

CRWMS/M&O

Design Analysis Cover Sheet

Complete only applicable items.

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9. Lead Design Engineer	Dan Thomas	<i>D. Thomas</i>	09/02/97
10. Department Manager	Hugh Benton	<i>Hugh A. Benton</i>	9/2/97
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1. Purpose

The purpose of this design analysis is to determine the accuracy of the SAS2H module of SCALE 4.3 in predicting isotopic concentrations of spent fuel assemblies. The objective is to develop a methodology for modeling assemblies similar to those evaluated within this analysis and to establish the consistency of SAS2H predictions. The results of this analysis may then be applied to future depletion calculations using SAS2H in which no measurements are available.

2. Quality Assurance

The Quality Assurance (QA) program applies to this analysis. The work reported in this document is part of the Waste Package Design analysis that will eventually support the License Application Design phase. This activity, when appropriately confirmed, can impact the proper functioning of the Mined Geologic Disposal System (MGDS) waste package; the waste package has been identified as an MGDS Q-List item important to safety and waste isolation (pp. 4, 15, Reference 5.1). The waste package is on the Q-List by direct inclusion by the Department of Energy (DOE), without conducting a QAP-2-3 evaluation. The Waste Package Development Department (WPDD) responsible manager has evaluated this activity in accordance with QAP-2-0, *Conduct of Activities*. The *Perform Criticality, Thermal, Structural, and Shielding Analyses* (Reference 5.2) evaluation has determined the preparation and review of this design analysis is subject to *Quality Assurance Requirements and Description* (Reference 5.3) requirements. As specified in NLP-3-18, this activity is subject to QA controls.

The analysis described in this document supports development of the disposal criticality analysis methodology. No designs were analyzed in this document. This document will not directly support any construction, fabrication, or procurement activity and therefore is not required to be procedurally controlled as TBV (to be verified). The calculation design inputs or information used in this document come from data accepted by the Nuclear Regulatory Commission and by the scientific and engineering community as established fact. The specific references are listed in Section 5 and identified in Section 7. The information is therefore not treated as unqualified data

3. Method

The analytical model employed for this analysis was the SAS2H module of the SCALE sequence. Based upon fuel design, power history, and operating data for specific assemblies in the Yankee Rowe pressurized water reactor (PWR), a computational model was developed for use with the SAS2H module of SCALE. The SAS2H module is used to perform a fuel depletion analysis to predict the isotopic concentrations in localized areas of assembly pins (pellet samples) subsequent to irradiation and cooling time. The isotopic concentrations predicted by the SAS2H module are then compared with measured concentrations of the same localized areas (axial locations) of the assembly pins to determine the accuracy of the developed model. The measured isotopic concentrations used for comparisons in the analysis are obtained from a separate report (Reference 5.5).

4. Design Inputs

The sources for the design parameters are References 5.4 through 5.8. Reference 5.4 provides information on molar masses; the assembly design, power history and operating parameters are obtained from References 5.5 through 5.7; the cladding composition from References 5.8 and 5.9; and a list of trace elements in the fuel is derived from Reference 5.10.

4.1 Design Parameters

The molar masses of selected elements are obtained from Reference 5.4 and are provided below within three significant figures. Precision beyond three significant figures is not necessary since calculated isotopic concentrations from SCALE are only to three significant figures. Also, the weight per mole of enriched uranium is approximated by the weight per mole of natural uranium since the weight percent of enrichment is small.

Mole of natural uranium = 238 g,
 6.02×10^{23} atoms per mole. (Reference 5.4)

General spent fuel characteristics for each pellet sample are presented in Table 4-1 and include the initial ^{235}U enrichment, final burnup and the cooling time (Section 2.1.1, Reference 5.5). The initial enrichment for all samples is 3.40 wt% ^{235}U and the burnup ranges from 15.95 to 35.97 GWd/MTU. The cooling time for the sample E6-C-f6 at 138.94 cm is 717 days and for the other samples is 281.5 days. Reference 5.5 indicates that the measured isotopic concentrations for ^{241}Pu were back calculated to a zero cooling time.

Assembly design parameters are presented in Table 4-2 (Section 2.1.1, Reference 5.5; p. 2-1, Reference 5.6). The samples come from a special design, Westinghouse 17 x 18 assembly with an empty cell in the center for a flux wire thimble. A diagram of the cross section of the Yankee Rowe assembly is given in Figure 4-1. Since only 22 out of the 76 assemblies were equipped with the thimble, it is assumed that the thimble is not present. The assembly is in effect a square 18 x 18 lattice without 18 of its outer cell positions, which accommodates cruciform blades. In the Yankee Rowe core there are 76 square assemblies and 32 cruciform blades, of which 24 are Ag-In-Cd control blades and 8 are zircaloy shims.

It is assumed that the controls blades are not inserted during Cycles I, II or IV, since accurate information about the control blades composition and movement could not be obtained. However, the zircaloy shims occupied some of the outer ring of control blade positions during each cycle. Although the placement of the assembly during Cycle I is unknown, the placement during Cycles II and IV are in the center of the core, so that the effect of the zircaloy shims would not be significant. Therefore, it is assumed that samples from the assembly examined do not experience the effects of the zircaloy shims. Furthermore, Cycle IV contained 72 assemblies enriched to 4.1 wt.

% ^{235}U ; however, due to the limitations of the SAS2H module, it is assumed that all assemblies were enriched to 3.4 wt % ^{235}U (pp. 2-1 through 2-5, Reference 5.6).

The operating parameters in Table 4-3 include the uptime and downtime, cumulative burnups, specific powers, and average cycle boron concentrations (Table 2.1-2 and Appendix A, Reference 5.5). The temperatures of the fuel, cladding and moderator, and the moderator density are presented in Table 4-4 (Table 2.1-2, Reference 5.5). The moderator density is obtained from Appendix A of Reference 5.5 (pp. A-2 and A-3). Unfortunately, Reference 5.5 does not describe the operating data in sufficient detail to determine its accuracy. However, Reference 5.6 (pp. 2-7 through 2-9) provides diagrams of the power history and indicates that the assembly resided in the core during low power testing prior to Cycle I, which are not indicated by Reference 5.5. Although the information in Reference 5.6 is not in sufficient detail to allow accurate modeling, it does indicate that the operating data obtained from Reference 5.5 may have been simplified.

The composition of the cladding, stainless steel 348, is presented in Table 4-5, and has a density of 8.03 g/cm^3 (Table 8, p. 151, Reference 5.8; p. 46, Reference 5.9). However, SCALE 4.3 does not recognize the isotope ^{180}Ta , which is 0.012 wt % of natural tantalum. Since only one other isotope of tantalum exists and the weight percent of ^{181}Ta is small, tantalum is approximated as consisting of only ^{181}Ta . A list of trace elements in the fuel used in updating cross sections during the depletion analysis are presented in Table 4-6 and developed with consideration of elements used in Table 1 of Reference 5.10. A generic set of light element weights for PWRs that is typically used in depletion analyses is included in Table 4-7 (Table 17, Reference 5.7). Variations in light element masses per unit fuel in different PWRs are small when compared to this generic set (p. 2-2, Reference 5.9). This data is provided in units of kg/MTUO₂ or kg/MTU depending on the units required in the analysis.

Measured isotopic concentrations are presented in Table 4-8 and are given in g/MTU (Table 2.1-3, Reference 5.5). The measurements were performed as part of the Yankee Core Evaluation (EYC) Program, a three phase program that performed radiochemical analyses on fuel pellet samples. Samples analyzed in this report are from Phase 3, which examined samples from an assembly that was irradiated in Cycles I, II and IV. Note that the concentration of ^{241}Pu was back calculated to the time of discharge, with a cooling time of zero days (pp. 2-10, Reference 5.5).

Table 4-1. Spent Fuel Characteristic Parameters for Yankee Rowe PWR

Assembly and Rod Number	Axial Location from Bottom of Assembly, cm	Enrichment, wt % ²³⁵ U	Burnup, GWd/MTU	Cooling Time, days
E6-C-f6	220.22	3.400	15.95	281.5
E6-C-f6	138.94	3.400	30.39	717.0
E6-C-f6	57.66	3.400	31.33	281.5
E6-C-f6	17.02	3.400	20.19	281.5
E6-SE-c2	138.94	3.400	32.03	281.5
E6-SE-c2	57.66	3.400	31.41	281.5
E6-SE-e4	138.94	3.400	35.97	281.5
E6-SE-e4	57.66	3.400	35.26	281.5

Reference 5.5

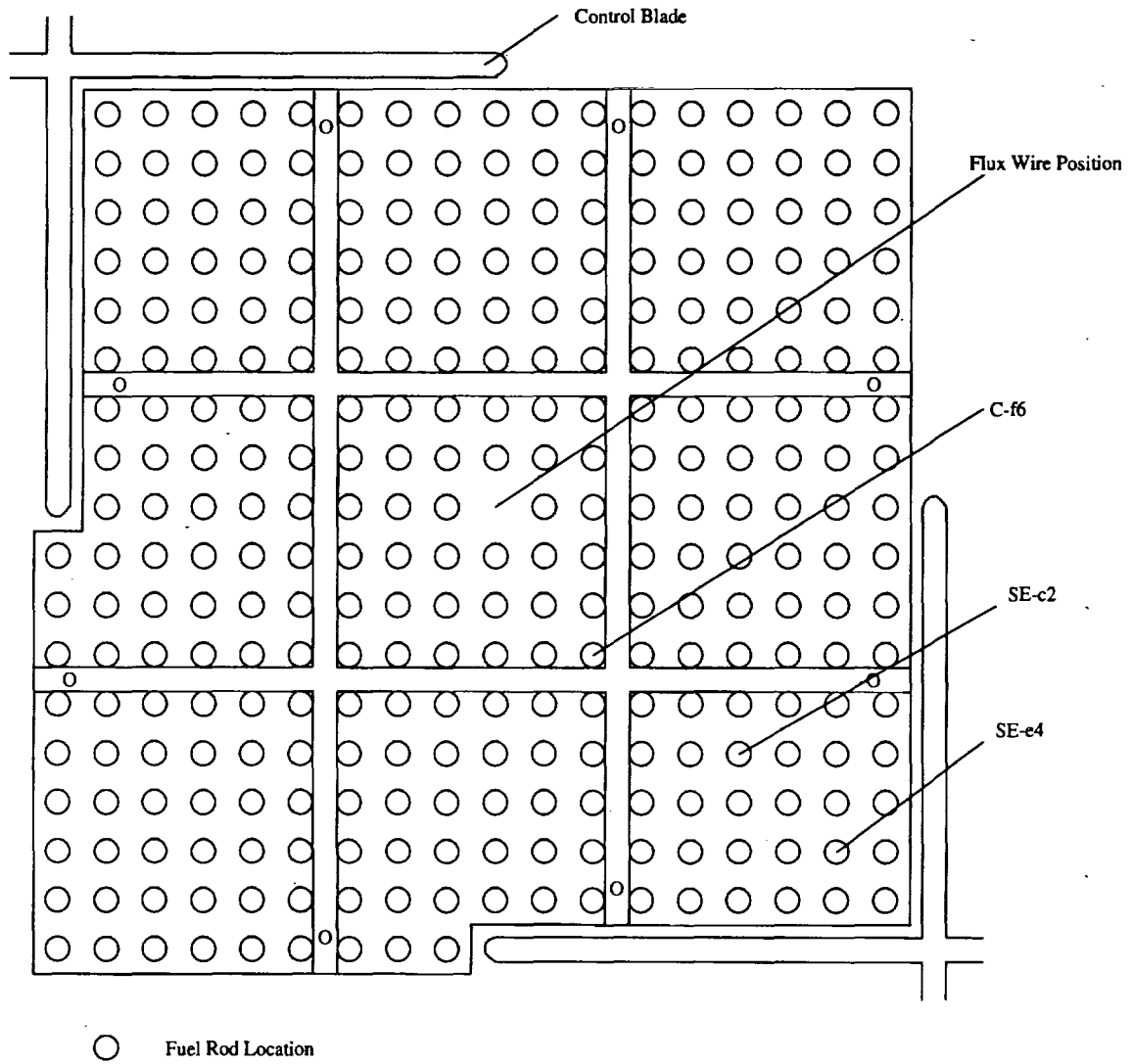
Table 4-2. Assembly Design Parameters for Yankee Rowe PWR

Parameter	Data
Core Data:	
Number of Rods per Core	23,142
Uranium Fuel Loading, kg U	20,908
Assembly General Data:	
Designer	Westinghouse
Type	17 x 18
Number of Fuel Rods	305
Number of Instrument Cells	1
Assembly Pitch, cm	19.46
Enrichment:	
wt % ²³⁴ U	0.020
wt % ²³⁵ U	3.400
wt % ²³⁶ U	0.020
wt % ²³⁸ U	96.56
Fuel Rod Data:	
Type of Fuel Pellet	UO ₂
Pellet Density, g/cm ³	10.18
Rod Pitch, cm	1.072
Rod Outside Diameter (OD), cm	0.864
Rod Inside Diameter (ID), cm	0.757
Pellet Diameter, cm	0.747
Active Fuel Length, cm	230.05 ^a
Clad Material	SS-348

^aThe active fuel length was given as 90.57 inches in Reference 5.6 and converted to cm by the following relation: 1 in. = 2.54 cm.

