
y-89 1 0 1-20 743 end
sr-90 1 0 1-20 743 end
zr-93 1 0 1-20 743 end
zr-94 1 0 1-20 743 end
zr-95 1 0 1-20 743 end
nb-94 1 0 1-20 743 end
mo-95 1 0 1-20 743 end
tc-99 1 0 1-20 743 end
ru-101 1 0 1-20 743 end
ru-106 1 0 1-20 743 end
rh-103 1 0 1-20 743 end
rh-105 1 0 1-20 743 end
pd-105 1 0 1-20 743 end
pd-108 1 0 1-20 743 end
ag-109 1 0 1-20 743 end
sb-124 1 0 1-20 743 end
xe-131 1 0 1-20 743 end
xe-132 1 0 1-20 743 end
xe-135 1 0 1-20 743 end
xe-136 1 0 1-20 743 end
cs-134 1 0 1-20 743 end
cs-135 1 0 1-20 743 end
cs-137 1 0 1-20 743 end
ba-136 1 0 1-20 743 end
la-139 1 0 1-20 743 end
pr-141 1 0 1-20 743 end
pr-143 1 0 1-20 743 end
ce-144 1 0 1-20 743 end
nd-143 1 0 1-20 743 end
nd-145 1 0 1-20 743 end
nd-147 1 0 1-20 743 end
pm-147 1 0 1-20 743 end
pm-148 1 0 1-20 743 end
sm-147 1 0 1-20 743 end
sm-149 1 0 1-20 743 end
sm-150 1 0 1-20 743 end
sm-151 1 0 1-20 743 end
sm-152 1 0 1-20 743 end
eu-153 1 0 1-20 743 end
eu-154 1 0 1-20 743 end
eu-155 1 0 1-20 743 end
gd-155 1 0 1-20 743 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 450.0e-6 572 end
```

```
450 ppm boron (wt) in moderator
```

```
-----
end comp
```

```
-----
fuel-pin-cell geometry:
```

```
squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end
```

```
assembly and cycle parameters:
```

```
npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
```

```
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
```

```
power=20.929 burn=288 down=81 end
```

```
power=37.468 burn=309.0 down=396 temkcyc=896 end
```

```
power=33.564 burn=248.0 down=10 temkcyc=851 end
```

```
o 135 cr 5.9 mn 0.33
```

```
fe 13 co 0.075 ni 9.9
```

```
zr 221 nb 0.71 sn 3.6
```

```
-----
end
```

## ob171g29.input

```
=sas2h parm=skipshipdata
obrighiem (kwo) pwr, assm 171, batch 89, 29.04 gwd/mtu 3-cyc June 97
.....used 180 fuel rode, 16 guide tubes.....
```

```
-----
mixtures of fuel-pin-unit-cell:
```

```
44group latticecell
uo2 1 den=10.05 1 813
92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 813 end
kr-85 1 0 1-20 813 end
y-89 1 0 1-20 813 end
sr-90 1 0 1-20 813 end
zr-93 1 0 1-20 813 end
zr-94 1 0 1-20 813 end
zr-95 1 0 1-20 813 end
nb-94 1 0 1-20 813 end
mo-95 1 0 1-20 813 end
tc-99 1 0 1-20 813 end
ru-101 1 0 1-20 813 end
ru-106 1 0 1-20 813 end
rh-103 1 0 1-20 813 end
rh-105 1 0 1-20 813 end
pd-105 1 0 1-20 813 end
pd-108 1 0 1-20 813 end
ag-109 1 0 1-20 813 end
sb-124 1 0 1-20 813 end
xe-131 1 0 1-20 813 end
xe-132 1 0 1-20 813 end
xe-135 1 0 1-20 813 end
xe-136 1 0 1-20 813 end
cs-134 1 0 1-20 813 end
cs-135 1 0 1-20 813 end
cs-137 1 0 1-20 813 end
ba-136 1 0 1-20 813 end
la-139 1 0 1-20 813 end
pr-141 1 0 1-20 813 end
pr-143 1 0 1-20 813 end
ce-144 1 0 1-20 813 end
nd-143 1 0 1-20 813 end
nd-145 1 0 1-20 813 end
nd-147 1 0 1-20 813 end
pm-147 1 0 1-20 813 end
pm-148 1 0 1-20 813 end
sm-147 1 0 1-20 813 end
sm-149 1 0 1-20 813 end
sm-150 1 0 1-20 813 end
sm-151 1 0 1-20 813 end
sm-152 1 0 1-20 813 end
eu-153 1 0 1-20 813 end
eu-154 1 0 1-20 813 end
eu-155 1 0 1-20 813 end
gd-155 1 0 1-20 813 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 450.0e-6 572 end
```

```
450 ppm boron (wt) in moderator
```

```
-----
end comp
```

```
-----
fuel-pin-cell geometry:
```

```
squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end
-----
```

```
assembly and cycle parameters:
```

```
npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
```

```
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
power=29.124 burn=288 down=81 end
```

```
power=38.952 burn=309.0 down=396 temkcyc=905 end
```

```
power=34.748 burn=248.0 down=10 temkcyc=865 end
```

```
o 135 cr 5.9 mn 0.33
fe 13 co 0.075 ni 9.9
zr 221 nb 0.71 sa 3.6
```

```
-----
end
```

## ob172g26.input

=sas2h parm=skipshipdata

obrighiem (kwo) pwr, assm 172, batch 92, 26.54 gwd/mtu 3-cyc June 97

-----

mixtures of fuel-pin-unit-cell:

```

44group latticecell
uo2 1 den=10.05 1 865
92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 865 end
kr-85 1 0 1-20 865 end
y-89 1 0 1-20 865 end
sr-90 1 0 1-20 865 end
zr-93 1 0 1-20 865 end
zr-94 1 0 1-20 865 end
zr-95 1 0 1-20 865 end
nb-94 1 0 1-20 865 end
mo-95 1 0 1-20 865 end
tc-99 1 0 1-20 865 end
ru-101 1 0 1-20 865 end
ru-106 1 0 1-20 865 end
rh-103 1 0 1-20 865 end
rh-105 1 0 1-20 865 end
pd-105 1 0 1-20 865 end
pd-108 1 0 1-20 865 end
ag-109 1 0 1-20 865 end
sb-124 1 0 1-20 865 end
xe-131 1 0 1-20 865 end
xe-132 1 0 1-20 865 end
xe-135 1 0 1-20 865 end
xe-136 1 0 1-20 865 end
cs-134 1 0 1-20 865 end
cs-135 1 0 1-20 865 end
cs-137 1 0 1-20 865 end
ba-136 1 0 1-20 865 end
la-139 1 0 1-20 865 end
pr-141 1 0 1-20 865 end
pr-143 1 0 1-20 865 end
ce-144 1 0 1-20 865 end
nd-143 1 0 1-20 865 end
nd-145 1 0 1-20 865 end
nd-147 1 0 1-20 865 end
pm-147 1 0 1-20 865 end
pm-148 1 0 1-20 865 end
sm-147 1 0 1-20 865 end
sm-149 1 0 1-20 865 end
sm-150 1 0 1-20 865 end
sm-151 1 0 1-20 865 end
sm-152 1 0 1-20 865 end
eu-153 1 0 1-20 865 end
eu-154 1 0 1-20 865 end
eu-155 1 0 1-20 865 end
gd-155 1 0 1-20 865 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 450.0e-6 572 end

```

450 ppm boron (wt) in moderator

-----

end comp

-----

fuel-pin-cell geometry:

```

squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end

```

-----

assembly and cycle parameters:

```

npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5

```

```

printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
power=34.833 burn=288 down=81 end

```

```

power=25.035 burn=309.0 down=396 temkcyc=778 end

```

```

power=35.374 burn=248.0 down=10 temkcyc=870 end

```

```

o 135 cr 5.9 mn 0.33
fe 13 co 0.075 ni 9.9
zr 221 nb 0.71 sn 3.6

```

-----

end



ob176g29.input

=sas2h parm=skipshipdata  
obrighiem (kwo) pwr, assm 176, batch 90, 29.52 gwd/mtu 3-cyc June 97

.....  
' mixtures of fuel-pin-unit-cell:

44group latticecell  
uo2 1 den=10.05 1 840  
92234 0.028 92235 3.13 92236 0.014 92238 96.828 end  
kr-83 1 0 1-20 840 end  
kr-85 1 0 1-20 840 end  
y-89 1 0 1-20 840 end  
sr-90 1 0 1-20 840 end  
zr-93 1 0 1-20 840 end  
zr-94 1 0 1-20 840 end  
zr-95 1 0 1-20 840 end  
nb-94 1 0 1-20 840 end  
mo-95 1 0 1-20 840 end  
tc-99 1 0 1-20 840 end  
ru-101 1 0 1-20 840 end  
ru-106 1 0 1-20 840 end  
rh-103 1 0 1-20 840 end  
rh-105 1 0 1-20 840 end  
pd-105 1 0 1-20 840 end  
pd-108 1 0 1-20 840 end  
ag-109 1 0 1-20 840 end  
sb-124 1 0 1-20 840 end  
xe-131 1 0 1-20 840 end  
xe-132 1 0 1-20 840 end  
xe-135 1 0 1-20 840 end  
xe-136 1 0 1-20 840 end  
cs-134 1 0 1-20 840 end  
cs-135 1 0 1-20 840 end  
cs-137 1 0 1-20 840 end  
ba-136 1 0 1-20 840 end  
la-139 1 0 1-20 840 end  
pr-141 1 0 1-20 840 end  
pr-143 1 0 1-20 840 end  
ce-144 1 0 1-20 840 end  
nd-143 1 0 1-20 840 end  
nd-145 1 0 1-20 840 end  
nd-147 1 0 1-20 840 end  
pm-147 1 0 1-20 840 end  
pm-148 1 0 1-20 840 end  
sm-147 1 0 1-20 840 end  
sm-149 1 0 1-20 840 end  
sm-150 1 0 1-20 840 end  
sm-151 1 0 1-20 840 end  
sm-152 1 0 1-20 840 end  
eu-153 1 0 1-20 840 end  
eu-154 1 0 1-20 840 end  
eu-155 1 0 1-20 840 end  
gd-155 1 0 1-20 840 end  
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40  
40000 98.18 2 1.0 605 end  
h2o 3 den=0.7283 1 572 end  
arbm-bormod 0.7283 1 1 0 0 5000 100 3 450.0e-6 572 end

' 450 ppm boron (wt) in moderator

.....  
end comp

.....  
' fuel-pin-cell geometry:

squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end

' assembly and cycle parameters:

.....  
npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5  
printlevel=5 lightel=9 inplevel=2 numztotal=5 end  
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379  
power=32.121 burn=288 down=81 end  
power=36.801 burn=309.0 down=396 temkcyc=883 end  
power=35.875 burn=248.0 down=10 temkcyc=875 end  
o 135 cr 5.9 mn 0.33  
fe 13 co 0.075 ni 9.9  
zr 221 nb 0.71 sn 3.6

.....  
end

## ob176g27.input

=sas2h parm=skipshipdata

obrighiem (kwo) pwr, assm 176, batch 91, 27.99 gwd/mtu 3-cyc June 97

.....used 180 fuel rode, 16 guide tubes.....

-----

mixtures of fuel-pin-unit-cell:

```

44group latticecell
uo2 1 den=10.05 1 825
  92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 825 end
kr-85 1 0 1-20 825 end
y-89 1 0 1-20 825 end
sr-90 1 0 1-20 825 end
zr-93 1 0 1-20 825 end
zr-94 1 0 1-20 825 end
zr-95 1 0 1-20 825 end
nb-94 1 0 1-20 825 end
mo-95 1 0 1-20 825 end
tc-99 1 0 1-20 825 end
ru-101 1 0 1-20 825 end
ru-106 1 0 1-20 825 end
rh-103 1 0 1-20 825 end
rh-105 1 0 1-20 825 end
pd-105 1 0 1-20 825 end
pd-108 1 0 1-20 825 end
ag-109 1 0 1-20 825 end
sb-124 1 0 1-20 825 end
xe-131 1 0 1-20 825 end
xe-132 1 0 1-20 825 end
xe-135 1 0 1-20 825 end
xe-136 1 0 1-20 825 end
cs-134 1 0 1-20 825 end
cs-135 1 0 1-20 825 end
cs-137 1 0 1-20 825 end
ba-136 1 0 1-20 825 end
la-139 1 0 1-20 825 end
pr-141 1 0 1-20 825 end
pr-143 1 0 1-20 825 end
ce-144 1 0 1-20 825 end
nd-143 1 0 1-20 825 end
nd-145 1 0 1-20 825 end
nd-147 1 0 1-20 825 end
pm-147 1 0 1-20 825 end
pm-148 1 0 1-20 825 end
sm-147 1 0 1-20 825 end
sm-149 1 0 1-20 825 end
sm-150 1 0 1-20 825 end
sm-151 1 0 1-20 825 end
sm-152 1 0 1-20 825 end
eu-153 1 0 1-20 825 end
eu-154 1 0 1-20 825 end
eu-155 1 0 1-20 825 end
gd-155 1 0 1-20 825 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 450.0e-6 572 end

```

450 ppm boron (wt) in moderator

-----

end comp

-----

fuel-pin-cell geometry:

```

squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end

```

-----

assembly and cycle parameters:

npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5

printlevel=5 lightel=9 inplevel=2 numztotal=5 end

3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379

power=30.457 burn=288 down=81 end

power=34.894 burn=309.0 down=396 temkcyc=865 end

power=34.016 burn=248.0 down=10 temkcyc=855 end

o 135 cr 5.9 mn 0.33

fe 13 co 0.075 ni 9.9

zr 221 nb 0.71 sn 3.6

-----

end

## ob170g25plus100boron.input

```
=sas2h parm=skipshipdata
obrighiem (kwo) pwr, assm 170, batch 94, 25.93 gwd/mtu 3-cyc June97
.....used 180 fuel rode, 16 guide tubes....
```

```
-----
mixtures of fuel-pin-unit-cell:
```

```
44group latticecell
uo2 1 den=10.05 1 743
92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 743 end
kr-85 1 0 1-20 743 end
y-89 1 0 1-20 743 end
sr-90 1 0 1-20 743 end
zr-93 1 0 1-20 743 end
zr-94 1 0 1-20 743 end
zr-95 1 0 1-20 743 end
nb-94 1 0 1-20 743 end
mo-95 1 0 1-20 743 end
tc-99 1 0 1-20 743 end
ru-101 1 0 1-20 743 end
ru-106 1 0 1-20 743 end
rh-103 1 0 1-20 743 end
rh-105 1 0 1-20 743 end
pd-105 1 0 1-20 743 end
pd-108 1 0 1-20 743 end
ag-109 1 0 1-20 743 end
sb-124 1 0 1-20 743 end
xe-131 1 0 1-20 743 end
xe-132 1 0 1-20 743 end
xe-135 1 0 1-20 743 end
xe-136 1 0 1-20 743 end
cs-134 1 0 1-20 743 end
cs-135 1 0 1-20 743 end
cs-137 1 0 1-20 743 end
ba-136 1 0 1-20 743 end
la-139 1 0 1-20 743 end
pr-141 1 0 1-20 743 end
pr-143 1 0 1-20 743 end
ce-144 1 0 1-20 743 end
nd-143 1 0 1-20 743 end
nd-145 1 0 1-20 743 end
nd-147 1 0 1-20 743 end
pm-147 1 0 1-20 743 end
pm-148 1 0 1-20 743 end
sm-147 1 0 1-20 743 end
sm-149 1 0 1-20 743 end
sm-150 1 0 1-20 743 end
sm-151 1 0 1-20 743 end
sm-152 1 0 1-20 743 end
eu-153 1 0 1-20 743 end
eu-154 1 0 1-20 743 end
eu-155 1 0 1-20 743 end
gd-155 1 0 1-20 743 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 550.0e-6 572 end
```