References 5.5 and 5.6

Figure 4-1. Cross Section of Yankee Rowe Assembly



Reference 5.5

Table 4-3. Operating Data for Yankee Rowe PWR

	Sample Identifier	Axial Location, cm	Cycle I	Cycle II	Cycle IV
Uptime, days	all	all	451.5	333.1	337.0
Downtime, days	all	all	129.0	370.0	See Table 4-1
Cumulative Burnup, GWd/MTU	E6-C-f6	220.22	5.90	10.23	15.95
	E6-C-f6	138.94	12.53	22.78	30.39
	E6-C-f6	57.66	13.29	23.54	31.33
	E6-C-f6	17.02	8.19	14.54	20.19
	E6-SE-c2	138.94	13.20	24.01	32.03
	E6-SE-c2	57.66	13.33	23.30	31.41
	E6-SE-e4	138.94	14.83	26.97	35.97
	E6-SE-e4	57.66	14.96	26.15	35.26
Specific Power, MW/MTU	E6-C-f6	220.22	13.07	13.00	16.97
	E6-C-f6	138.94	27.74	30.79	22.57
	E6-C-f6	57.66	29.44	29.86	24.01
	E6-C-f6	17.02	18.14	19.07	16.76
	E6-SE-c2	138.94	29.24	32.45	23.79
	E6-SE-c2	57.66	29.51	29.93	24.07
	E6-SE-e4	138.94	32.84	36.44	26.72
	E6-SE-e4	57.66	33.13	33.60	27.02
Boron Concentration, ppm	1 hour	all	0	0	835
	2022 hours	all	0	0	707
	2022 hours	all	0	0	337
	4044 hours	all	0	0	0

Reference 5.5

Table 4-4. Operating Temperatures for Yankee Rowe PWR

	Sample Identifier	Axial Location, cm	Cycle I	Cycle II	Cycle IV	Average H ₂ O Density, g/cm ³
Moderator Temperature, K	E6-C-f6	220.22	548	549	549	0.77017
	E6-C-f6	138.94	541	541	540	0.78338
	E6-C-f6	57.66	531	531	534	0.79733
	E6-C-f6	17.02	527	527	531	0.80256
	E6-SE-c2	138.94	541	541	540	0.78338
	E6-SE-c2	57.66	531	531	534	0.79733
	E6-SE-e4	138.94	541	541	540	0.78338
	E6-SE-e4	57.66	531	531	534	0.79733
Cladding Temperature, K	E6-C-f6	220.22	558	559	561	
	E6-C-f6	138.94	560	563	557	
	E6-C-f6	57.66	551	552	550	
	E6-C-f6	17.02	540	540	543	
	E6-SE-c2	138.94	560	563	557	
	E6-SE-c2	57.66	540	552	550	
	E6-SE-e4	138.94	560	563	557	
	E6-SE-e4	57.66	540	552	550	
Fuel Temperature, K	E6-C-f6	220.22	755	755	800	
	E6-C-f6	138.94	894	915	848	
	E6-C-f6	57.66	885	889	847	
	E6-C-f6	17.02	788	796	777	
	E6-SE-c2	138.94	894	915	848	
	E6-SE-c2	57.66	885	889	847	
	E6-SE-e4	138.94	894	915	848	
	E6-SE-e4	57.66	885	889	847	

Reference 5.5

Table 4-5. Composition of SS-348

Material	Weight Percent
C	0.08
Mn	2.00
P	0.045
S	0.030
Si	0.75
Cr	18.00
Ni	11.00
Cb	0.70
Ta	0.10
Co	0.20
Fe	67.095

References 5.8 and 5.9

Table 4-6. Nuclides Updated in SAS2H

⁸³ Kr	⁸⁵ Kr	⁸⁹ Y	⁹⁰ Sr	⁹⁵ Mo	⁹³ Zr
⁹⁴ Zr	⁹⁴ Nb	⁹⁵ Zr	⁹⁹ Tc	¹⁰¹ Ru	¹⁰³ Rh
¹⁰⁵ Rh	¹⁰⁶ Ru	¹⁰⁵ Pd	¹⁰⁸ Pd	¹⁰⁹ Ag	¹²⁴ Sb
¹³¹ Xe	¹³² Xe	¹³⁴ Cs	¹³⁵ Xe	¹³⁵ Cs	¹³⁶ Xe
¹³⁶ Ba	¹³⁷ Cs	¹³⁹ La	¹⁴¹ Pr	¹⁴³ Pr	¹⁴³ Nd
¹⁴⁴ Ce	¹⁴⁵ Nd	¹⁴⁷ Nd	¹⁴⁷ Pm	¹⁴⁷ Sm	¹⁴⁸ Pm
¹⁴⁹ Sm	¹⁵⁰ Sm	¹⁵¹ Sm	¹⁵² Sm	¹⁵³ Eu	¹⁵⁴ Eu
¹⁵⁵ Gd	¹⁵⁵ Eu				

Reference 5.10

Table 4-7. Light Element Mass per Unit of Fuel for a Typical PWR

Element	kg/MTU
O	135.0
Cr	5.9
Mn	0.33
Fe	13.0
Co	0.075
Ni	9.9
Zr	221.0
Nb	0.71
Sn	3.6

Reference 5.7

Table 4-8. Measured Isotopic Concentrations (g/MTU)

Sample	E6-C-f6	E6-C-f6	E6-C-f6	E6-C-f6	E6-SE-c2	E6-SE-c2	E6-SE-e4	E6-SE-e4
Location, cm	220.22	138.94	57.66	17.02	138.94	57.66	138.94	57.66
Burnup, Gwd/MTU	15.95	30.39	31.33	20.19	32.03	31.41	35.97	35.26
²³⁴ U	155	142	119	144	114	115	118	120
²³⁵ U	19800	12600	11900	17200	11800	11900	9780	9840
²³⁶ U	2880	4080	4150	3300	4180	4090	4450	4440
²³⁸ U	949000	937000	935000	936000	935000	936000	933000	934000
²³⁸ Pu	47.3	176	214	79.1	222	211	247	240
²³⁹ Pu	5950	7870	8010	6600	7980	7680	6950	6820
²⁴⁰ Pu	1120	2120	2260	1440	2370	2270	2570	2480
²⁴¹ Pu	663	1540	1640	915	1670	1580	1680	1620
²⁴² Pu	80.3	346	398	145	422	400	552	529

Reference 5.5

4.2 Criteria

The design of the waste package will depend on waste package configuration criticality analyses performed using an acceptable disposal criticality analysis methodology. Criteria that relate to the development and design of repository and engineered barrier components are derived from the applicable requirements and planning documents. The Engineered Barrier Design Requirements Document (EBDRD, Reference 5.13) provides requirements for engineered barrier segment design. The Repository Design Requirements Document (RDRD, Reference 5.14) provides requirements for repository design. The Controlled Design Assumptions Document (Reference 5.15) provides guidance for requirements listed in the EBDRD and RDRD which have unqualified or unconfirmed data associated with the requirement.

This analysis supports the disposal criticality analysis methodology by providing input, in the form of fuel depletion results, to benchmark calculations which address the prediction of both spent fuel isotopic compositions and their associated reactivity. These benchmark calculations will contribute to the determination of bias values in the method of critical multiplication factor calculation that is implemented by the analytic tools to be used in the disposal criticality methodology. The requirements for utilizing the bias in the method of calculation of the critical multiplication factor for disposal configurations containing spent nuclear fuel are located in Section 3.2.2.5 of the RDRD and Section 3.2.2.6 of the EBDRD. This analysis does not satisfy these requirements, but the results from this analysis will be used as input to subsequent analyses which will satisfy these requirements.

4.3 Assumptions

- 4.3.1 It is assumed that the flux wire thimble was not present in the empty unit cell. The basis for this assumption is that there were only 22 out of 76 assemblies equipped with a thimble and data could not be obtained on the dimensions and composition of the thimble. Therefore, the probability of the assembly containing the thimble is low and the thimble dimensions and compositions would have had to be assumed. This assumption is used throughout Section 7.
- 4.3.2 It is assumed that effects from the zircaloy shims are negligible. The basis for this assumption is that during Cycles II and IV the assembly was loaded in the center of the core and the zircaloy shims were located in the outer ring of the cruciform positions, so that effects of the zircaloy shims would not be experienced by the assembly during these cycles. However, it is not known where the assembly resided during Cycle I, which could have been next to a zircaloy shim. This assumption is used throughout Section 7.

4.4 Codes and Standards

There are no applicable codes or standards for this design analysis.

5. References

- 5.1 *Yucca Mountain Site Characterization Project Q-List*, YMP/90-55Q REV 4, Yucca Mountain Site Characterization Project.
- 5.2 *QAP-2-0 Activity Evaluations: ID #WP-20, Perform Criticality, Thermal, Structural, and Shielding Analyses*, Civilian Radioactive Waste Management System (CRWMS) Management and Operating Contractor (M&O), August 3, 1997.
- 5.3 *Quality Assurance Requirements and Description*, DOE/RW-0333P REV 7, U.S. Department of Energy (DOE) Office of Civilian Radioactive Waste Management (OCRWM).
- 5.4 *Nuclides and Isotopes*, General Electric Company, 14ed., 1989.
- 5.5 *Isotopic and Criticality Validation for PWR-Actinide Only Burnup Credit*, DOE/RW-0497, DOE OCRWM.
- 5.6 *Supplementary Report on Evaluation of Mass Spectrometric and Radiochemical Analyses of Yankee Core 1 Spent Fuel, Including Isotopes of Elements Thorium Through Curium*, WCAP-6086, Westinghouse Electric Corporation.
- 5.7 *Validation of the Scale System for PWR Spent Fuel Isotopic Composition Analyses*, ORNL/TM-12667, Oak Ridge National Laboratory, March 1995.
- 5.8 *Standard Specification for Heat-Resisting Chromium and Chromium-Nickel Stainless Steel Plate, Sheet, and Strip for Pressure Vessels*, ASTM Designation: A240-91a.
- 5.9 C. F. Lewis, *Materials Engineering: Materials Selector 1991*, Penton Publishers, Cleveland, OH, December 1990.
- 5.10 *SCALE-4 Analysis of Pressurized Water Reactor Critical Configurations: Volume 2- Sequoyah Unit 2 Cycle 3*, ORNL/TM-12294/V2, March 1995.
- 5.11 *SCALE 4.3, A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation for Workstations and Personal Computers*, NUREG/CR-0200 REV 5, ORNL/NUREG/CSD-2/R5, Volumes 1-3, Oak Ridge National Laboratory.
- 5.12 *Software Qualification Report for the SCALE Modular Code System*, Document Identifier Number: 30011-2002 REV 01, CRWMS M&O.

- 5.13 *Engineered Barrier Design Requirements Document*, YMP/CM-0024, REV 00, ICN 01, DOE OCRWM.
- 5.14 *Repository Design Requirements Document*, YMP/CM-0023, REV 00, ICN 01, DOE OCRWM.
- 5.15 *Controlled Design Assumptions Document*, DI#: B00000000-01717-4600-00032 REV 04, ICN 01, CRWMS M&O.

6. Use of Computer Software

- A.** Reference 5.11 describes the SAS2H module of SCALE 4.3 that is used with the 44GROUPNDF5 cross section library to calculate the isotopic concentrations for the specified burnup and cooling time. The computer code's spatially independent point depletion model is appropriate for comparison with pellet sample measurements, and is used within the range of validation, as described in Reference 5.12, in accordance with the QAP-SI series procedures. SCALE is obtained from the Software Configuration Management in accordance with appropriate procedures. SCALE's CSCI number is 30011 V4.3 and is installed on the WPDD HP 9000, 700 Workstation with CRWMS M&O tag number 110433.

- B.** *Lotus 1-2-3* Release 5 for Windows 95 is an Acquired Software spreadsheet program as defined in QAP-SI-0. User defined formulas and/or algorithms, inputs and results, are documented in the appropriate sections.

7. Design Analysis

The SAS2H module of SCALE 4.3 is used to perform one-dimensional (1-D) neutron transport and point depletion analyses on the Yankee Rowe assemblies using the preferred 44GROUPNDF5 cross-section library. To properly model the neutron flux spectrum and the nuclide composition changes, it is necessary to define the compositions, temperatures, and geometry of the fuel assembly. This is accomplished with the use of data blocks in which similar parameters are grouped together.

7.1 SCALE Input Data Blocks 1, 2, and 3

Data blocks 1 through 3 define the SCALE module to be used, the title of the input file, the cross section library to be used, and the lattice type to be modeled. The module used is SAS2H and the cross sectional library is 44GROUPNDF5, abbreviated as 44GROUP. The 44GROUP cross section library is recommended by Oak Ridge National Laboratory. Since SAS2H is only to be used for isotopic depletion/generation, the 'parm=skipshipdata' option is used so that a shipping cask shielding analysis is not performed. The title is arbitrary and should contain information that is sample specific, while the lattice type is "latticecell" to reflect the array characteristic of the assembly.

7.2 SCALE Input Data Block 4

Data block 4 defines the material compositions present in the assembly. A unique mixture number is assigned to each composition, and follows the form of mixture 1 for fuel, mixture 2 for cladding and mixture 3 for moderator.

The fuel mixture is specified as UO_2 with isotopic weight percentages from Table 4-2. The stack density is calculated from the fuel dimensions and the initial uranium fuel loading, with the following equation:

$$StackDensity = \frac{ULoad}{(NFR)\left(\frac{\pi}{4}\right)(PDia.)^2(FuelLength)} \left(\frac{1000gU}{1kgU}\right)\left(\frac{270gUO_2}{238gU}\right) \quad \text{Equation 7-1}$$

Where:

StackDensity = Fuel Stack Density (gUO_2/cm^3)

ULoad = Initial Uranium Fuel Loading of the Entire Core ($kgUO_2$)

NFR = Number of Fuel Rods in the Entire Core

PDia. = Fuel Pellet Diameter (cm)

FuelLength = Active Fuel Length (cm)

The resulting stack density is $10.17 gUO_2/cm^3$, compared to the pellet density of $10.18 gUO_2/cm^3$. Therefore, it is believed that the pellet density reported in Table 4-2 is the stack density, with the

difference being a result of rounding, and is used for mixture 1. Fuel temperatures for the samples during each cycle are presented in Table 4-4 and the temperature during Cycle I is input for the fuel temperature specification in data block 4. The other cycle fuel temperatures are input in data block 9. Isotopes which are selected as needing their cross sections updated during the depletion analysis are included in the fuel mixture. A standard list of trace fuel elements is given in Table 4-6 and defined in the fuel mixture to have a concentration of 10^{-20} atoms/barn·cm.

The cladding material is stainless steel 348 with a material composition given in Table 4-5 and a temperature derived from Table 4-4 by averaging the cladding temperature over the three cycles. The cladding temperatures used for each sample are presented in Table 7-1.