```
550 ppm boron (wt) in moderator
```

```
-----
end comp
```

```
-----
fuel-pin-cell geometry:
```

```
squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end
```

```
assembly and cycle parameters:
```

```
npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
```

```
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
```

```
power=20.929 burn=288 down=81 end
```

```
power=37.468 burn=309.0 down=396 temkcyc=896 end
```

```
power=33.564 burn=248.0 down=10 temkcyc=851 end
```

```
o 135 cr 5.9 mn 0.33
```

```
fe 13 co 0.075 ni 9.9
```

```
zr 221 nb 0.71 sn 3.6
```

```
-----
end
```

## ob176g29plus100boron.input

```
=sas2h parm=skipshipdata
obrighiem (kwo) pwr, assm 176, batch 90, 29.52 gwd/mtu 3-cyc June 97
```

```
-----
mixtures of fuel-pin-unit-cell:
```

```
44group latticecell
uo2 1 den=10.05 1 840
  92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 840 end
kr-85 1 0 1-20 840 end
y-89 1 0 1-20 840 end
sr-90 1 0 1-20 840 end
zr-93 1 0 1-20 840 end
zr-94 1 0 1-20 840 end
zr-95 1 0 1-20 840 end
nb-94 1 0 1-20 840 end
mo-95 1 0 1-20 840 end
tc-99 1 0 1-20 840 end
ru-101 1 0 1-20 840 end
ru-106 1 0 1-20 840 end
rh-103 1 0 1-20 840 end
rh-105 1 0 1-20 840 end
pd-105 1 0 1-20 840 end
pd-108 1 0 1-20 840 end
ag-109 1 0 1-20 840 end
sb-124 1 0 1-20 840 end
xe-131 1 0 1-20 840 end
xe-132 1 0 1-20 840 end
xe-135 1 0 1-20 840 end
xe-136 1 0 1-20 840 end
cs-134 1 0 1-20 840 end
cs-135 1 0 1-20 840 end
cs-137 1 0 1-20 840 end
ba-136 1 0 1-20 840 end
la-139 1 0 1-20 840 end
pr-141 1 0 1-20 840 end
pr-143 1 0 1-20 840 end
ce-144 1 0 1-20 840 end
nd-143 1 0 1-20 840 end
nd-145 1 0 1-20 840 end
nd-147 1 0 1-20 840 end
pm-147 1 0 1-20 840 end
pm-148 1 0 1-20 840 end
sm-147 1 0 1-20 840 end
sm-149 1 0 1-20 840 end
sm-150 1 0 1-20 840 end
sm-151 1 0 1-20 840 end
sm-152 1 0 1-20 840 end
eu-153 1 0 1-20 840 end
eu-154 1 0 1-20 840 end
eu-155 1 0 1-20 840 end
gd-155 1 0 1-20 840 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 550.0e-6 572 end
```

```
550 ppm boron (wt) in moderator
```

```
-----
end comp
```

```
-----
fuel-pin-cell geometry:
```

```
squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end
```

```
assembly and cycle parameters:
```

```
npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
```

```
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
power=32.121 burn=288 down=81 end
```

```
power=36.801 burn=309.0 down=396 temkcy=883 end
```

```
power=35.875 burn=248.0 down=10 temkcy=875 end
```

```
o 135 cr 5.9 mn 0.33
fe 13 co 0.075 ni 9.9
zr 221 nb 0.71 sn 3.6
```

```
-----
end
```

ob168g28.sum

```

0.....
  |                                     |
  |          SCALE4.3  Bulletin Board   |
  |          -----                     |
  |          Welcome to SCALE-4.3.      |
  |                                     |
0.....

```

```

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
  module sas2h will be called
  obrightiem (kwo) pwr, assm 168, batch 86, 28.40 gwd/mtu 3-cyc June 97
  .....used 180 fuel rode, 16 guide tubes.....

```

```

  mixtures of fuel-pin-unit-cell:
44group latticecell
uo2 1 den=10.05 1 807
  92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 807 end
kr-85 1 0 1-20 807 end
y-89 1 0 1-20 807 end
sr-90 1 0 1-20 807 end
zr-93 1 0 1-20 807 end
zr-94 1 0 1-20 807 end
zr-95 1 0 1-20 807 end
nb-94 1 0 1-20 807 end
mo-95 1 0 1-20 807 end
tc-99 1 0 1-20 807 end
ru-101 1 0 1-20 807 end
ru-106 1 0 1-20 807 end
rh-103 1 0 1-20 807 end
rh-105 1 0 1-20 807 end
pd-105 1 0 1-20 807 end
pd-108 1 0 1-20 807 end
ag-109 1 0 1-20 807 end
sb-124 1 0 1-20 807 end
xe-131 1 0 1-20 807 end
xe-132 1 0 1-20 807 end
xe-135 1 0 1-20 807 end
xe-136 1 0 1-20 807 end
cs-134 1 0 1-20 807 end
cs-135 1 0 1-20 807 end
cs-137 1 0 1-20 807 end
ba-136 1 0 1-20 807 end
la-139 1 0 1-20 807 end
pr-141 1 0 1-20 807 end
pr-143 1 0 1-20 807 end
ce-144 1 0 1-20 807 end
nd-143 1 0 1-20 807 end
nd-145 1 0 1-20 807 end
nd-147 1 0 1-20 807 end
pm-147 1 0 1-20 807 end
pm-148 1 0 1-20 807 end
sm-147 1 0 1-20 807 end
sm-149 1 0 1-20 807 end
sm-150 1 0 1-20 807 end
sm-151 1 0 1-20 807 end
sm-152 1 0 1-20 807 end
eu-153 1 0 1-20 807 end
eu-154 1 0 1-20 807 end
eu-155 1 0 1-20 807 end
gd-155 1 0 1-20 807 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3.450.0e-6 572 end
  450 ppm boron (wt) in moderator
end comp

```

```

  fuel-pin-cell geometry:
squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end

```

```

  assembly and cycle parameters:
npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numztotal=5 end
3 0.6413 2 0.6845 3 0.8069 500 2.8238 3 2.8379
power=28.336 burn=288 down=81 end
power=38.005 burn=309 down=396 temkcyc=895 end
power=34.249 burn=248 down=10 temkcyc=860 end
o 135 cr 5.9 mn 0.33
fe 13 co 0.075 ni 9.9
zr 221 nb 0.71 sn 3.6

```

```

1 *****
*****
ss aa aa ss
ss aa aa ss
ss aa aa ss
ss aa aa ss
*****
*****
ss aa aa ss
ss aa aa ss
ss aa aa ss
*****
*****
*****
*****

```





ob170g25.sum

```

.....
:
:          SCALE4.3  Bulletin Board
:          -----
:
:          Welcome to SCALE-4.3.
:
:
:-----
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
  obrighiem (kwo) pwr, assm 170, batch 94, 25.93 gwd/mtu 3-cyc June97
  .....used 180 fuel rode, 16 guide tubes....
:-----
:
:  mixtures of fuel-pin-unit-cell:
:
:44group      latticecell
uo2 1 den=10.05 1 743
    92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 743 end
kr-85 1 0 1-20 743 end
y-89 1 0 1-20 743 end
sr-90 1 0 1-20 743 end
zr-93 1 0 1-20 743 end
zr-94 1 0 1-20 743 end
zr-95 1 0 1-20 743 end
nb-94 1 0 1-20 743 end
mo-95 1 0 1-20 743 end
tc-99 1 0 1-20 743 end
ru-101 1 0 1-20 743 end
ru-106 1 0 1-20 743 end
rh-103 1 0 1-20 743 end
rh-105 1 0 1-20 743 end
pd-105 1 0 1-20 743 end
pd-108 1 0 1-20 743 end
ag-109 1 0 1-20 743 end
sb-124 1 0 1-20 743 end
xe-131 1 0 1-20 743 end
xe-132 1 0 1-20 743 end
xe-135 1 0 1-20 743 end
xe-136 1 0 1-20 743 end
cs-134 1 0 1-20 743 end
cs-135 1 0 1-20 743 end
cs-137 1 0 1-20 743 end
ba-136 1 0 1-20 743 end
la-139 1 0 1-20 743 end
pr-141 1 0 1-20 743 end
pr-143 1 0 1-20 743 end
ce-144 1 0 1-20 743 end
nd-143 1 0 1-20 743 epd
nd-145 1 0 1-20 743 end
nd-147 1 0 1-20 743 end
pm-147 1 0 1-20 743 end
pm-148 1 0 1-20 743 end
sm-147 1 0 1-20 743 end
sm-149 1 0 1-20 743 end
sm-150 1 0 1-20 743 end
sm-151 1 0 1-20 743 end
sm-152 1 0 1-20 743 end
eu-153 1 0 1-20 743 end
eu-154 1 0 1-20 743 end
eu-155 1 0 1-20 743 end
gd-155 1 0 1-20 743 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
            40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 450.0e-6 572 end
:
: 450 ppm boron (wt) in moderator
:-----
:
:  fuel-pin-cell geometry:
:
squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end
:-----
:
:  assembly and cycle parameters:
:
mpin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numtotal=5 end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
power=20.929 burn=288 down=81 end
power=37.468 burn=309.0 down=396 tenkcyc=896 end
power=33.564 burn=248.0 down=10 tenkcyc=851 end
o 135 cr 5.9 mn 0.33
fe 13 co 0.075 ni 9.9
zr 221 nb 0.71 sn 3.6
:-----
1  SSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSSS  2222222222  hh  hh
SSSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSSS  222222222222  hh  hh
ss  ss  aa  aa  ss  ss  22  22  hh  hh
ss  ss  aa  aa  ss  ss  22  22  hh  hh
ss  ss  aa  aa  ss  ss  22  22  hh  hh
SSSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSSS  22  hhhhhhhhhhhh
SSSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSSS  22  hhhhhhhhhhhh
ss  ss  aa  aa  ss  ss  22  hh  hh
ss  ss  aa  aa  ss  ss  22  hh  hh
SS  SS  aa  aa  SS  SS  22  hh  hh
SSSSSSSSSSSS  aa  aa  SSSSSSSSSSS  222222222222  hh  hh
SSSSSSSSSSSS  aa  aa  SSSSSSSSSSS  222222222222  hh  hh
0

```







ob171g29.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....

```

```

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  obrighiem (kwo) pwr, assm 171, batch 89, 29.04 gwd/mtu 3-cyc June 97
  .....used 180 fuel rode, 16 guide tubes....

```

```

mixtures of fuel-pin-unit-cell:
44group latticecell
uo2 1 den=10.05 1 813
   92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 813 end
kr-85 1 0 1-20 813 end
y-89 1 0 1-20 813 end
sr-90 1 0 1-20 813 end
zr-93 1 0 1-20 813 end
zr-94 1 0 1-20 813 end
zr-95 1 0 1-20 813 end
nb-94 1 0 1-20 813 end
mo-95 1 0 1-20 813 end
tc-99 1 0 1-20 813 end
ru-101 1 0 1-20 813 end
ru-106 1 0 1-20 813 end
rh-103 1 0 1-20 813 end
rh-105 1 0 1-20 813 end
pd-105 1 0 1-20 813 end
pd-108 1 0 1-20 813 end
ag-109 1 0 1-20 813 end
sb-124 1 0 1-20 813 end
xe-131 1 0 1-20 813 end
xe-132 1 0 1-20 813 end
xe-135 1 0 1-20 813 end
xe-136 1 0 1-20 813 end
cs-134 1 0 1-20 813 end
cs-135 1 0 1-20 813 end
cs-137 1 0 1-20 813 end
ba-136 1 0 1-20 813 end
la-139 1 0 1-20 813 end
pr-141 1 0 1-20 813 end
pr-143 1 0 1-20 813 end
ce-144 1 0 1-20 813 end
nd-143 1 0 1-20 813 end
nd-145 1 0 1-20 813 end
nd-147 1 0 1-20 813 end
pm-147 1 0 1-20 813 end
pm-148 1 0 1-20 813 end
sm-147 1 0 1-20 813 end
sm-149 1 0 1-20 813 end
sm-150 1 0 1-20 813 end
sm-151 1 0 1-20 813 end
sm-152 1 0 1-20 813 end
eu-153 1 0 1-20 813 end
eu-154 1 0 1-20 813 end
eu-155 1 0 1-20 813 end
gd-155 1 0 1-20 813 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
            40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 450.0e-6 572 end
: 450 ppm boron (wt) in moderator
end comp

```

```

fuel-pin-cell geometry:
squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end

```

```

assembly and cycle parameters:
npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numsttotal=5 end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
power=29.124 burn=288 down=81 end
power=38.952 burn=309.0 down=396 temkcy=905 end
power=34.748 burn=248.0 down=10 temkcy=865 end
o 135 cr 5.9 mn 0.33
fe 13 co 0.075 ni 9.9
zr 221 nb 0.71 sn 3.6

```

```

1  SSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  2222222222  hh  hh
   SSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  2222222222  hh  hh
SS  SS  AA  AA  SS  SS  22  22  hh  hh
SS  SS  AA  AA  SS  SS  22  22  hh  hh
SS  SS  AA  AA  SS  SS  22  22  hh  hh
SSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  22  hhhhhhhhhhhh
SSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  22  hhhhhhhhhhhhh
SS  SS  AA  AA  SS  SS  22  hh  hh
SS  SS  AA  AA  SS  SS  22  hh  hh
SS  SS  AA  AA  SS  SS  22  hh  hh
SSSSSSSSSSS  AA  AA  SSSSSSSSSS  2222222222  hh  hh
SSSSSSSSSSS  AA  AA  SSSSSSSSSS  2222222222  hh  hh
0

```

```

nn      nn      iiiiiiiiii      cccccccccc      hh      hh      oooooooooo      ll
nnn     nn      iiiiiiiiii      cccccccccc      hh      hh      oooooooooo      ll
nnnn    nn      ii           cc           cc      hh      hh      oo           oo      ll
nn nn   nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn     nn      ii           cc           cc      hhhhhhhhhhhh      oo           oo      ll
nn      nn      ii           cc           cc      hhhhhhhhhhhh      oo           oo      ll
nn     nn      ii           cc           cc      hh      hh      oo           oo      ll
nn     nn      ii           cc           cc      hh      hh      oo           oo      ll
nn     nn      ii           cc           cc      hh      hh      oo           oo      ll
nn     nn      ii           cc           cc      hh      hh      oo           oo      ll
nn     nn      ii           cc           cc      hh      hh      oo           oo      ll
nn     nn      ii           cc           cc      hh      hh      oo           oo      ll
nn     nn      iiiiiiiiii      cccccccccc      hh      hh      oooooooooo      ll
nn     nn      iiiiiiiiii      cccccccccc      hh      hh      oooooooooo      ll