The moderator temperature, density and boron concentration are given in Tables 4-3 and 4-4. The moderator is composed of H₂O and boron. The moderator temperature is determined by averaging the temperature over the three cycles and is presented in Table 7-1. The boron is defined as an arbitrary material with the moderator density and temperature, a volume fraction equal to a cycle average boron concentration of 1 ppm, and a standard boron composition from the Standard Composition Library designated as 5000. A boron concentration of 1 ppm is used to approximate a zero boron concentration so that a boron concentration may be specified for Cycle IV in data block 9, Section 7.5. Included in Table 7-1 is the value of the average boron concentration for Cycle IV, which is calculated by maintaining the cumulative boron concentration over time, as specified in Table 4-3.

Table 7-1. Average Cladding and Moderator Temperatures

Sample	Location	Cladding Temperature, K	Moderator Temperature, K	Cycle IV Boron Concentration, ppm
E6-C-f6	220.22	559	549	261
E6-C-f6	138.94	560	541	261
E6-C-f6	57.66	551	532	261
E6-C-f6	17.02	541	528	261
E6-SE-c2	138.94	560	541	261
E6-SE-c2	57.66	547	532	261
E6-SE-e4	138.94	560	541	261
E6-SE-e4	57.66	547	532	261

7.3 SCALE Input Data Blocks 5 Through 7

The unit fuel rod cell geometry is defined in data block 5. The 'squarepitch' designation for the type of lattice is appropriate since the fuel assembly consists of a square array of fuel rods. Fuel rod, cladding and pitch dimensions are given in Table 4-2 with the mixture number for each composition defined in Section 7.2. The gap mixture is defined as 0.

Data block 6 allows the user to specify such parameters as the spatial mesh, angular quadrature and the convergence criteria. It is determined that the default values are sufficient and such options are not used in this design model.

In data block 7 the user defines general assembly data and determines the level of detail in which the assembly is to be modeled. The number of fuel rods per assembly is given in Table 4-2 and the length is calculated so that an assembly contains 1 MTU, using the following equation:

$$Length = \frac{1}{\frac{\pi}{4}(POD)^2(PDen)(NFR)} * \frac{270gUO_2}{238gU} * \frac{10^6gU}{1MTU} \quad \text{Equation 7-2}$$

Where:

- Length = Length Required for an Assembly to Contain 1 MTU (cm)
- POD = Fuel Pellet Diameter (cm)
- PDen = Fuel Pellet Density (gUO₂/cm³)
- NFR = Number of Fuel Rods

Since measured isotopic concentrations are presented in grams of isotope per Metric Ton of Uranium (MTU) and SCALE presents concentrations in grams of isotope per assembly, it is possible to alter the length so that the assembly contains 1 MTU. This is possible since the 1-D transport calculation is axially independent. Consequently, the length of the assembly does not impact the neutron flux spectrum nor the nuclide cross sections. The resulting length for the Yankee Rowe assembly is 833.69 cm.

The assembly was irradiated for three cycles. It is determined that approximately 80 days per cross section library is sufficient to accurately model the change in nuclide cross sections with increasing burnup, without over-burdening the SAS2H code. Therefore, the number of libraries per cycle are specified as five. To obtain the concentrations of all interested nuclides, a print level of 5 is chosen, while an input level of 2 is defined so that a Path B model may be utilized. The number of light elements is nine and is determined from Table 4-7, while the number of zones is three which is determined by the Path B model described in Section 7.4.

7.4 SCALE Input Data Block 8

The Path B model for Yankee Rowe centralizes the empty cell in the center of the assembly, which is surrounded by the homogenized fuel and moderator mixture, and finally, the moderator between assemblies. It is noted that if information concerning the control blade insertion could have been obtained, then the Path B model would incorporate structure to properly model control blade insertion histories. The equations below are used to determine the number of fuel unit cells that surround the empty unit cell, by conserving the fuel to moderator volume ratio. All of the following equations used to calculate the Path B model dimensions are derived. The results of the fuel-unit-cell calculations are presented in Table 7-2, and the resulting Path B model dimensions are presented in Table 7-3.

$$x = \frac{\left(\frac{F}{M}\right)(CUCMV)}{(FV) - \left(\frac{F}{M}\right)(MV)} \quad \text{Equation 7-3}$$

$$\frac{F}{M} = \frac{(NFR)\left(\frac{\pi}{4}\right)(POD)^2}{(NFR)[RP^2 - \left(\frac{\pi}{4}\right)(COD)^2] + [RP^2]} \quad \text{Equation 7-4}$$

$$CUCMV = RP^2 \quad \text{Equation 7-5}$$

$$FV = \left(\frac{\pi}{4}\right)(POD)^2 \quad \text{Equation 7-6}$$

$$MV = RP^2 - \left(\frac{\pi}{4}\right)(COD)^2 \quad \text{Equation 7-7}$$

Where:

x = Number of Unit Fuel Cells per Empty Unit Cell

F/M = Fuel to Moderator Volume Ratio

NFR = Number of Fuel Rods

POD = Fuel Pellet Outer Diameter

RP = Rod Pitch

COD = Cladding Outer Diameter

CUCMV = Central Unit Cell Moderator Volume

FV = Fuel Volume of One Fuel Unit Cell

MV = Moderator Volume of One Fuel Unit Cell

Once the number of fuel cells per empty unit cell is determined, the geometry of the Path B model is calculated. Since the empty unit cell is centralized, the dimensions of the radius for the moderator in the empty unit cell is calculated with the following equation:

$$R_1 = \sqrt{\left(\frac{1}{\pi}\right)RP^2} \quad \text{Equation 7-8}$$

Where:

R_1 = Radius of Central Moderator Zone

The area of an annular region is calculated by the difference between the outer circular area and the inner circular area. Equation 7-9 is the basis for the Equations 7-10 and 7-11 which determine the radii of the homogenized fuel zone and the outer moderator zone.

$$ARA = \pi(ORAR^2 - IRAR^2) \quad \text{Equation 7-9}$$

Where:

ARA = Annular Region Area

ORAR = Outer Radius of Annular Region

IRAR = Inner Radius of Annular Region

The area of the homogenized fuel zone surrounding the guide tube unit cell is equal to the number of fuel unit cells surrounding the guide tube multiplied by the area of a fuel unit cell. Consequently, the radius of the homogenized fuel zone is computed with the following equation:

$$R_2 = \sqrt{\left(\frac{x}{\pi}\right)RP^2 + R_1^2} \quad \text{Equation 7-10}$$

Where:

R_2 = Radius of Homogenized Fuel and Moderator Zone

The mixture number of the homogenized fuel and moderator mixture must be specified as 500. The code then determines the composition of the region based upon the dimensions and mixtures specified in the fuel unit cell data block 5.

The moderator in the channel between assemblies is determined by calculating the total moderator volume and multiplying by the fraction of unit cells in the larger unit cell of the Path B model. The total moderator volume between assemblies is determined by the assembly pitch and the fuel cell pitch multiplied by the number of unit cells. The radius of the moderator between assemblies is calculated from the following equation:

$$R_3 = \sqrt{\frac{(x+1)}{\pi * N_{Cell}} [AP^2 - (N_{Cell})(RP^2)] + R_2^2} \quad \text{Equation 7-11}$$

Where:

R₃ = Radius of Moderator Surrounding Assembly Zone

NCell = Number of Cells in Assembly

AP = Assembly Pitch

Table 7-2. Calculation of Fuel Unit Cell per Guide Tube Unit Cell

F/M	CUCMV, cm ²	FV, cm ²	MV, cm ²	x
0.7734	1.1492	0.4383	0.5629	305

Table 7-3. Path B Model Dimensions

	R ₁	R ₂	R ₃
Radius, cm	0.6048	10.5799	10.9791
Composition	Moderator	Fuel/Moderator	Moderator

7.5 SCALE Input Data Blocks 9 Through 16

Data block 9 is used to describe the power history of the reactor. The specific power, fuel irradiation period, the length of downtime, the fraction of boron and moderator density, and the temperature during the cycle may all be defined. The specific power is in units of MW/MTU while the irradiation period and length of downtime are both defined in days and are given in Table 4-3. The moderator density is assumed constant for all cycles and the boron fraction is determined by dividing the cycle average boron concentration found in Table 7-1 by the boron concentration specified in data block 4, Section 7.2. The individual cycle temperatures are given in Table 4-4. The boron fraction is specified with the command 'bfrac=' and the temperature with 'temkcyc='.

Light elements and their effective weight, in kg per assembly, are entered in data block 10. Table 4-7 provides a generic set of light elements from a typical PWR and their weights, in kg per MTU. Since the fuel length is altered so that there is 1 MTU per assembly the use of light elements with weights of kg per MTU is appropriate.

Data blocks 11 through 15 describe parameters used in the radial shielding analysis of a shipping cask and are not necessary in performing the depletion analyses. Data block 16 denotes the end of the SCALE input.

7.6 Comparison of Calculated and Measured Concentrations

Comparisons of corresponding calculated and measured concentrations are performed on a percent difference basis. The difference between the measured and the calculated value is divided by the measured value to determine the accuracy of the SAS2H calculation. A positive percent difference represents an over-prediction by the code, while a negative percent difference represents an under-prediction by the code. The measured concentrations are given in Table 4-8, calculated concentrations are presented in Table 7-4 and the percent differences are presented in Table 7-5. Isotopic concentrations of ^{241}Pu are obtained for a zero cooling time since the measured ^{241}Pu concentrations were back calculated to that time.

7.7 Results

SAS2H predicted isotopic concentrations are presented in Table 7-4. The calculated concentrations are obtained through the methodology described in Sections 7.1 through 7.5, and with the input parameters defined in Section 4.1. Calculated concentrations are compared with measured concentrations as described in Section 7.6 to determine the accuracy of the SAS2H code. Results of the comparison, in the form of percent differences, are presented in Table 7-5.

Table 7-4. Calculated Isotopic Concentrations (g/MTU)

Sample	E6-C-f6	E6-C-f6	E6-C-f6	E6-C-f6	E6-SE-c2	E6-SE-c2	E6-SE-e4	E6-SE-e4
Location, cm	220.22	138.94	57.66	17.02	138.94	57.66	138.94	57.66
Burnup, GWd/MTU	15.95	30.39	31.33	20.19	32.03	31.41	35.97	35.26
^{234}U	1.54E2	1.25E2	1.22E2	1.45E2	1.20E2	1.22E2	1.13E2	1.14E2
^{235}U	1.98E4	1.23E4	1.18E4	1.71E4	1.16E4	1.18E4	1.02E4	1.03E4
^{236}U	2.85E3	4.07E3	4.13E3	3.29E3	4.17E3	4.13E3	4.36E3	4.33E3
^{238}U	9.53E5	9.40E5	9.40E5	9.50E5	9.39E5	9.40E5	9.35E5	9.36E5
^{238}Pu	3.84E1	1.79E2	1.85E2	6.66E1	1.97E2	1.86E2	2.51E2	2.38E2
^{239}Pu	5.36E3	6.57E3	6.52E3	5.67E3	6.66E3	6.52E3	6.87E3	6.71E3
^{240}Pu	1.18E3	2.36E3	2.41E3	1.55E3	2.46E3	2.42E3	2.70E3	2.65E3
^{241}Pu	6.24E2	1.53E3	1.56E3	8.81E2	1.62E3	1.56E3	1.82E3	1.76E3
^{242}Pu	8.37E1	4.27E2	4.53E2	1.60E2	4.77E2	4.55E2	6.04E2	5.78E2

Table 7-5. Percent Difference Between Measured and Calculated [(C/M-1)*100]

Sample	E6-C-f6	E6-C-f6	E6-C-f6	E6-C-f6	E6-SE-c2	E6-SE-c2	E6-SE-e4	E6-SE-e4
Location, cm	220.22	138.94	57.66	17.02	138.94	57.66	138.94	57.66
Burnup, GWd/MTU	15.95	30.39	31.33	20.19	32.03	31.41	35.97	35.26
²³⁴ U	-0.65	-11.97	2.52	0.69	5.26	6.09	-4.24	-5.00
²³⁵ U	0.00	-2.38	-0.84	-0.58	-1.69	-0.84	4.29	4.67
²³⁶ U	-1.04	-0.25	-0.48	-0.30	-0.24	0.98	-2.02	-2.48
²³⁸ U	0.42	0.32	0.53	1.50	0.43	0.43	0.21	0.21
²³⁸ Pu	-18.82	1.70	-13.55	-15.80	-11.26	-11.85	1.62	-0.83
²³⁹ Pu	-9.92	-16.52	-18.60	-14.09	-16.54	-15.10	-1.15	-1.61
²⁴⁰ Pu	5.36	11.32	6.64	7.64	3.80	6.61	5.06	6.85
²⁴¹ Pu	-5.88	-0.65	-4.88	-3.72	-2.99	-1.27	8.33	8.64
²⁴² Pu	4.23	23.41	13.82	10.34	13.03	13.75	9.42	9.26

8. Conclusions

The accuracy in which the SAS2H module is able to predict isotopic concentrations is indicated by the percent differences presented in Table 7-5. Inspection of such results reveals that generally the isotopes of ^{238}Pu and ^{239}Pu are under-predicted, while the isotopes of ^{240}Pu and ^{242}Pu are over-predicted. Due to the lack of detail concerning the operation of Yankee Rowe Cycles I through IV, it is difficult to determine the causes for the under or over-prediction of such isotopes. Percent differences from this analysis are compared with results from Reference 5.5, in which similar calculations were performed with a previous version of SCALE and the 27burnplib cross section library. The concentrations calculated in Reference 5.5 for the most part agree with the concentrations calculated in this analysis; however, significant differences are seen for the plutonium isotopes. Since there are few differences between the model in Reference 5.5 and the model contained within, it is believed that the discrepancy between calculated concentrations for plutonium isotopes is caused by a change in the cross section library.

The SAS2H code normally predicts isotopic concentrations as a radial assembly average; however, measurements are performed on individual pellet samples. Therefore, local pellet conditions are modeled as closely as possible in this analysis so that a more realistic pellet composition can be determined. However, approximations made to obtain local pellet conditions will influence the calculated isotopic concentrations.