```

```

00000000      8888888888      //      00000000      8888888888      //      9999999999      7777777777
0000000000      888888888888      //      0000000000      888888888888      //      999999999999      7777777777
00      00      88      88      //      00      00      88      88      //      99      99      77
00      00      88      88      //      00      00      88      88      //      99      99      77
00      00      88      88      //      00      00      88      88      //      99      99      77
00      00      8888888888      //      00      00      8888888888      //      999999999999      77
00      00      888888888888      //      00      00      888888888888      //      999999999999      77
00      00      88      88      //      00      00      88      88      //      99      99      77
00      00      88      88      //      00      00      88      88      //      99      99      77
00      00      88      88      //      00      00      88      88      //      99      99      77
0000000000      888888888888      //      0000000000      888888888888      //      999999999999      77
00000000      8888888888      //      00000000      8888888888      //      999999999999      77

```

```

2222222222      00000000      //      2222222222      8888888888      //      00000000      6666666666
222222222222      0000000000      //      222222222222      888888888888      //      0000000000      6666666666
22      22      00      00      //      22      22      88      88      //      00      00      66
22      22      00      00      //      22      22      88      88      //      00      00      66
22      22      00      00      //      22      22      88      88      //      00      00      66
22      22      00      00      //      22      22      8888888888      //      00      00      6666666666
22      22      00      00      //      22      22      8888888888      //      00      00      6666666666
22      22      00      00      //      22      22      88      88      //      00      00      66
22      22      00      00      //      22      22      88      88      //      00      00      66
22      22      00      00      //      22      22      88      88      //      00      00      66
22      22      00      00      //      22      22      88      88      //      00      00      66
222222222222      0000000000      //      222222222222      888888888888      //      0000000000      6666666666
222222222222      00000000      //      222222222222      888888888888      //      00000000      6666666666

```

```

1
0
ssssssssss      cccccccccc      aaaaaaaaaa      ll      eeeeeeeeeeee
ssssssssssss      cccccccccc      aaaaaaaaaa      ll      eeeeeeeeeeee
ss      ss      cc           cc      aa           aa      ll      ee
ss      ss      cc           cc      aa           aa      ll      ee
ss      ss      cc           cc      aa           aa      ll      ee
ssssssssssss      cc           aa           aa      ll      eeeeeeee
ssssssssssss      cc           aa           aa      ll      eeeeeeee
ss      ss      cc           aa           aa      ll      ee
ss      ss      cc           aa           aa      ll      ee
ss      ss      cc           aa           aa      ll      ee
ss      ss      cc           cc      aa           aa      ll      ee
ssssssssssss      cccccccccc      aa           aa      llllllllllll      eeeeeeeeeeee
ssssssssssss      cccccccccc      aa           aa      llllllllllll      eeeeeeeeeeee

```

```

.....
program verification information
code system:  scale version:  4.3
.....
program:  sas2
creation date:  03/07/97
library:  /opt/neut/Scale4.3/bin
.....
this is not a  scale configuration controlled code
jobname:  nichol
date of execution:  08/08/97
time of execution:  20:28:06
.....

```

1  
0  
0  
0  
0  
0  
0  
0  
0  
0  
0  
0

```

.....used 180 fuel rods, 16 guide tubes....
.....
nuclide concentrations, grams
basis =single reactor assembly
o 16      initial 1E-18 d
          1.35E+05  1.35E+05
total    3.90E+05  3.90E+05
.....
nuclide concentrations, grams
basis =single reactor assembly
u234      initial 1E-18 d
          2.80E+02  2.80E+02
u235      3.13E+04  3.13E+04
u236      1.40E+02  1.40E+02
u238      9.68E+05  9.68E+05
total    1.00E+06  1.00E+06
.....
basis =
initial    14.4 d      28.8 d      43.2 d      57.6 d      57.6 d
initial    14.4 d      28.8 d      43.2 d      57.6 d      57.6 d
.....
nuclide concentrations, grams
basis =single reactor assembly
initial    1.7 d      3.3 d      5.0 d      6.7 d      8.3 d      10.0 d

```



ob172g26.sum

```

.....
*
*          SCALE4.3  Bulletin  Board
*          -----
*
*          Welcome to SCALE-4.3.
*
*
.....

```

```

1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
   obrighiem (kwo) pwr. assm 172, batch 92, 26.54 gwd/mtu 3-cyc June 97

```

```

-----
:  mixtures of fuel-pin-unit-cell:
:
44group      latticecell
uo2 1 den=10.05 1 865
    92234 0.028 92235 3.13 92236 0.014 92238 96.828  end
kr-83 1 0 1-20 865  end
kr-85 1 0 1-20 865  end
y-89 1 0 1-20 865  end
sr-90 1 0 1-20 865  end
zr-93 1 0 1-20 865  end
zr-94 1 0 1-20 865  end
zr-95 1 0 1-20 865  end
nb-94 1 0 1-20 865  end
mo-95 1 0 1-20 865  end
tc-99 1 0 1-20 865  end
ru-101 1 0 1-20 865  end
ru-106 1 0 1-20 865  end
rh-103 1 0 1-20 865  end
rh-105 1 0 1-20 865  end
pd-105 1 0 1-20 865  end
pd-108 1 0 1-20 865  end
ag-109 1 0 1-20 865  end
sb-124 1 0 1-20 865  end
xe-131 1 0 1-20 865  end
xe-132 1 0 1-20 865  end
xe-135 1 0 1-20 865  end
xe-136 1 0 1-20 865  end
ca-134 1 0 1-20 865  end
cs-135 1 0 1-20 865  end
cs-137 1 0 1-20 865  end
ba-136 1 0 1-20 865  end
la-139 1 0 1-20 865  end
pr-141 1 0 1-20 865  end
pr-143 1 0 1-20 865  end
ce-144 1 0 1-20 865  end
nd-143 1 0 1-20 865  end
nd-145 1 0 1-20 865  end
nd-147 1 0 1-20 865  end
pm-147 1 0 1-20 865  end
pm-148 1 0 1-20 865  end
sm-147 1 0 1-20 865  end
sm-149 1 0 1-20 865  end
sm-150 1 0 1-20 865  end
sm-151 1 0 1-20 865  end
sm-152 1 0 1-20 865  end
eu-153 1 0 1-20 865  end
eu-154 1 0 1-20 865  end
eu-155 1 0 1-20 865  end
gd-155 1 0 1-20 865  end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
            40000 98.18 2 1.0 605  end
h2o 3 den=0.7283 1 572  end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 450.0e-6 572  end
:
:  450 ppm boron (wt) in moderator
:
-----
end comp

```

```

-----
:  fuel-pin-cell geometry:
:
squarepitch 1.43 0.913 1 3 1.074 2 0.930 0  end

```

```

-----
:  assembly and cycle parameters:
:
npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numztotal=5  end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
power=34.833 burn=288 down=81  end
power=25.035 burn=309.0 down=196 temkcyc=778  end
power=35.374 burn=248.0 down=10 temkcyc=870  end
o 135 cr 5.9 mm 0.33
fe 13 co 0.075 ni 9.9
zr 221 nb 0.71 sn 3.6

```

```

1  SSSSSSSSSS  aaaaaaaaaa  SSSSSSSSSS  2222222222  hh  hh
SSSSSSSSSSS  aaaaaaaaaa  SSSSSSSSSS  222222222222  hh  hh
SS  SS  aa  aa  SS  SS  22  22  hh  hh
SS  SS  aa  aa  SS  SS  22  22  hh  hh
SS  SS  aa  aa  SS  SS  22  22  hh  hh
SSSSSSSSSSS  aaaaaaaaaa  SSSSSSSSSS  22  hhhhhhhhhhhh
SSSSSSSSSSS  aaaaaaaaaa  SSSSSSSSSS  22  hhhhhhhhhhhhh
SS  SS  aa  aa  SS  SS  22  hh  hh
SS  SS  aa  aa  SS  SS  22  hh  hh
SS  SS  aa  aa  SS  SS  22  hh  hh
SSSSSSSSSSS  aa  aa  SSSSSSSSSS  222222222222  hh  hh
SSSSSSSSSSS  aa  aa  SSSSSSSSSS  222222222222  hh  hh
0