In general, the percent differences reveal that the SAS2H module of SCALE is adequate in predicting isotopic concentrations for Yankee Rowe assemblies, using the modeling methodology presented. The lack of detailed assembly design and operating data requires approximations that are believed to cause the inconsistencies between the calculated and measured concentrations. It is believed that improvements in the model for Yankee Rowe are possible with sample specific operating conditions, and detailed information concerning the cruciform control blades. More detailed operating data would be expected to improve the accuracy of the calculated concentrations in relation to the corresponding measurements. It is recommended that future analyses use more detailed data if possible.

9. Attachments

Attachment I includes eight pages and contains the input files used in the modeling of the Yankee Rowe samples. A description of the parameters contained within the input files is found in Sections 7.1 through 7.5.

Included in Attachment II is an extraction from each of the output files, containing the following information:

- echo of the SAS2H input deck,
- time/date stamp for when the SAS2H depletion calculation was performed,
- the output extraction of information pertinent to the Radiochemical Assay evaluations from the final ORIGEN calculation of the SAS2H depletion calculation.

ye6cf6h1.input

=sas2h parm=skipshipdata

Yankee Rowe sample E6-C-f6-1, 220.22 cm 15.95 gwd/MTU, July 97

' mixtures of fuel-pin-unit-cell:'
' 44group latticecell
'

uo2 1 den=10.18 1 755

92234 0.020 92235 3.40 92236 0.020 92238 96.56 end

kr-83 1 0 1-20 755 end

kr-85 1 0 1-20 755 end

y-89 1 0 1-20 755 end

sr-90 1 0 1-20 755 end

zr-93 1 0 1-20 755 end

zr-94 1 0 1-20 755 end

zr-95 1 0 1-20 755 end

nb-94 1 0 1-20 755 end

mo-95 1 0 1-20 755 end

tc-99 1 0 1-20 755 end

ru-101 1 0 1-20 755 end

ru-106 1 0 1-20 755 end

rh-103 1 0 1-20 755 end

rh-105 1 0 1-20 755 end

pd-105 1 0 1-20 755 end

pd-108 1 0 1-20 755 end

ag-109 1 0 1-20 755 end

sb-124 1 0 1-20 755 end

xe-131 1 0 1-20 755 end

xe-132 1 0 1-20 755 end

xe-135 1 0 1-20 755 end

xe-136 1 0 1-20 755 end

cs-134 1 0 1-20 755 end

cs-135 1 0 1-20 755 end

cs-137 1 0 1-20 755 end

ba-136 1 0 1-20 755 end

la-139 1 0 1-20 755 end

pr-141 1 0 1-20 755 end

pr-143 1 0 1-20 755 end

ce-144 1 0 1-20 755 end

nd-143 1 0 1-20 755 end

nd-145 1 0 1-20 755 end

nd-147 1 0 1-20 755 end

pm-147 1 0 1-20 755 end

pm-148 1 0 1-20 755 end

sm-147 1 0 1-20 755 end

sm-149 1 0 1-20 755 end

sm-150 1 0 1-20 755 end

sm-151 1 0 1-20 755 end

sm-152 1 0 1-20 755 end

eu-153 1 0 1-20 755 end

eu-154 1 0 1-20 755 end

eu-155 1 0 1-20 755 end

gd-155 1 0 1-20 755 end

arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045

16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7

73181 0.1 27059 0.2 26000 67.095 2 1 559 end

h2o 3 den=0.77017 1 549 end

arbm-bormod 0.77017 1 1 0 0 5000 100 3 1.0e-6 549 end

' 261 ppm boron (wt) in moderator for Core IV

' end comp-----
' fuel-pin-cell geometry:

squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end

' assembly and cycle parameters:

npin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5

printlevel=5 lightel=9 inplevel=2 numztotal=3 end

3 0.6048 500 10.5799 3 10.9791

power=13.07 burn=451.5 down=129 end

power=13.00 burn=333.1 down=370 end

power=16.97 burn=337 down=281.5 bfrac=261

temkcycc=800 end

o 135.0 cr 5.9 mn 0.33

fe 13.0 co 0.075 ni 9.9

zr 221.0 nb 0.71 sn 3.6

' end

ye6cf6h3.input

=sas2h parm=skipshipdata

Yankee Rowe sample E6-C-f6-3, 138.94 cm 30.39 gwd/MTU, July 97

' mixtures of fuel-pin-unit-cell:'
' 44group latticecell'
' uo2 1 den=10.18 1 894
' 92234 0.020 92235 3.40 92236 0.020 92238 96.56 end

' kr-83 1 0 1-20 894 end

' kr-85 1 0 1-20 894 end

' y-89 1 0 1-20 894 end

' sr-90 1 0 1-20 894 end

' zr-93 1 0 1-20 894 end

' zr-94 1 0 1-20 894 end

' zr-95 1 0 1-20 894 end

' nb-94 1 0 1-20 894 end

' mo-95 1 0 1-20 894 end

' tc-99 1 0 1-20 894 end

' ru-101 1 0 1-20 894 end

' ru-106 1 0 1-20 894 end

' rh-103 1 0 1-20 894 end

' rh-105 1 0 1-20 894 end

' pd-105 1 0 1-20 894 end

' pd-108 1 0 1-20 894 end

' ag-109 1 0 1-20 894 end

' sb-124 1 0 1-20 894 end

' xe-131 1 0 1-20 894 end

' xe-132 1 0 1-20 894 end

' xe-135 1 0 1-20 894 end

' xe-136 1 0 1-20 894 end

' cs-134 1 0 1-20 894 end

' cs-135 1 0 1-20 894 end

' cs-137 1 0 1-20 894 end

' ba-136 1 0 1-20 894 end

' la-139 1 0 1-20 894 end

' pr-141 1 0 1-20 894 end

' pr-143 1 0 1-20 894 end

' ce-144 1 0 1-20 894 end

' nd-143 1 0 1-20 894 end

' nd-145 1 0 1-20 894 end

' nd-147 1 0 1-20 894 end

' pm-147 1 0 1-20 894 end

' pm-148 1 0 1-20 894 end

' sm-147 1 0 1-20 894 end

' sm-149 1 0 1-20 894 end

' sm-150 1 0 1-20 894 end

' sm-151 1 0 1-20 894 end

' sm-152 1 0 1-20 894 end

' eu-153 1 0 1-20 894 end

' eu-154 1 0 1-20 894 end

' eu-155 1 0 1-20 894 end

' gd-155 1 0 1-20 894 end

' arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045

' 16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7

' 73181 0.1 27059 0.2 26000 67.095 2 1 560 end

' h2o 3 den=0.78338 1 541 end

' arbm-bormod 0.78338 1 1 0 0 5000 100 3 1.0e-6 541 end

' 261 ppm boron (wt) in moderator for Core IV

' end comp-----
' fuel-pin-cell geometry:

' squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end

' assembly and cycle parameters:

' npin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5

' printlevel=5 lightel=9 inplevel=2 numztotal=3 end

' 3 0.6048 500 10.5799 3 10.9791

' power=27.74 burn=451.5 down=129 end

' power=30.79 burn=333.1 down=370 temkcyc=915 end

' power=22.57 burn=337 down=717 bfrac=261 temkcyc=848

' end-

' o 135.0 cr 5.9 mn 0.33

' fe 13.0 co 0.075 ni 9.9

' zr 221.0 nb 0.71 sn 3.6

' end

ye6cf6h5.input

=sas2h parm=skipshipdata

Yankee Rowe sample E6-C-f6-5, 57.66 cm 31.33 gwd/MTU, July 97

```

-----
mixtures of fuel-pin-unit-cell:

```

```

44group latticecell

```

```

uo2 1 den=10.18 1 885
  92234 0.020 92235 3.40 92236 0.020 92238 96.56 end
kr-83 1 0 1-20 885 end
kr-85 1 0 1-20 885 end
y-89 1 0 1-20 885 end
sr-90 1 0 1-20 885 end
zr-93 1 0 1-20 885 end
zr-94 1 0 1-20 885 end
zr-95 1 0 1-20 885 end
nb-94 1 0 1-20 885 end
mo-95 1 0 1-20 885 end
tc-99 1 0 1-20 885 end
ru-101 1 0 1-20 885 end
ru-106 1 0 1-20 885 end
rh-103 1 0 1-20 885 end
rh-105 1 0 1-20 885 end
pd-105 1 0 1-20 885 end
pd-108 1 0 1-20 885 end
ag-109 1 0 1-20 885 end
sb-124 1 0 1-20 885 end
xe-131 1 0 1-20 885 end
xe-132 1 0 1-20 885 end
xe-135 1 0 1-20 885 end
xe-136 1 0 1-20 885 end
cs-134 1 0 1-20 885 end
cs-135 1 0 1-20 885 end
cs-137 1 0 1-20 885 end
ba-136 1 0 1-20 885 end
la-139 1 0 1-20 885 end
pr-141 1 0 1-20 885 end
pr-143 1 0 1-20 885 end
ce-144 1 0 1-20 885 end
nd-143 1 0 1-20 885 end
nd-145 1 0 1-20 885 end
nd-147 1 0 1-20 885 end
pm-147 1 0 1-20 885 end
pm-148 1 0 1-20 885 end
sm-147 1 0 1-20 885 end
sm-149 1 0 1-20 885 end
sm-150 1 0 1-20 885 end
sm-151 1 0 1-20 885 end
sm-152 1 0 1-20 885 end
eu-153 1 0 1-20 885 end
eu-154 1 0 1-20 885 end
eu-155 1 0 1-20 885 end
gd-155 1 0 1-20 885 end

```

```

arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
  16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
  73181 0.1 27059 0.2 26000 67.095 2 1 551 end

```

```

h2o 3 den=0.79733 1 532 end
arbm-bormod 0.79733 1 1 0 0 5000 100 3 1.0e-6 532 end

```

```

  261 ppm boron (wt) in moderator for the Core IV
-----

```

```

end comp

```

```

-----
fuel-pin-cell geometry:

```

```

squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end

```

```

-----
assembly and cycle parameters:

```

```

npin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=3 end
3 0.6048 500 10.5799 3 10.9791
power=29.44 burn=451.5 down=129 end
power=29.86 burn=333.1 down=370 temkcyc=889 end
power=24.01 burn=337 down=281.5 bfrac=261
temkcyc=847 end
  o 135.0 cr 5.9 mn 0.33
  fe 13.0 co 0.075 ni 9.9
  zr 221.0 nb 0.71 sn 3.6

```

```

-----
end

```

ye6cf6h6.input

=sas2h parm=skipshipdata
Yankee Rowe sample E6-C-f6-6, 17.02 cm 20.19 gwd/MTU, July 97

mixtures of fuel-pin-unit-cell:

44group latticecell

uo2 1 den=10.18 1 788
92234 0.020 92235 3.40 92236 0.020 92238 96.56 end

- kr-83 1 0 1-20 788 end
kr-85 1 0 1-20 788 end
y-89 1 0 1-20 788 end
sr-90 1 0 1-20 788 end
zr-93 1 0 1-20 788 end
zr-94 1 0 1-20 788 end
zr-95 1 0 1-20 788 end
nb-94 1 0 1-20 788 end
mo-95 1 0 1-20 788 end
tc-99 1 0 1-20 788 end
ru-101 1 0 1-20 788 end
ru-106 1 0 1-20 788 end
rh-103 1 0 1-20 788 end
rh-105 1 0 1-20 788 end
pd-105 1 0 1-20 788 end
pd-108 1 0 1-20 788 end
ag-109 1 0 1-20 788 end
sb-124 1 0 1-20 788 end
xe-131 1 0 1-20 788 end
xe-132 1 0 1-20 788 end
xe-135 1 0 1-20 788 end
xe-136 1 0 1-20 788 end
cs-134 1 0 1-20 788 end
cs-135 1 0 1-20 788 end
cs-137 1 0 1-20 788 end
ba-136 1 0 1-20 788 end
la-139 1 0 1-20 788 end
pr-141 1 0 1-20 788 end
pr-143 1 0 1-20 788 end
ce-144 1 0 1-20 788 end
nd-143 1 0 1-20 788 end
nd-145 1 0 1-20 788 end
nd-147 1 0 1-20 788 end
pm-147 1 0 1-20 788 end
pm-148 1 0 1-20 788 end
sm-147 1 0 1-20 788 end
sm-149 1 0 1-20 788 end
sm-150 1 0 1-20 788 end
sm-151 1 0 1-20 788 end
sm-152 1 0 1-20 788 end
eu-153 1 0 1-20 788 end
eu-154 1 0 1-20 788 end
eu-155 1 0 1-20 788 end
gd-155 1 0 1-20 788 end

arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
73181 0.1 27059 0.2 26000 67.095 2 1 541 end

h2o 3 den=0.80256 1 528 end
arbm-bormod 0.80256 1 1 0 0 5000 100 3 1.0e-6 528 end

261 ppm boron (wt) in moderator for the Core IV

end comp

fuel-pin-cell geometry:

squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end

assembly and cycle parameters:

npin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=3 end
3 0.6048 500 10.5799 3 10.9791
power=18.139 burn=451.5 down=129 end
power=19.070 burn=333.1 down=370 temkyc=796 end
power=16.755 burn=337 down=281.5 bfrac=261
temkyc=777 end
o 135.0 cr 5.9 mn 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

end

ye6sec2h3.input

=sas2h parm=skipshipdata
Yankee Rowe sample E6-SE-c2-3, 138.94 32.03 gwd/MTU, July 97

mixtures of fuel-pin-unit-cell:

44group latticecell

uo2 1 den=10.18 1 894
92234 0.020 92235 3.40 92236 0.020 92238 96.56 end
kr-83 1 0 1-20 894 end
kr-85 1 0 1-20 894 end
y-89 1 0 1-20 894 end
sr-90 1 0 1-20 894 end
zr-93 1 0 1-20 894 end
zr-94 1 0 1-20 894 end
zr-95 1 0 1-20 894 end
nb-94 1 0 1-20 894 end
mo-95 1 0 1-20 894 end
tc-99 1 0 1-20 894 end
ru-101 1 0 1-20 894 end
ru-106 1 0 1-20 894 end
rh-103 1 0 1-20 894 end
rh-105 1 0 1-20 894 end
pd-105 1 0 1-20 894 end
pd-108 1 0 1-20 894 end
ag-109 1 0 1-20 894 end
sb-124 1 0 1-20 894 end
xe-131 1 0 1-20 894 end
xe-132 1 0 1-20 894 end
xe-135 1 0 1-20 894 end
xe-136 1 0 1-20 894 end
cs-134 1 0 1-20 894 end
cs-135 1 0 1-20 894 end
cs-137 1 0 1-20 894 end
ba-136 1 0 1-20 894 end
la-139 1 0 1-20 894 end
pr-141 1 0 1-20 894 end
pr-143 1 0 1-20 894 end
ce-144 1 0 1-20 894 end
nd-143 1 0 1-20 894 end
nd-145 1 0 1-20 894 end
nd-147 1 0 1-20 894 end
pm-147 1 0 1-20 894 end
pm-148 1 0 1-20 894 end
sm-147 1 0 1-20 894 end
sm-149 1 0 1-20 894 end
sm-150 1 0 1-20 894 end
sm-151 1 0 1-20 894 end
sm-152 1 0 1-20 894 end
eu-153 1 0 1-20 894 end
eu-154 1 0 1-20 894 end
eu-155 1 0 1-20 894 end
gd-155 1 0 1-20 894 end

arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
73181 0.1 27059 0.2 26000 67.095 2 1 560 end

h2o 3 den=0.78338 1 541 end
arbm-bormod 0.78338 1 1 0 0 5000 100 3 1.0e-6 541 end

261 ppm boron (wt) in moderator for the Core IV

end comp

fuel-pin-cell geometry:

squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end

assembly and cycle parameters:

npin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=3 end
3 0.6048 500 10.5799 3 10.9791
power=29.24 burn=451.5 down=129 end
power=32.45 burn=333.1 down=370 temkcyc=915 end
power=23.79 burn=337 down=281.5 bfrac=261
temkcyc=848 end
o 135.0 cr 5.9 mn 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

end

ye6see4h3.input

=sas2h parm=skipshipdata

Yankee Rowe sample E6-SE-e4-3, 138.94 cm 30.39 gwd/MTU, July 97

mixtures of fuel-pin-unit-cell:

44group latticecell

uo2 1 den=10.18 1 894
92234 0.020 92235 3.40 92236 0.020 92238 96.56 end

kr-83 1 0 1-20 894 end

kr-85 1 0 1-20 894 end

y-89 1 0 1-20 894 end

sr-90 1 0 1-20 894 end

zr-93 1 0 1-20 894 end

zr-94 1 0 1-20 894 end

zr-95 1 0 1-20 894 end

nb-94 1 0 1-20 894 end

mo-95 1 0 1-20 894 end

tc-99 1 0 1-20 894 end

ru-101 1 0 1-20 894 end

ru-106 1 0 1-20 894 end

rh-103 1 0 1-20 894 end

rh-105 1 0 1-20 894 end

pd-105 1 0 1-20 894 end

pd-108 1 0 1-20 894 end

ag-109 1 0 1-20 894 end

sb-124 1 0 1-20 894 end

xe-131 1 0 1-20 894 end

xe-132 1 0 1-20 894 end

xe-135 1 0 1-20 894 end

xe-136 1 0 1-20 894 end

cs-134 1 0 1-20 894 end

cs-135 1 0 1-20 894 end

cs-137 1 0 1-20 894 end

ba-136 1 0 1-20 894 end

la-139 1 0 1-20 894 end

pr-141 1 0 1-20 894 end

pr-143 1 0 1-20 894 end

ce-144 1 0 1-20 894 end

nd-143 1 0 1-20 894 end

nd-145 1 0 1-20 894 end

nd-147 1 0 1-20 894 end

pm-147 1 0 1-20 894 end

pm-148 1 0 1-20 894 end

sm-147 1 0 1-20 894 end

sm-149 1 0 1-20 894 end

sm-150 1 0 1-20 894 end

sm-151 1 0 1-20 894 end

sm-152 1 0 1-20 894 end

eu-153 1 0 1-20 894 end

eu-154 1 0 1-20 894 end

eu-155 1 0 1-20 894 end

gd-155 1 0 1-20 894 end

arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
73181 0.1 27059 0.2 26000 67.095 2 1 560 end

h2o 3 den=0.78338 1 541 end

arbm-bormod 0.78338 1 1 0 0 5000 100 3 1.0e-6 541 end

261 ppm boron (wt) in moderator for Core IV

end comp

fuel-pin-cell geometry:

squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end

assembly and cycle parameters:

npin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5

printlevel=5 lightel=9 inplevel=2 numztotal=3 end

3 0.6048 500 10.5799 3 10.9791

power=32.84 burn=451.5 down=129 end

power=36.44 burn=333.1 down=370 temkyc=915 end

power=26.72 burn=337 down=281.5 bfrac=261

temkyc=848 end

o 135.0 cr 5.9 mn 0.33

fe 13.0 co 0.075 ni 9.9

zr 221.0 nb 0.71 sn 3.6

end

ye6see4h5.input

=sas2h parm=skipshipdata

Yankee Rowe sample E6-SE-e4-5, 57.66 cm 35.26 gwd/MTU, July 97

' mixtures of fuel-pin-unit-cell:

' Cross Section Library

' 44group latticecell

' Fuel Composition

```

uo2 1 den=10.18 1 885
  92234 0.020 92235 3.40 92236 0.020 92238 96.56 end
kr-83 1 0 1-20 885 end
kr-85 1 0 1-20 885 end
y-89 1 0 1-20 885 end
sr-90 1 0 1-20 885 end
zr-93 1 0 1-20 885 end
zr-94 1 0 1-20 885 end
zr-95 1 0 1-20 885 end
nb-94 1 0 1-20 885 end
mo-95 1 0 1-20 885 end
tc-99 1 0 1-20 885 end
ru-101 1 0 1-20 885 end
ru-106 1 0 1-20 885 end
rh-103 1 0 1-20 885 end
rh-105 1 0 1-20 885 end
pd-105 1 0 1-20 885 end
pd-108 1 0 1-20 885 end
ag-109 1 0 1-20 885 end
sb-124 1 0 1-20 885 end
xe-131 1 0 1-20 885 end
xe-132 1 0 1-20 885 end
xe-135 1 0 1-20 885 end
xe-136 1 0 1-20 885 end
cs-134 1 0 1-20 885 end
cs-135 1 0 1-20 885 end
cs-137 1 0 1-20 885 end
ba-136 1 0 1-20 885 end
la-139 1 0 1-20 885 end
pr-141 1 0 1-20 885 end
pr-143 1 0 1-20 885 end
ce-144 1 0 1-20 885 end
nd-143 1 0 1-20 885 end
nd-145 1 0 1-20 885 end
nd-147 1 0 1-20 885 end
pm-147 1 0 1-20 885 end
pm-148 1 0 1-20 885 end
sm-147 1 0 1-20 885 end
sm-149 1 0 1-20 885 end
sm-150 1 0 1-20 885 end
sm-151 1 0 1-20 885 end
sm-152 1 0 1-20 885 end
eu-153 1 0 1-20 885 end
eu-154 1 0 1-20 885 end
eu-155 1 0 1-20 885 end
gd-155 1 0 1-20 885 end

```

```

arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
  16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
  73181 0.1 27059 0.2 26000 67.095 2 1 547 end

```

```

h2o 3 den=0.79733 1 532 end
arbm-bormod 0.79733 1 1 0 0 5000 100 3 1.0e-6 532 end

```

' 261 ppm boron (wt) in moderator for the Core IV

end comp-----
fuel-pin-cell geometry:

squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end

assembly and cycle parameters:

```

npin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=3 end
3 0.6048 500 10.5799 3 10.9791
power=33.13 burn=451.5 down=129 end
power=33.60 burn=333.1 down=370 temkcyc=889 end
power=27.02 burn=337 down=281.5 bfrac=261
temkcyc=847 end
  o 135.0 cr 5.9 mn 0.33
  fe 13.0 co 0.075 ni 9.9
  zr 221.0 nb 0.71 sn 3.6

```

end

ye6cf6h1.sum

```

0.....
  |                                     |
  |          SCALE4.3  Bulletin Board   |
  |          -----                   |
  |          Welcome to SCALE-4.3.     |
  |                                     |
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
  Yankee Rowe sample E6-C-f6-1, 220.22 cm 15.95 gwd/MTU, July 97
  |
  |   mixtures of fuel-pin-unit-cell:
  |
  |   44group  latticecell
  |
  |   uo2  1 den=10.18  1  755
  |         92234 0.020 92235 3.40 92236 0.020 92238 96.56  end
  |   kr-83 1 0 1-20 755  end
  |   kr-85 1 0 1-20 755  end
  |   y-89  1 0 1-20 755  end
  |   sr-90 1 0 1-20 755  end
  |   zr-93 1 0 1-20 755  end
  |   zr-94 1 0 1-20 755  end
  |   zr-95 1 0 1-20 755  end
  |   nb-94 1 0 1-20 755  end
  |   mo-95 1 0 1-20 755  end
  |   tc-99 1 0 1-20 755  end
  |   ru-101 1 0 1-20 755  end
  |   ru-106 1 0 1-20 755  end
  |   rh-103 1 0 1-20 755  end
  |   rh-105 1 0 1-20 755  end
  |   pd-105 1 0 1-20 755  end
  |   pd-108 1 0 1-20 755  end
  |   ag-109 1 0 1-20 755  end
  |   sb-124 1 0 1-20 755  end
  |   xe-131 1 0 1-20 755  end
  |   xe-132 1 0 1-20 755  end
  |   xe-135 1 0 1-20 755  end
  |   xe-136 1 0 1-20 755  end
  |   cs-134 1 0 1-20 755  end
  |   cs-135 1 0 1-20 755  end
  |   cs-137 1 0 1-20 755  end
  |   ba-136 1 0 1-20 755  end
  |   la-139 1 0 1-20 755  end
  |   pr-141 1 0 1-20 755  end
  |   pr-143 1 0 1-20 755  end
  |   ce-144 1 0 1-20 755  end
  |   nd-143 1 0 1-20 755  end
  |   nd-145 1 0 1-20 755  end
  |   nd-147 1 0 1-20 755  end
  |   pm-147 1 0 1-20 755  end
  |   pm-148 1 0 1-20 755  end
  |   sm-147 1 0 1-20 755  end
  |   sm-149 1 0 1-20 755  end
  |   sm-150 1 0 1-20 755  end
  |   sm-151 1 0 1-20 755  end
  |   sm-152 1 0 1-20 755  end
  |   eu-153 1 0 1-20 755  end
  |   eu-154 1 0 1-20 755  end
  |   eu-155 1 0 1-20 755  end
  |   gd-155 1 0 1-20 755  end
  |
  |   arbm-ss348  8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
  |             16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
  |             73181 0.1 27059 0.2 26000 67.095 2 1 559  end
  |
  |   h2o  3 den=0.77017  1  549  end
  |   arbm-bormod 0.77017 1 1 0 0 5000 100 3 1.0e-6 549  end
  |
  |   261 ppm boron (wt) in moderator for Core IV
  |
  |   -----
  |   end comp
  |
  |   -----
  |
  |   fuel-pin-cell geometry:
  |
  |   squarepitch  1.072  0.747  1  3  0.864  2  0.757  0  end
  |
  |   -----
  |
  |   assembly and cycle parameters:
  |
  |   npin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5
  |   printlevel=5 lightel=9 implevel=2 numztotal=3  end
  |   3 0.6048 500 10.5799 3 10.9791
  |   power=13.07 burn=451.5 down=129  end
  |   power=13.00 burn=333.1 down=370  end
  |   power=16.97 burn=337 down=281.5 bfrac=261 tenkcyc=800  end
  |   o 135.0 cr 5.9 mm 0.33
  |   fe 13.0 co 0.075 ni 9.9
  |   zr 221.0 nb 0.71 sn 3.6
  |
  |   1  ssssssssss  aaaaaaaaaa  ssssssssss  2222222222  hh  hh
  |     ssssssssss  aaaaaaaaaa  ssssssssss  222222222222  hh  hh
  |     ss  ss  aa  aa  ss  ss  22  22  hh  hh
  |     ss  ss  aa  aa  ss  ss  22  22  hh  hh
  |     ss  ss  aa  aa  ss  ss  22  22  hh  hh
  |     ssssssssss  aaaaaaaaaa  ssssssssss  22  hhhhhhhhhhhh
  |     ssssssssss  aaaaaaaaaa  ssssssssss  22  hhhhhhhhhhhh
  |     ss  aa  aa  ss  22  hh  hh
  |     ss  aa  aa  ss  22  hh  hh
  |

```


ye6cf6h3.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  Yankee Rowe sample E6-C-f6-3, 138.94 cm 30.39 gwd/MTU, July 97

  mixtures of fuel-pin-unit-cell:

  44group latticecell

  uo2 1 den=10.18 1 894
    92234 0.020 92235 3.40 92236 0.020 92238 96.56 end
  kr-83 1 0 1-20 894 end
  kr-85 1 0 1-20 894 end
  y-89 1 0 1-20 894 end
  sr-90 1 0 1-20 894 end
  zr-93 1 0 1-20 894 end
  zr-94 1 0 1-20 894 end
  zr-95 1 0 1-20 894 end
  nb-94 1 0 1-20 894 end
  mo-95 1 0 1-20 894 end
  tc-99 1 0 1-20 894 end
  ru-101 1 0 1-20 894 end
  ru-106 1 0 1-20 894 end
  rh-103 1 0 1-20 894 end
  rh-105 1 0 1-20 894 end
  pd-105 1 0 1-20 894 end
  pd-108 1 0 1-20 894 end
  ag-109 1 0 1-20 894 end
  sb-124 1 0 1-20 894 end
  xe-131 1 0 1-20 894 end
  xe-132 1 0 1-20 894 end
  xe-135 1 0 1-20 894 end
  xe-136 1 0 1-20 894 end
  cs-134 1 0 1-20 894 end
  cs-135 1 0 1-20 894 end
  cs-137 1 0 1-20 894 end
  ba-136 1 0 1-20 894 end
  la-139 1 0 1-20 894 end
  pr-141 1 0 1-20 894 end
  pr-143 1 0 1-20 894 end
  ce-144 1 0 1-20 894 end
  nd-143 1 0 1-20 894 end
  nd-145 1 0 1-20 894 end
  nd-147 1 0 1-20 894 end
  pm-147 1 0 1-20 894 end
  pm-148 1 0 1-20 894 end
  sm-147 1 0 1-20 894 end
  sm-149 1 0 1-20 894 end
  sm-150 1 0 1-20 894 end
  sm-151 1 0 1-20 894 end
  sm-152 1 0 1-20 894 end
  eu-153 1 0 1-20 894 end
  eu-154 1 0 1-20 894 end
  eu-155 1 0 1-20 894 end
  gd-155 1 0 1-20 894 end

  arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
    16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
    73181 0.1 27059 0.2 26000 67.095 2 1 560 end

  h2o 3 den=0.78338 1 541 end
  arbm-bormod 0.78338 1 1 0 0 5000 100 3 1.0e-6 541 end

  261 ppm boron (wt) in moderator for Core IV
  -----
end comp

  fuel-pin-cell geometry:
squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end
  -----

  assembly and cycle parameters:
npin/asm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numztotal=3 end
3 0.6048 500 10.5799 3 10.9791
power=27.74 burn=451.5 down=129 end
power=30.79 burn=333.1 down=370 temkcyc=915 end
power=22.57 burn=337 down=717 bfrac=261 temkcyc=848 end
o 135.0 cr 5.9 mm 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

1 sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
ss ss aa aa ss ss 22 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh

```


ye6cf6h5.sum

```

0.....
*
*          SCALE4.3  Bulletin  Board
*          -----
*
*          Welcome to SCALE-4.3.
*
*.....
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
  Yankee Rowe sample E6-C-f6-5, 57.66 cm 31.33 gwd/MTU, July 97
  -----
  mixtures of fuel-pin-unit-cell:
  -----
  44group latticecell
  -----
  uo2 1 den=10.18 1 885
      92234 0.020 92235 3.40 92236 0.020 92238 96.56 end
  kr-83 1 0 1-20 885 end
  kr-85 1 0 1-20 885 end
  y-89 1 0 1-20 885 end
  sr-90 1 0 1-20 885 end
  zr-93 1 0 1-20 885 end
  zr-94 1 0 1-20 885 end
  zr-95 1 0 1-20 885 end
  nb-94 1 0 1-20 885 end
  mo-95 1 0 1-20 885 end
  tc-99 1 0 1-20 885 end
  ru-101 1 0 1-20 885 end
  ru-106 1 0 1-20 885 end
  rh-103 1 0 1-20 885 end
  rh-105 1 0 1-20 885 end
  pd-105 1 0 1-20 885 end
  pd-108 1 0 1-20 885 end
  ag-109 1 0 1-20 885 end
  sb-124 1 0 1-20 885 end
  xe-131 1 0 1-20 885 end
  xe-132 1 0 1-20 885 end
  xe-135 1 0 1-20 885 end
  xe-136 1 0 1-20 885 end
  cs-134 1 0 1-20 885 end
  cs-135 1 0 1-20 885 end
  cs-137 1 0 1-20 885 end
  ba-136 1 0 1-20 885 end
  la-139 1 0 1-20 885 end
  pr-141 1 0 1-20 885 end
  pr-143 1 0 1-20 885 end
  ce-144 1 0 1-20 885 end
  nd-143 1 0 1-20 885 end
  nd-145 1 0 1-20 885 end
  nd-147 1 0 1-20 885 end
  pm-147 1 0 1-20 885 end
  pm-148 1 0 1-20 885 end
  sm-147 1 0 1-20 885 end
  sm-149 1 0 1-20 885 end
  sm-150 1 0 1-20 885 end
  sm-151 1 0 1-20 885 end
  sm-152 1 0 1-20 885 end
  eu-153 1 0 1-20 885 end
  eu-154 1 0 1-20 885 end
  eu-155 1 0 1-20 885 end
  gd-155 1 0 1-20 885 end

  arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
             .16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
             73181 0.1 27059 0.2 26000 67.095 2 1 551 end

  h2o 3 den=0.79733 1 532 end
  arbm-bormod 0.79733 1 1 0 0 5000 100 3 1.0e-6 532 end
  -----
  261 ppm boron (wt) in moderator for the Core IV
  -----
  end comp
  -----
  fuel-pin-cell geometry:
  -----
  squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end
  -----
  assembly and cycle parameters:
  -----
  npin/assm=305 fuelnngth=833.69 ncycles=3 nlib/cyc=5
  printlevel=5 lightel=9 inplevel=2 numztotal=3 end
  3 0.6048 500 10.5799 3 10.9791
  power=29.44 burn=451.5 down=129 end
  power=29.86 burn=333.1 down=370 temkcycc=889 end
  power=24.01 burn=337 down=281.5 bfrac=261 temkcycc=847 end
  o 135.0 cr 5.9 mn 0.33
  fe 13.0 co 0.075 ni 9.9
  zr 221.0 nb 0.71 sn 3.6
  -----
  1  sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
  ss ss aa aa ss ss 22 22 hh hh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh

```


	initial	22.6 d	45.2 d	67.7 d	90.3 d	90.3 d
o 16	charge 8.41E+03	8.41E+03	8.41E+03	8.41E+03	8.41E+03	8.41E+03
mo 95	charge .00E+00	6.02E-05	4.11E-04	1.19E-03	2.43E-03	2.43E-03
tc 99	charge .00E+00	3.21E-12	3.31E-11	1.22E-10	3.02E-10	3.02E-10
totals	1.15E+04	1.15E+04	1.15E+04	1.15E+04	1.15E+04	1.15E+04
u233	charge .00E+00	3.04E-07	5.99E-07	8.78E-07	1.14E-06	1.14E-06
u234	8.55E-01	8.46E-01	8.37E-01	8.28E-01	8.19E-01	8.19E-01
u235	1.45E+02	1.41E+02	1.38E+02	1.35E+02	1.32E+02	1.32E+02
u236	8.47E-01	1.48E+00	2.10E+00	2.70E+00	3.28E+00	3.28E+00
u238	4.06E+03	4.05E+03	4.05E+03	4.05E+03	4.05E+03	4.05E+03
np237	.00E+00	8.24E-03	2.31E-02	4.07E-02	6.05E-02	6.05E-02
pu236	.00E+00	2.12E-10	1.30E-09	3.53E-09	7.05E-09	7.05E-09
pu238	.00E+00	4.58E-05	2.91E-04	8.03E-04	1.62E-03	1.62E-03
pu238	.00E+00	4.58E-05	2.91E-04	8.03E-04	1.62E-03	1.62E-03
pu239	.00E+00	1.51E+00	3.18E+00	4.73E+00	6.15E+00	6.16E+00
pu240	.00E+00	2.02E-02	8.32E-02	1.81E-01	3.06E-01	3.06E-01
pu241	.00E+00	7.20E-04	6.09E-03	2.00E-02	4.52E-02	4.52E-02
pu242	.00E+00	3.20E-06	5.59E-05	2.81E-04	8.57E-04	8.57E-04
am241	charge .00E+00	5.13E-07	8.79E-06	4.40E-05	1.34E-04	1.34E-04
am242m	.00E+00	7.88E-10	2.64E-08	1.91E-07	7.46E-07	7.46E-07
am243	.00E+00	1.06E-08	3.78E-07	2.89E-06	1.19E-05	1.19E-05
totals	4.20E+03	4.20E+03	4.20E+03	4.19E+03	4.19E+03	4.19E+03
decay data, including gamma and total energy, are from endf/b-vi						
1697 total number of nuclides in library						
nuclide concentrations, grams						
o 16	initial 1.35E+05	46.9 d 1.35E+05	93.8 d 1.35E+05	140.8 d 1.35E+05	187.7 d 1.35E+05	234.6 d 1.35E+05
mo 95	initial 1.71E+01	46.9 d 1.71E+01	93.8 d 1.84E+01	140.8 d 1.88E+01	187.7 d 1.90E+01	234.6 d 1.92E+01
tc 99	7.93E-05	46.9 d 8.01E-05	93.8 d 8.01E-05	140.8 d 8.01E-05	187.7 d 8.01E-05	234.6 d 8.01E-05
total	3.92E+05	46.9 d 3.92E+05	93.8 d 3.92E+05	140.8 d 3.92E+05	187.7 d 3.92E+05	234.6 d 3.92E+05
nuclide concentrations, grams						
u233	initial 1.83E-03	46.9 d 1.85E-03	93.8 d 1.87E-03	140.8 d 1.89E-03	187.7 d 1.91E-03	234.6 d 1.93E-03
u234	1.21E+02	46.9 d 1.21E+02	93.8 d 1.21E+02	140.8 d 1.21E+02	187.7 d 1.21E+02	234.6 d 1.22E+02
u235	1.18E+04	46.9 d 1.18E+04	93.8 d 1.18E+04	140.8 d 1.18E+04	187.7 d 1.18E+04	234.6 d 1.18E+04
u236	4.13E+03	46.9 d 4.13E+03	93.8 d 4.13E+03	140.8 d 4.13E+03	187.7 d 4.13E+03	234.6 d 4.13E+03
u238	9.40E+05	46.9 d 9.40E+05	93.8 d 9.40E+05	140.8 d 9.40E+05	187.7 d 9.40E+05	234.6 d 9.40E+05
np237	4.61E+02	46.9 d 4.68E+02	93.8 d 4.69E+02	140.8 d 4.69E+02	187.7 d 4.69E+02	234.6 d 4.69E+02
pu236	6.73E-04	46.9 d 6.55E-04	93.8 d 6.35E-04	140.8 d 6.16E-04	187.7 d 5.97E-04	234.6 d 5.79E-04
pu238	1.71E+02	46.9 d 1.76E+02	93.8 d 1.79E+02	140.8 d 1.81E+02	187.7 d 1.83E+02	234.6 d 1.84E+02
pu238	1.71E+02	46.9 d 1.76E+02	93.8 d 1.79E+02	140.8 d 1.81E+02	187.7 d 1.83E+02	234.6 d 1.84E+02
pu239	6.45E+03	46.9 d 6.52E+03	93.8 d 6.52E+03	140.8 d 6.52E+03	187.7 d 6.52E+03	234.6 d 6.52E+03
pu240	2.41E+03	46.9 d 2.41E+03	93.8 d 2.41E+03	140.8 d 2.41E+03	187.7 d 2.41E+03	234.6 d 2.41E+03
pu241	1.56E+03	46.9 d 1.55E+03	93.8 d 1.54E+03	140.8 d 1.53E+03	187.7 d 1.52E+03	234.6 d 1.51E+03
pu242	4.53E+02	46.9 d 4.53E+02	93.8 d 4.53E+02	140.8 d 4.53E+02	187.7 d 4.53E+02	234.6 d 4.53E+02
am241	8.58E+01	46.9 d 9.55E+01	93.8 d 1.05E+02	140.8 d 1.15E+02	187.7 d 1.24E+02	234.6 d 1.33E+02
am242m	2.41E+00	46.9 d 2.41E+00	93.8 d 2.41E+00	140.8 d 2.41E+00	187.7 d 2.41E+00	234.6 d 2.40E+00
am243	9.84E+01	46.9 d 9.85E+01	93.8 d 9.85E+01	140.8 d 9.85E+01	187.7 d 9.85E+01	234.6 d 9.85E+01
total	9.67E+05	46.9 d 9.67E+05	93.8 d 9.67E+05	140.8 d 9.67E+05	187.7 d 9.67E+05	234.6 d 9.67E+05
element concentrations, grams						
nuclide concentrations, grams						
mo 95	initial 6.42E+02	46.9 d 6.64E+02	93.8 d 6.81E+02	140.8 d 6.93E+02	187.7 d 7.01E+02	234.6 d 7.06E+02
tc 99	initial 7.49E+02	46.9 d 7.51E+02	93.8 d 7.51E+02	140.8 d 7.51E+02	187.7 d 7.51E+02	234.6 d 7.51E+02
ru101	7.24E+02	46.9 d 7.24E+02	93.8 d 7.24E+02	140.8 d 7.24E+02	187.7 d 7.24E+02	234.6 d 7.24E+02
rh103	4.37E+02	46.9 d 4.56E+02	93.8 d 4.64E+02	140.8 d 4.67E+02	187.7 d 4.69E+02	234.6 d 4.70E+02
rh103m	3.26E-02	46.9 d 1.42E-02	93.8 d 6.22E-03	140.8 d 2.72E-03	187.7 d 1.19E-03	234.6 d 5.18E-04
ag109	8.62E+01	46.9 d 8.64E+01	93.8 d 8.64E+01	140.8 d 8.64E+01	187.7 d 8.64E+01	234.6 d 8.64E+01
nuclide concentrations, grams						
nd143	initial 8.20E+02	46.9 d 8.34E+02	93.8 d 8.35E+02	140.8 d 8.35E+02	187.7 d 8.35E+02	234.6 d 8.35E+02
nd145	initial 6.37E+02	46.9 d 6.38E+02	93.8 d 6.38E+02	140.8 d 6.38E+02	187.7 d 6.38E+02	234.6 d 6.38E+02
sm147	1.06E+02	46.9 d 1.11E+02	93.8 d 1.16E+02	140.8 d 1.20E+02	187.7 d 1.25E+02	234.6 d 1.29E+02
sm149	4.37E+00	46.9 d 4.37E+00	93.8 d 4.37E+00	140.8 d 4.37E+00	187.7 d 4.37E+00	234.6 d 4.37E+00
sm150	2.81E+02	46.9 d 2.81E+02	93.8 d 2.81E+02	140.8 d 2.81E+02	187.7 d 2.81E+02	234.6 d 2.81E+02
sm151	2.33E+01	46.9 d 2.35E+01	93.8 d 2.35E+01	140.8 d 2.34E+01	187.7 d 2.34E+01	234.6 d 2.34E+01
eu151	4.76E-02	46.9 d 7.09E-02	93.8 d 9.41E-02	140.8 d 1.17E-01	187.7 d 1.40E-01	234.6 d 1.64E-01
sm152	1.18E+02	46.9 d 1.18E+02	93.8 d 1.18E+02	140.8 d 1.18E+02	187.7 d 1.18E+02	234.6 d 1.18E+02
eu153	1.09E+02	46.9 d 1.10E+02	93.8 d 1.10E+02	140.8 d 1.10E+02	187.7 d 1.10E+02	234.6 d 1.10E+02
gd155	1.00E-01	46.9 d 1.85E-01	93.8 d 2.68E-01	140.8 d 3.50E-01	187.7 d 4.30E-01	234.6 d 5.08E-01
total	3.20E+04	46.9 d 3.20E+04	93.8 d 3.20E+04	140.8 d 3.20E+04	187.7 d 3.20E+04	234.6 d 3.20E+04

ye6cf6h6.sum