```







ob176g29.sum

```

0.....
  |
  |          SCALE4.3  Bulletin  Board
  |          -----
  |
  |          Welcome to SCALE-4.3.
  |
  |.....
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
  obrighiem (kwo) pwr, assm 176, batch 90, 29.52 gwd/mtu 3-cyc June 97

```

```

-----
: mixtures of fuel-pin-unit-cell:
44group latticecell
uo2 1 den=10.05 1 840
  92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 840 end
kr-85 1 0 1-20 840 end
y-89 1 0 1-20 840 end
sr-90 1 0 1-20 840 end
zr-93 1 0 1-20 840 end
zr-94 1 0 1-20 840 end
zr-95 1 0 1-20 840 end
nb-94 1 0 1-20 840 end
mo-95 1 0 1-20 840 end
tc-99 1 0 1-20 840 end
ru-101 1 0 1-20 840 end
ru-106 1 0 1-20 840 end
rh-103 1 0 1-20 840 end
rh-105 1 0 1-20 840 end
pd-105 1 0 1-20 840 end
pd-108 1 0 1-20 840 end
ag-109 1 0 1-20 840 end
sb-124 1 0 1-20 840 end
xe-131 1 0 1-20 840 end
xe-132 1 0 1-20 840 end
xe-135 1 0 1-20 840 end
xe-136 1 0 1-20 840 end
cs-134 1 0 1-20 840 end
cs-135 1 0 1-20 840 end
cs-137 1 0 1-20 840 end
ba-136 1 0 1-20 840 end
la-139 1 0 1-20 840 end
pr-141 1 0 1-20 840 end
pr-143 1 0 1-20 840 end
ce-144 1 0 1-20 840 end
nd-143 1 0 1-20 840 end
nd-145 1 0 1-20 840 end
nd-147 1 0 1-20 840 end
pm-147 1 0 1-20 840 end
pm-148 1 0 1-20 840 end
sm-147 1 0 1-20 840 end
sm-149 1 0 1-20 840 end
sm-150 1 0 1-20 840 end
sm-151 1 0 1-20 840 end
sm-152 1 0 1-20 840 end
eu-153 1 0 1-20 840 end
eu-154 1 0 1-20 840 end
eu-155 1 0 1-20 840 end
gd-155 1 0 1-20 840 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 450.0e-6 572 end
: 450 ppm boron (wt) in moderator
:
end comp

```

```

-----
: fuel-pin-cell geometry:
squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end

```

```

-----
: assembly and cycle parameters:
npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numztotal=5 end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
power=32.121 burn=288 down=81 end
power=36.801 burn=309.0 down=396 temkcy=883 end
power=35.875 burn=248.0 down=10 temkcy=875 end
o 135 cr 5.9 sn 0.33
fe 13 co 0.075 ni 9.9
zr 221 nb 0.71 sn 3.6

```

```

1  SSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  2222222222  hh  hh
SSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  2222222222  hh  hh
SS  SS  AA  AA  SS  SS  22  22  hh  hh
SS  SS  AA  AA  SS  SS  22  22  hh  hh
SS  SS  AA  AA  SS  SS  22  22  hh  hh
SSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  22  hhhhhhhhhhhh
SSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  22  hhhhhhhhhhhh
SS  SS  AA  AA  SS  SS  22  hh  hh
SS  SS  AA  AA  SS  SS  22  hh  hh
SS  SS  AA  AA  SS  SS  22  hh  hh
SSSSSSSSSSS  AA  AA  SSSSSSSSSS  2222222222  hh  hh
SSSSSSSSSSS  AA  AA  SSSSSSSSSS  2222222222  hh  hh

```

0

```

nn      nn      iiiiiiiiii      cccccccccc      hh      hh      oooooooooo      ll
nnn     nn      iiiiiiiiii      cccccccccc      hh      hh      oooooooooooooo      ll
nnnn    nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      ii           cc           cc      hh      hh      oo           oo      ll
nn  nn  nn      iiiiiiiiii      cccccccccc      hh      hh      oooooooooooooo      ll
nn  nn  nn      iiiiiiiiii      cccccccccc      hh      hh      oooooooooooooo      ll

```

```

00000000      888888888888      //      00000000      888888888888      //      999999999999      777777777777
0000000000      88888888888888      //      0000000000      88888888888888      //      99999999999999      777777777777
00      00      88      88      //      00      00      88      88      //      99      99      77      77
00      00      88      88      //      00      00      88      88      //      99      99      77      77
00      00      88      88      //      00      00      88      88      //      99      99      77      77
00      00      888888888888      //      00      00      888888888888      //      99999999999999      77
00      00      888888888888      //      00      00      888888888888      //      99999999999999      77
00      00      88      88      //      00      00      88      88      //      99      99      77      77
00      00      88      88      //      00      00      88      88      //      99      99      77      77
00      00      88      88      //      00      00      88      88      //      99      99      77      77
0000000000      88888888888888      //      0000000000      88888888888888      //      99999999999999      77
00000000      88888888888888      //      00000000      88888888888888      //      99999999999999      77

```

```

2222222222      11      3333333333      555555555555      11      888888888888
222222222222      111      333333333333      55555555555555      111      88888888888888
22      22      1111      :::      33      33      55      55      :::      1111      88      88
      22      11      :::      33      33      55      55      :::      11      88      88
      22      11      :::      33      33      55      55      :::      11      88      88
      22      11      :::      33      33      55      55      :::      11      88      88
      22      11      :::      33      33      55      55      :::      11      88      88
      22      11      :::      33      33      55      55      :::      11      88      88
      22      11      :::      33      33      55      55      :::      11      88      88
222222222222      11111111      333333333333      55555555555555      11111111      88888888888888
222222222222      11111111      333333333333      55555555555555      11111111      88888888888888

```

```

1
0
#####      cccccccccc      ll      cccccccccc
#####      cccccccccc      ll      cccccccccc
ss      ss      cc      cc      aa      aa      ll      ee      ee
ss      cc      cc      aa      aa      aa      ll      ee      ee
ss      cc      cc      aa      aa      aa      ll      ee      ee
#####      cc      aaaaaaaaaa      ll      cccccccccc
#####      cc      aaaaaaaaaa      ll      cccccccccc
      ss      cc      aa      aa      ll      ee      ee
      ss      cc      aa      aa      ll      ee      ee
      ss      cc      aa      aa      ll      ee      ee
#####      cccccccccc      ll      cccccccccc
#####      cccccccccc      ll      cccccccccc

```

```

.....
.....
.....
program verification information
.....
code system: scale version: 4.3
.....
.....
program: sas2
.....
creation date: 03/07/97
.....
library: /opt/neut/Scale4.3/bin
.....
this is not a scale configuration controlled code
.....
jobname: nichol
.....
date of execution: 08/08/97
.....
time of execution: 21:35:18
.....
.....
.....

```

```

1
0
0
0
-----
nuclide concentrations, grams
basis =single reactor assembly

o 16      initial 1E-18 d
total 1.35E+05 1.35E+05
total 3.90E+05 3.90E+05

nuclide concentrations, grams
basis =single reactor assembly

u234      initial 1E-18 d
u235      2.80E+02 2.80E+02
u236      3.13E+04 3.13E+04
u238      1.40E+02 1.40E+02
total 9.68E+05 9.68E+05
total 1.00E+06 1.00E+06

basis =
initial 14.4 d      28.8 d      43.2 d      57.6 d      57.6 d
initial 14.4 d      28.8 d      43.2 d      57.6 d      57.6 d

nuclide concentrations, grams
basis =single reactor assembly
initial 1.7 d      3.3 d      5.0 d      6.7 d      8.3 d      10.0 d

```



ob176g27.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....

```

```

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  obrighiem (kwo) pwr, assm 176, batch 91, 27.99 gwd/mtu 3-cyc June 97
  ....used 180 fuel rode, 16 guide tubes....

```

```

-----
mixtures of fuel-pin-unit-cell:
44group latticecell
uo2 1 den=10.05 1 825
  92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 825 end
kr-85 1 0 1-20 825 end
y-89 1 0 1-20 825 end
sr-90 1 0 1-20 825 end
zr-93 1 0 1-20 825 end
zr-94 1 0 1-20 825 end
zr-95 1 0 1-20 825 end
nb-94 1 0 1-20 825 end
mo-95 1 0 1-20 825 end
tc-99 1 0 1-20 825 end
ru-101 1 0 1-20 825 end
ru-106 1 0 1-20 825 end
rh-103 1 0 1-20 825 end
rh-105 1 0 1-20 825 end
pd-105 1 0 1-20 825 end
pd-108 1 0 1-20 825 end
ag-109 1 0 1-20 825 end
sb-124 1 0 1-20 825 end
xe-131 1 0 1-20 825 end
xe-132 1 0 1-20 825 end
xe-135 1 0 1-20 825 end
xe-136 1 0 1-20 825 end
cs-134 1 0 1-20 825 end
cs-135 1 0 1-20 825 end
cs-137 1 0 1-20 825 end
ba-136 1 0 1-20 825 end
la-139 1 0 1-20 825 end
pr-141 1 0 1-20 825 end
pr-143 1 0 1-20 825 end
ce-144 1 0 1-20 825 end
nd-143 1 0 1-20 825 end
nd-145 1 0 1-20 825 end
nd-147 1 0 1-20 825 end
pm-147 1 0 1-20 825 end
pm-148 1 0 1-20 825 end
sm-147 1 0 1-20 825 end
sm-149 1 0 1-20 825 end
sm-150 1 0 1-20 825 end
sm-151 1 0 1-20 825 end
sm-152 1 0 1-20 825 end
eu-153 1 0 1-20 825 end
eu-154 1 0 1-20 825 end
eu-155 1 0 1-20 825 end
gd-155 1 0 1-20 825 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 450.0e-6 572 end
. 450 ppm boron (wt) in moderator
-----
end comp

```

```

-----
fuel-pin-cell geometry:
squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end
-----

```

```

-----
assembly and cycle parameters:
npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numztotal=5 end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
power=30.457 burn=288 down=81 end
power=34.894 burn=309.0 down=396 temkyc=865 end
power=34.016 burn=248.0 down=10 temkyc=855 end
o 135 cr 5.9 mm 0.33
fe 13 co 0.075 ni 9.9
zr 221 nb 0.71 sn 3.6
-----

```

```

1  SSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  2222222222  hh  hh
  SSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  2222222222  hh  hh
  SS  SS  AA  AA  SS  SS  22  22  hh  hh
  SS  SS  AA  AA  SS  SS  22  22  hh  hh
  SS  SS  AA  AA  SS  SS  22  22  hh  hh
  SSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  22  hhhhhhhhhhhh
  SSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  22  hhhhhhhhhhhh
  SS  SS  AA  AA  SS  SS  22  hh  hh
  SS  SS  AA  AA  SS  SS  22  hh  hh
  SSSSSSSSSS  AA  AA  SSSSSSSSSS  2222222222  hh  hh
  SSSSSSSSSS  AA  AA  SSSSSSSSSS  2222222222  hh  hh
0

```





ob170g25plus100boron.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....

```

```

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  obrighiem (kwo) pwr, assm 170, batch 94, 25.93 gwd/mtu 3-cyc June97
  .....used 180 fuel rode, 16 guide tubes....

```

```

mixtures of fuel-pin-unit-cell:
44group latticecell
uo2 1 den=10.05 1 743
  92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 743 end
kr-85 1 0 1-20 743 end
y-89 1 0 1-20 743 end
sr-90 1 0 1-20 743 end
zr-93 1 0 1-20 743 end
zr-94 1 0 1-20 743 end
zr-95 1 0 1-20 743 end
nb-94 1 0 1-20 743 end
mo-95 1 0 1-20 743 end
tc-99 1 0 1-20 743 end
ru-101 1 0 1-20 743 end
ru-106 1 0 1-20 743 end
rh-103 1 0 1-20 743 end
rh-105 1 0 1-20 743 end
pd-105 1 0 1-20 743 end
pd-108 1 0 1-20 743 end
ag-109 1 0 1-20 743 end
sb-124 1 0 1-20 743 end
xe-131 1 0 1-20 743 end
xe-132 1 0 1-20 743 end
xe-135 1 0 1-20 743 end
xe-136 1 0 1-20 743 end
cs-134 1 0 1-20 743 end
cs-135 1 0 1-20 743 end
cs-137 1 0 1-20 743 end
ba-136 1 0 1-20 743 end
la-139 1 0 1-20 743 end
pr-141 1 0 1-20 743 end
pr-143 1 0 1-20 743 end
ce-144 1 0 1-20 743 end
nd-143 1 0 1-20 743 end
nd-145 1 0 1-20 743 end
nd-147 1 0 1-20 743 end
pm-147 1 0 1-20 743 end
pm-148 1 0 1-20 743 end
sm-147 1 0 1-20 743 end
sm-149 1 0 1-20 743 end
sm-150 1 0 1-20 743 end
sm-151 1 0 1-20 743 end
sm-152 1 0 1-20 743 end
eu-153 1 0 1-20 743 end
eu-154 1 0 1-20 743 end
eu-155 1 0 1-20 743 end
gd-155 1 0 1-20 743 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 550.0e-6 572 end
550 ppm boron (wt) in moderator
end comp

```

```

fuel-pin-cell geometry:
squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end

```

```

assembly and cycle parameters:
npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numstotal=5 end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
power=20.929 burn=288 down=81 end
power=37.468 burn=309.0 down=396 temkcyc=896 end
power=33.564 burn=248.0 down=10 temkcyc=851 end
o 135 cr 5.9 mn 0.33
fe 13 co 0.075 ni 9.9
zr 221 nb 0.71 sn 3.6

```

```

1 #####          #####          #####          222222222222 hh hh
#####          #####          #####          222222222222 hh hh
ss          ss          ss          ss          22          22 hh hh
ss          ss          ss          ss          22          22 hh hh
ss          ss          ss          ss          22          22 hh hh
#####          #####          #####          22          hhhhhhhhhhhhh
#####          #####          #####          22          hhhhhhhhhhhhh
ss          ss          ss          ss          22          hh hh
ss          ss          ss          ss          22          hh hh
ss          ss          ss          ss          22          hh hh
ss          ss          ss          ss          22          hh hh
#####          #####          #####          222222222222 hh hh
#####          #####          #####          222222222222 hh hh
0

```







ob176g29plus100boron.sum

SCALE4.3 Bulletin Board
Welcome to SCALE-4.3.

primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
module sas2h will be called
obrighiem (kwo) pwr, assm 176, batch 90, 29.52 gwd/mtu 3-cyc June 97

mixtures of fuel-pin-unit-cell:

44group latticecell
uo2 1 den=10.05 1 840
92234 0.028 92235 3.13 92236 0.014 92238 96.828 end
kr-83 1 0 1-20 840 end
kr-85 1 0 1-20 840 end
y-89 1 0 1-20 840 end
sr-90 1 0 1-20 840 end
zr-93 1 0 1-20 840 end
zr-94 1 0 1-20 840 end
zr-95 1 0 1-20 840 end
nb-94 1 0 1-20 840 end
mo-95 1 0 1-20 840 end
tc-99 1 0 1-20 840 end
ru-101 1 0 1-20 840 end
ru-106 1 0 1-20 840 end
rh-103 1 0 1-20 840 end
rh-105 1 0 1-20 840 end
pd-105 1 0 1-20 840 end
pd-108 1 0 1-20 840 end
ag-109 1 0 1-20 840 end
sb-124 1 0 1-20 840 end
xe-131 1 0 1-20 840 end
xe-132 1 0 1-20 840 end
xe-135 1 0 1-20 840 end
xe-136 1 0 1-20 840 end
cs-134 1 0 1-20 840 end
cs-135 1 0 1-20 840 end
cs-137 1 0 1-20 840 end
ba-136 1 0 1-20 840 end
la-139 1 0 1-20 840 end
pr-141 1 0 1-20 840 end
pr-143 1 0 1-20 840 end
ce-144 1 0 1-20 840 end
nd-143 1 0 1-20 840 end
nd-145 1 0 1-20 840 end
nd-147 1 0 1-20 840 end
pm-147 1 0 1-20 840 end
pm-148 1 0 1-20 840 end
sm-147 1 0 1-20 840 end
sm-149 1 0 1-20 840 end
sm-150 1 0 1-20 840 end
sm-151 1 0 1-20 840 end
sm-152 1 0 1-20 840 end
eu-153 1 0 1-20 840 end
eu-154 1 0 1-20 840 end
eu-155 1 0 1-20 840 end
gd-155 1 0 1-20 840 end
arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 605 end
h2o 3 den=0.7283 1 572 end
arbm-bormod 0.7283 1 1 0 0 5000 100 3 550.0e-6 572 end

550 ppm boron (wt) in moderator

end comp

fuel-pin-cell geometry:

squarepitch 1.43 0.913 1 3 1.074 2 0.930 0 end

assembly and cycle parameters:

npin/assm=180 fuelnght=957.89 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numstotal=5 end
3 0.6413 2 0.6845 3 0.8068 500 2.8238 3 2.8379
power=32.121 burn=288 down=81 end
power=36.801 burn=309.0 down=396 temkcyc=883 end
power=35.875 burn=248.0 down=10 temkcyc=875 end
o 135 cr 5.9 ni 0.33
fe 13 co 0.075 ni 9.9
zr 221 nb 0.71 sn 3.6

1 sssssssss aaaaaaaaa sssssssss 222222222 hh hh
ss aa aa ss ss 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 222222222 hh hh
ss aa aa sssssssss 222222222 hh hh

```

nn      nn      iiiiiiiiii      cccccccccc      hh      hh      oooooooooo      11
nnn     nn     iiiiiiiiii     cccccccccc     hh     hh     oooooooooooooo     11
nnnn    nn    11           cc          cc      hh      hh      oo          oo     11
nn nn   nn    11           cc          hh      hh      oo          oo     11
nn nn   nn    11           cc          hh      hh      oo          oo     11
nn nn   nn    11           cc          hhhhhhhhhhhhh     oo          oo     11
nn nn   nn    11           cc          hhhhhhhhhhhhh     oo          oo     11
nn nn   nn    11           cc          hh      hh      oo          oo     11
nn nn   nn    11           cc          hh      hh      oo          oo     11
nn nn   nn    11           cc          hh      hh      oo          oo     11
nn      nnn    11           cc          cc      hh      hh      oo          oo     11
nn      nnn    iiiiiiiiii     cccccccccc     hh      hh      oooooooooooooo     1111111111111111
nn      nn     iiiiiiiiii     cccccccccc     hh      hh      oooooooooooooo     1111111111111111
0
 00000000      8888888888      //      00000000      8888888888      //      9999999999      7777777777777
00000000      8888888888      //      00000000      8888888888      //      9999999999      77777777777
00      00      88      88      //      00      00      88      88      //      99      99      77
00      00      88      88      //      00      00      88      88      //      99      99      77
00      00      88      88      //      00      00      88      88      //      99      99      77
00      00      88      88      //      00      00      88      88      //      99      99      77
00      00      8888888888      //      00      00      8888888888      //      9999999999      77
00      00      8888888888      //      00      00      8888888888      //      9999999999      77
00      00      88      88      //      00      00      88      88      //      99      99      77
00      00      88      88      //      00      00      88      88      //      99      99      77
00      00      88      88      //      00      00      88      88      //      99      99      77
0000000000      88888888888888      //      0000000000      88888888888888      //      99999999999999      77
00000000      8888888888      //      00000000      8888888888      //      99999999999999      77
0
2222222222222222      2222222222222222      //      2222222222222222      00000000      //      00000000      3333333333333
2222222222222222      2222222222222222      //      2222222222222222      000000000000      //      000000000000      3333333333333
22      22      22      //      22      22      00      00      //      00      00      33
22      22      22      //      22      22      00      00      //      00      00      33
22      22      22      //      22      22      00      00      //      00      00      33
22      22      22      //      22      22      00      00      //      00      00      33
22      22      22      //      22      22      00      00      //      00      00      33
22      22      22      //      22      22      00      00      //      00      00      33
22      22      22      //      22      22      00      00      //      00      00      33
22      22      22      //      22      22      00      00      //      00      00      33
2222222222222222      2222222222222222      //      2222222222222222      0000000000      //      0000000000      3333333333333
2222222222222222      2222222222222222      //      2222222222222222      00000000      //      00000000      3333333333333
1
0
  sssssssssss      cccccccccc      aaaaaaaaa      11      eeeeeeeeeee
  sssssssssss      cccccccccc      aaaaaaaaa      11      eeeeeeeeeee
  ss      ss      cc          cc      aa          aa      11      ee
  ss      ss      cc          cc      aa          aa      11      ee
  ss      ss      cc          cc      aa          aa      11      ee
  sssssssssss      cc          aaaaaaaaa      11      eeeeeeee
  sssssssssss      cc          aaaaaaaaa      11      eeeeeeee
  ss      ss      cc          aa          aa      11      ee
  ss      ss      cc          aa          aa      11      ee
  ss      ss      cc          aa          aa      11      ee
  sssssssssss      cccccccccc      aa          aa      1111111111111111      eeeeeeeeeeee
  sssssssssss      cccccccccc      aa          aa      1111111111111111      eeeeeeeeeeee

```

```

.....
program verification information
.....
code system:   scale version:   4.3
.....
.....
program:   sas2
.....
creation date:   03/07/97
.....
library:   /opt/neut/Scale4.3/bin
.....
this is not a   scale configuration controlled code
.....
jobname:   nichol
.....
date of execution:   08/08/97
.....
time of execution:   22:20:03
.....
.....

```

1	0	0	0	0
0	0	0	0	0
0	-----			
0	nuclide concentrations, grams			
	basis =single reactor assembly			
0	initial	1E-18 d		
o	16	1.35E+05	1.35E+05	
0	total	3.90E+05	3.90E+05	
0	nuclide concentrations, grams			
	basis =single reactor assembly			
	initial	1E-18 d		
u	234	2.80E+02	2.80E+02	
u	235	3.13E+04	3.13E+04	
u	236	1.40E+02	1.40E+02	
u	238	9.68E+05	9.68E+05	
0	total	1.00E+06	1.00E+06	
0		initial	14.4 d	28.8 d
0		initial	14.4 d	28.8 d
0			43.2 d	57.6 d
			43.2 d	57.6 d
		initial	1.7 d	3.3 d
			5.0 d	6.7 d
			8.3 d	10.0 d