```

0.....
|
|          SCALE4.3  Bulletin  Board
|          -----
|
|          Welcome to SCALE-4.3.
|
|.....

```

```

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  Yankee Rowe sample E6-C-f6-6, 17.02 cm 20.19 gwd/MTU, July 97

```

mixtures of fuel-pin-unit-cell:

44group latticecell

```

uo2 1 den=10.18 1 788
    92234 0.020 92235 3.40 92236 0.020 92238 96.56 end
kr-83 1 0 1-20 788 end
kr-85 1 0 1-20 788 end
y-89 1 0 1-20 788 end
sr-90 1 0 1-20 788 end
zr-93 1 0 1-20 788 end
zr-94 1 0 1-20 788 end
zr-95 1 0 1-20 788 end
nb-94 1 0 1-20 788 end
mo-95 1 0 1-20 788 end
tc-99 1 0 1-20 788 end
ru-101 1 0 1-20 788 end
ru-106 1 0 1-20 788 end
rh-103 1 0 1-20 788 end
rh-105 1 0 1-20 788 end
pd-105 1 0 1-20 788 end
pd-108 1 0 1-20 788 end
ag-109 1 0 1-20 788 end
sb-124 1 0 1-20 788 end
xe-131 1 0 1-20 788 end
xe-132 1 0 1-20 788 end
xe-135 1 0 1-20 788 end
xe-136 1 0 1-20 788 end
cs-134 1 0 1-20 788 end
cs-135 1 0 1-20 788 end
cs-137 1 0 1-20 788 end
ba-136 1 0 1-20 788 end
la-139 1 0 1-20 788 end
pr-141 1 0 1-20 788 end
pr-143 1 0 1-20 788 end
ce-144 1 0 1-20 788 end
nd-143 1 0 1-20 788 end
nd-145 1 0 1-20 788 end
nd-147 1 0 1-20 788 end
pm-147 1 0 1-20 788 end
pm-148 1 0 1-20 788 end
sm-147 1 0 1-20 788 end
sm-149 1 0 1-20 788 end
sm-150 1 0 1-20 788 end
sm-151 1 0 1-20 788 end
sm-152 1 0 1-20 788 end
eu-153 1 0 1-20 788 end
eu-154 1 0 1-20 788 end
eu-155 1 0 1-20 788 end
gd-155 1 0 1-20 788 end

```

```

arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
          16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
          73181 0.1 27059 0.2 26000 67.095 2 1 541 end

```

```

h2o 3 den=0.80256 1 528 end
arbm-bormod 0.80256 1 1 0 0 5000 100 3 1.0e-6 528 end

```

261 ppm boron (wt) in moderator for the Core IV

end comp

fuel-pin-cell geometry:

```

squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end

```

assembly and cycle parameters:

```

npin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numztotal=3 end
3 0.6048 500 10.5799 3 10.9791
power=18.139 burn=451.5 down=129 end
power=19.070 burn=333.1 down=370 temkcyc=796 end
power=16.755 burn=337 down=281.5 bfrac=261 temkcyc=777 end
o 135.0 cr 5.9 mm 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

```

```

1 ssssssssss aaaaaaaaaa ssssssssss 2222222222 hh hh
  ssssssssss aaaaaaaaaa ssssssssss 2222222222 hh hh
  ss ss aa aa ss ss 22 22 hh hh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  ssssssssss aaaaaaaaaa ssssssssss 22 hhhhhhhhhhhh
  ssssssssss aaaaaaaaaa ssssssssss 22 hhhhhhhhhhhh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh

```


ye6sec2h3.sum

```

.....
:
:          SCALE4.3  Bulletin Board
:          -----
:
:          Welcome to SCALE-4.3.
:
:          .....
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
  Yankee Rowe sample E6-SE-c2-3, 138.94 32.03 gwd/MTU, July 97
  .....
  mixtures of fuel-pin-unit-cell:
  .....
  44group latticecell
  .....
  uo2 1 den=10.18 1 894
    92234 0.020 92235 3.40 92236 0.020 92238 96.56 end
  kr-83 1 0 1-20 894 end
  kr-85 1 0 1-20 894 end
  y-89 1 0 1-20 894 end
  sr-90 1 0 1-20 894 end
  zr-93 1 0 1-20 894 end
  zr-94 1 0 1-20 894 end
  zr-95 1 0 1-20 894 end
  nb-94 1 0 1-20 894 end
  mo-95 1 0 1-20 894 end
  tc-99 1 0 1-20 894 end
  ru-101 1 0 1-20 894 end
  ru-106 1 0 1-20 894 end
  rh-103 1 0 1-20 894 end
  rh-105 1 0 1-20 894 end
  pd-105 1 0 1-20 894 end
  pd-108 1 0 1-20 894 end
  ag-109 1 0 1-20 894 end
  sb-124 1 0 1-20 894 end
  xe-131 1 0 1-20 894 end
  xe-132 1 0 1-20 894 end
  xe-135 1 0 1-20 894 end
  xe-136 1 0 1-20 894 end
  cs-134 1 0 1-20 894 end
  cs-135 1 0 1-20 894 end
  cs-137 1 0 1-20 894 end
  ba-136 1 0 1-20 894 end
  la-139 1 0 1-20 894 end
  pr-141 1 0 1-20 894 end
  pr-143 1 0 1-20 894 end
  ce-144 1 0 1-20 894 end
  nd-143 1 0 1-20 894 end
  nd-145 1 0 1-20 894 end
  nd-147 1 0 1-20 894 end
  pm-147 1 0 1-20 894 end
  pm-148 1 0 1-20 894 end
  sm-147 1 0 1-20 894 end
  sm-149 1 0 1-20 894 end
  sm-150 1 0 1-20 894 end
  sm-151 1 0 1-20 894 end
  sm-152 1 0 1-20 894 end
  eu-153 1 0 1-20 894 end
  eu-154 1 0 1-20 894 end
  eu-155 1 0 1-20 894 end
  gd-155 1 0 1-20 894 end
  .....
  arbm=ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
    16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
    73181 0.1 27059 0.2 26000 67.095 2 1 560 end
  h2o 3 den=0.78338 1 541 end
  arbm=bormod 0.78338 1 1 0 0 5000 100 3 1.0e-6 541 end
  .....
  261 ppm boron (wt) in moderator for the Core IV
  .....
  end comp
  .....
  fuel-pin-cell geometry:
  squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end
  .....
  assembly and cycle parameters:
  npin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5
  printlevel=5 lightel=9 implevel=2 numztotal=3 end
  3 0.6048 500 10.5799 3 10.9791
  power=29.24 burn=451.5 down=129 end
  power=32.45 burn=333.1 down=370 temkcyc=915 end
  power=23.79 burn=337 down=281.5 bfrac=261 temkcyc=848 end
  o 135.0 cr 5.9 mn 0.33
  fe 13.0 co 0.075 ni 9.9
  sr 221.0 nb 0.71 sn 3.6
  .....
1  ssssssssss aaaaaaaaaa ssssssssss 2222222222 hh hh
  ssssssssssss aaaaaaaaaa ssssssssssss 222222222222 hh hh
  ss ss aa aa ss ss 22 22 hh hh
  ss aa aa aa ss ss 22 22 hh hh
  ss aa aa aa ss ss 22 22 hh hh
  ssssssssssss aaaaaaaaaa ssssssssss 22 hhhhhhhhhhhh
  ssssssssssss aaaaaaaaaa ssssssssssss 22 hhhhhhhhhhhh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  .....

```


ye6sec2h5.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  Yankee Rowe sample E6-SE-c2-5, 57.66 cm 31.41 gwd/MTU, July 97
  -----
  mixtures of fuel-pin-unit-cell:
  -----
44group latticecell
-----
uo2 1 den=10.18 1 885
  92234 0.020 92235 3.40 92236 0.020 92238 96.56 end
kr-83 1 0 1-20 885 end
kr-85 1 0 1-20 885 end
y-89 1 0 1-20 885 end
sr-90 1 0 1-20 885 end
zr-93 1 0 1-20 885 end
zr-94 1 0 1-20 885 end
zr-95 1 0 1-20 885 end
nb-94 1 0 1-20 885 end
mo-95 1 0 1-20 885 end
tc-99 1 0 1-20 885 end
ru-101 1 0 1-20 885 end
ru-106 1 0 1-20 885 end
rh-103 1 0 1-20 885 end
rh-105 1 0 1-20 885 end
pd-105 1 0 1-20 885 end
pd-108 1 0 1-20 885 end
ag-109 1 0 1-20 885 end
sb-124 1 0 1-20 885 end
xe-131 1 0 1-20 885 end
xe-132 1 0 1-20 885 end
xe-135 1 0 1-20 885 end
xe-136 1 0 1-20 885 end
cs-134 1 0 1-20 885 end
cs-135 1 0 1-20 885 end
cs-137 1 0 1-20 885 end
ba-136 1 0 1-20 885 end
la-139 1 0 1-20 885 end
pr-141 1 0 1-20 885 end
pr-143 1 0 1-20 885 end
ce-144 1 0 1-20 885 end
nd-143 1 0 1-20 885 end
nd-145 1 0 1-20 885 end
nd-147 1 0 1-20 885 end
pm-147 1 0 1-20 885 end
pm-148 1 0 1-20 885 end
sm-147 1 0 1-20 885 end
sm-149 1 0 1-20 885 end
sm-150 1 0 1-20 885 end
sm-151 1 0 1-20 885 end
sm-152 1 0 1-20 885 end
eu-153 1 0 1-20 885 end
eu-154 1 0 1-20 885 end
eu-155 1 0 1-20 885 end
gd-155 1 0 1-20 885 end

arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
73181 0.1 27059 0.2 26000 67.095 2 1 547 end

h2o 3 den=0.79733 1 532 end
arbm-bormod 0.79733 1 1 0 0 5000 100 3 1.0e-6 532 end
-----
261 ppm boron (wt) in moderator for the Core IV
-----
end comp
-----

fuel-pin-cell geometry:
squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end
-----

assembly and cycle parameters:
npin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numzttotal=3 end
3 0.6048 500 10.5799 3 10.9791
power=29.51 burn=451.5 down=129 end
power=29.93 burn=333.1 down=370 temkyc=889 end
power=24.07 burn=337 down=281.5 bfrac=261 temkyc=847 end
o 135.0 cr 5.9 un 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

1 sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 222222222222 hh hh
ss ss aa aa ss ss 22 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ssssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh

```


	initial	22.6 d	45.2 d	67.7 d	90.3 d	90.3 d
o 16	charge 22.6 d 45.2 d 67.7 d 90.3 d 90.3 d	8.41E+03	8.41E+03	8.41E+03	8.41E+03	8.41E+03
mo 95	charge 22.6 d 45.2 d 67.7 d 90.3 d 90.3 d	.00E+00	6.04E-05	4.12E-04	1.19E-03	2.43E-03
tc 99	charge 22.6 d 45.2 d 67.7 d 90.3 d 90.3 d	.00E+00	3.24E-12	3.33E-11	1.21E-10	3.04E-10
totals	charge 22.6 d 45.2 d 67.7 d 90.3 d 90.3 d	1.15E+04	1.15E+04	1.15E+04	1.15E+04	1.15E+04
u233	charge 22.6 d 45.2 d 67.7 d 90.3 d 90.3 d	.00E+00	3.05E-07	6.00E-07	8.80E-07	1.15E-06
u234		8.55E-01	8.46E-01	8.37E-01	8.28E-01	8.19E-01
u235		1.45E+02	1.41E+02	1.38E+02	1.35E+02	1.32E+02
u236		8.47E-01	1.48E+00	2.10E+00	2.71E+00	3.29E+00
u238		4.06E+03	4.05E+03	4.05E+03	4.05E+03	4.05E+03
np237		.00E+00	8.27E-03	2.31E-02	4.08E-02	6.07E-02
pu236		.00E+00	2.13E-10	1.30E-09	3.55E-09	7.09E-09
pu238		.00E+00	4.60E-05	2.92E-04	8.07E-04	1.63E-03
pu238		.00E+00	4.60E-05	2.92E-04	8.07E-04	1.63E-03
pu239		.00E+00	1.51E+00	3.19E+00	4.74E+00	6.17E+00
pu240		.00E+00	2.03E-02	8.35E-02	1.82E-01	3.07E-01
pu241		.00E+00	7.25E-04	6.13E-03	2.01E-02	4.55E-02
pu242		.00E+00	3.23E-06	5.65E-05	2.83E-04	8.64E-04
am241	charge 22.6 d 45.2 d 67.7 d 90.3 d 90.3 d	.00E+00	5.17E-07	8.85E-06	4.43E-05	1.35E-04
am242m		.00E+00	7.95E-10	2.66E-08	1.93E-07	7.52E-07
am243		.00E+00	1.07E-08	3.83E-07	2.92E-06	1.20E-05
totals	charge 22.6 d 45.2 d 67.7 d 90.3 d 90.3 d	4.20E+03	4.20E+03	4.20E+03	4.19E+03	4.19E+03
decay data, including gamma and total energy, are from endf/b-vi						
1697 total number of nuclides in library						
nuclide concentrations, grams						
o 16	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d	1.35E+05	1.35E+05	1.35E+05	1.35E+05	1.35E+05
mo 95	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d	1.71E+01	1.79E+01	1.84E+01	1.88E+01	1.92E+01
tc 99	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d	7.99E-05	8.08E-05	8.08E-05	8.08E-05	8.08E-05
total	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d	3.92E+05	3.92E+05	3.92E+05	3.92E+05	3.92E+05
nuclide concentrations, grams						
u233	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d	1.83E-03	1.85E-03	1.87E-03	1.89E-03	1.91E-03
u234		1.20E+02	1.21E+02	1.21E+02	1.21E+02	1.22E+02
u235		1.18E+04	1.18E+04	1.18E+04	1.18E+04	1.18E+04
u236		4.13E+03	4.13E+03	4.13E+03	4.13E+03	4.13E+03
u238		9.40E+05	9.40E+05	9.40E+05	9.40E+05	9.40E+05
np237		4.62E+02	4.70E+02	4.70E+02	4.70E+02	4.70E+02
pu236		6.77E-04	6.59E-04	6.39E-04	6.20E-04	6.01E-04
pu238		1.72E+02	1.77E+02	1.80E+02	1.82E+02	1.84E+02
pu238		1.72E+02	1.77E+02	1.80E+02	1.82E+02	1.84E+02
pu239		6.46E+03	6.52E+03	6.52E+03	6.52E+03	6.52E+03
pu240		2.41E+03	2.41E+03	2.41E+03	2.41E+03	2.42E+03
pu241		1.56E+03	1.55E+03	1.54E+03	1.53E+03	1.52E+03
pu242		4.55E+02	4.55E+02	4.55E+02	4.55E+02	4.55E+02
am241		8.60E+01	9.56E+01	1.05E+02	1.15E+02	1.24E+02
am242m		2.42E+00	2.41E+00	2.41E+00	2.41E+00	2.41E+00
am243		9.91E+01	9.92E+01	9.92E+01	9.92E+01	9.92E+01
total	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d	9.67E+05	9.67E+05	9.67E+05	9.67E+05	9.67E+05
element concentrations, grams						
mo 95	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d	6.43E+02	6.65E+02	6.83E+02	6.95E+02	7.03E+02
tc 99	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d	7.50E+02	7.53E+02	7.53E+02	7.53E+02	7.53E+02
ru101		7.26E+02	7.26E+02	7.26E+02	7.26E+02	7.26E+02
rh103		4.38E+02	4.56E+02	4.65E+02	4.68E+02	4.70E+02
rh103m		3.27E-02	1.43E-02	6.24E-03	2.73E-03	1.19E-03
ag109		8.65E+01	8.66E+01	8.66E+01	8.66E+01	8.66E+01
nd143	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d	8.21E+02	8.35E+02	8.36E+02	8.36E+02	8.36E+02
nd145	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d	6.39E+02	6.39E+02	6.39E+02	6.39E+02	6.39E+02
sm147		1.06E+02	1.11E+02	1.16E+02	1.20E+02	1.25E+02
sm149		3.47E+00	4.38E+00	4.38E+00	4.38E+00	4.38E+00
sm150		2.82E+02	2.82E+02	2.82E+02	2.82E+02	2.82E+02
sm151		2.34E+01	2.35E+01	2.35E+01	2.35E+01	2.34E+01
eu151		4.76E-02	7.08E-02	9.41E-02	1.17E-01	1.41E-01
sm152		1.18E+02	1.18E+02	1.18E+02	1.18E+02	1.18E+02
eu153		1.09E+02	1.10E+02	1.10E+02	1.10E+02	1.10E+02
gd155		1.01E-01	1.86E-01	2.69E-01	3.51E-01	4.31E-01
total	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d	3.21E+04	3.21E+04	3.21E+04	3.21E+04	3.21E+04

ye6see4h3.sum

```

.....
SCALE4.3 Bulletin Board
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Welcome to SCALE-4.3.
.....

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  Yankee Rowe sample E6-SE-e4-3, 138.94 cm 30.39 gwd/MTU, July 97
  -----
  mixtures of fuel-pin-unit-cell:
  -----
44group latticecell
.
uo2 1 den=10.18 1 894
  92234 0.020 92235 3.40 92236 0.020 92238 96.56 end
kr-83 1 0 1-20 894 end
kr-85 1 0 1-20 894 end
y-89 1 0 1-20 894 end
sr-90 1 0 1-20 894 end
zr-93 1 0 1-20 894 end
zr-94 1 0 1-20 894 end
zr-95 1 0 1-20 894 end
nb-94 1 0 1-20 894 end
mo-95 1 0 1-20 894 end
tc-99 1 0 1-20 894 end
ru-101 1 0 1-20 894 end
ru-106 1 0 1-20 894 end
rh-103 1 0 1-20 894 end
rh-105 1 0 1-20 894 end
pd-105 1 0 1-20 894 end
pd-108 1 0 1-20 894 end
ag-109 1 0 1-20 894 end
sb-124 1 0 1-20 894 end
xe-131 1 0 1-20 894 end
xe-132 1 0 1-20 894 end
xe-135 1 0 1-20 894 end
xe-136 1 0 1-20 894 end
cs-134 1 0 1-20 894 end
cs-135 1 0 1-20 894 end
cs-137 1 0 1-20 894 end
ba-136 1 0 1-20 894 end
la-139 1 0 1-20 894 end
pr-141 1 0 1-20 894 end
pr-143 1 0 1-20 894 end
ce-144 1 0 1-20 894 end
nd-143 1 0 1-20 894 end
nd-145 1 0 1-20 894 end
nd-147 1 0 1-20 894 end
pm-147 1 0 1-20 894 end
pm-148 1 0 1-20 894 end
sm-147 1 0 1-20 894 end
sm-149 1 0 1-20 894 end
sm-150 1 0 1-20 894 end
sm-151 1 0 1-20 894 end
sm-152 1 0 1-20 894 end
eu-153 1 0 1-20 894 end
eu-154 1 0 1-20 894 end
eu-155 1 0 1-20 894 end
gd-155 1 0 1-20 894 end

arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
  16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
  73181 0.1 27059 0.2 26000 67.095 2 1 560 end

h2o 3 den=0.78338 1 541 end
arbm-bormod 0.78338 1 1 0 0 5000 100 3 1.0e-6 541 end
.
  261 ppm boron (wt) in moderator for Core IV
  -----
end comp
.
.
fuel-pin-cell geometry:
squarepitch 1.072 0.747 1 3 0.864 2 0.757 0 end
.
.
assembly and cycle parameters:
npin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numtotal=3 end
3 0.6048 500 10.5799 3 10.9791
power=32.84 burn=451.5 down=129 end
power=36.44 burn=333.1 down=370 temkcy=915 end
power=26.72 burn=337 down=281.5 bfrac=261 temkcy=848 end
o 135.0 cr 5.9 mn 0.33
fe 11.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

1 sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 222222222222 hh hh
ss ss aa aa ss ss 22 22 hh hh
ss ss aa aa ss ss 22 22 hh hh
ss ss aa aa ss ss 22 22 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh

```


	initial	22.6 d	45.2 d	67.7 d	90.3 d	90.3 d
0						
0						
o 16	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d					
	1.35E+05 1.35E+05 1.35E+05 1.35E+05 1.35E+05 1.35E+05					
0						
mo 95	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d					
	2.02E+01 2.10E+01 2.17E+01 2.21E+01 2.24E+01 2.26E+01 2.27E+01					
tc 99	1.31E-04 1.32E-04 1.32E-04 1.32E-04 1.32E-04 1.32E-04 1.32E-04					
0						
total	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d					
	3.92E+05 3.92E+05 3.92E+05 3.92E+05 3.92E+05 3.92E+05					
0						
u233	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d					
	1.92E-03 1.94E-03 1.96E-03 1.99E-03 2.01E-03 2.03E-03 2.05E-03					
u234	1.12E+02 1.12E+02 1.12E+02 1.12E+02 1.12E+02 1.13E+02 1.13E+02					
u235	1.02E+04 1.02E+04 1.02E+04 1.02E+04 1.02E+04 1.02E+04 1.02E+04					
u236	4.36E+03 4.36E+03 4.36E+03 4.36E+03 4.36E+03 4.36E+03 4.36E+03					
u238	9.35E+05 9.35E+05 9.35E+05 9.35E+05 9.35E+05 9.35E+05 9.35E+05					
np237	5.47E+02 5.55E+02 5.55E+02 5.55E+02 5.56E+02 5.56E+02 5.56E+02					
pu236	9.65E-04 9.39E-04 9.11E-04 8.83E-04 8.56E-04 8.30E-04 8.05E-04					
pu238	2.33E+02 2.39E+02 2.43E+02 2.46E+02 2.48E+02 2.50E+02 2.51E+02					
pu239	2.33E+02 2.39E+02 2.43E+02 2.46E+02 2.48E+02 2.50E+02 2.51E+02					
pu239	6.79E+03 6.87E+03 6.87E+03 6.87E+03 6.87E+03 6.87E+03 6.87E+03					
pu240	2.70E+03 2.70E+03 2.70E+03 2.70E+03 2.70E+03 2.70E+03 2.70E+03					
pu241	1.82E+03 1.80E+03 1.79E+03 1.78E+03 1.77E+03 1.76E+03 1.75E+03					
pu242	6.04E+02 6.04E+02 6.04E+02 6.04E+02 6.04E+02 6.04E+02 6.04E+02					
am241	9.70E+01 1.08E+02 1.19E+02 1.30E+02 1.41E+02 1.52E+02 1.63E+02					
am242m	2.80E+00 2.80E+00 2.80E+00 2.80E+00 2.80E+00 2.79E+00 2.79E+00					
am243	1.50E+02 1.50E+02 1.50E+02 1.50E+02 1.50E+02 1.50E+02 1.50E+02					
total	9.63E+05 9.63E+05 9.63E+05 9.63E+05 9.63E+05 9.63E+05 9.63E+05					
0						
0						
mo 95	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d					
	7.23E+02 7.47E+02 7.66E+02 7.79E+02 7.88E+02 7.93E+02 7.96E+02					
0						
tc 99	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d					
	8.41E+02 8.44E+02 8.44E+02 8.44E+02 8.44E+02 8.44E+02 8.44E+02					
ru101	8.27E+02 8.27E+02 8.27E+02 8.27E+02 8.27E+02 8.27E+02 8.27E+02					
rh103	4.89E+02 5.10E+02 5.20E+02 5.24E+02 5.25E+02 5.26E+02 5.27E+02					
rh103m	3.72E-02 1.62E-02 7.09E-03 3.10E-03 1.35E-03 5.91E-04 2.58E-04					
ag109	1.03E+02 1.03E+02 1.03E+02 1.03E+02 1.03E+02 1.03E+02 1.03E+02					
0						
nd143	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d					
	9.02E+02 9.17E+02 9.19E+02 9.19E+02 9.19E+02 9.19E+02 9.19E+02					
nd145	7.11E+02 7.11E+02 7.11E+02 7.11E+02 7.11E+02 7.11E+02 7.11E+02					
sm147	1.10E+02 1.15E+02 1.20E+02 1.25E+02 1.30E+02 1.34E+02 1.39E+02					
sm149	3.69E+00 4.74E+00 4.74E+00 4.74E+00 4.74E+00 4.74E+00 4.74E+00					
sm150	3.31E+02 3.31E+02 3.31E+02 3.31E+02 3.31E+02 3.31E+02 3.31E+02					
sm151	2.59E+01 2.61E+01 2.61E+01 2.60E+01 2.60E+01 2.60E+01 2.59E+01					
eu151	4.61E-02 7.19E-02 9.77E-02 1.23E-01 1.49E-01 1.75E-01 2.01E-01					
sm152	1.33E+02 1.33E+02 1.33E+02 1.33E+02 1.33E+02 1.33E+02 1.33E+02					
eu153	1.31E+02 1.32E+02 1.32E+02 1.32E+02 1.32E+02 1.32E+02 1.32E+02					
gd155	1.22E-01 2.28E-01 3.32E-01 4.34E-01 5.34E-01 6.33E-01 7.29E-01					
0						
total	initial 46.9 d 93.8 d 140.8 d 187.7 d 234.6 d 281.5 d					
	3.66E+04 3.66E+04 3.66E+04 3.66E+04 3.66E+04 3.66E+04 3.66E+04					

ye6see4h5.output

```

0.....
:
:          SCALE4.3  Bulletin  Board
:          -----  -----
:
:          Welcome to SCALE-4.3.
:
:.....
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
  Yankee Rowe sample E6-SE-e4-5, 57.66 cm 35.26 gwd/MTU, July 97
:
:  mixtures of fuel-pin-unit-cell:
:
:  Cross Section Library
:
: 44group  latticecell
:
:  Fuel Composition
:
uo2  1 den=10.18  1  885
    92234 0.020 92235 3.40 92236 0.020 92238 96.56  end
kr-83 1 0 1-20 885  end
kr-85 1 0 1-20 885  end
y-89  1 0 1-20 885  end
sr-90 1 0 1-20 885  end
zr-93 1 0 1-20 885  end
zr-94 1 0 1-20 885  end
zr-95 1 0 1-20 885  end
nb-94 1 0 1-20 885  end
mo-95 1 0 1-20 885  end
tc-99 1 0 1-20 885  end
ru-101 1 0 1-20 885  end
ru-106 1 0 1-20 885  end
rh-103 1 0 1-20 885  end
rh-105 1 0 1-20 885  end
pd-105 1 0 1-20 885  end
pd-108 1 0 1-20 885  end
ag-109 1 0 1-20 885  end
sb-124 1 0 1-20 885  end
xe-131 1 0 1-20 885  end
xe-132 1 0 1-20 885  end
xe-135 1 0 1-20 885  end
xe-136 1 0 1-20 885  end
cs-134 1 0 1-20 885  end
cs-135 1 0 1-20 885  end
cs-137 1 0 1-20 885  end
ba-136 1 0 1-20 885  end
la-139 1 0 1-20 885  end
pr-141 1 0 1-20 885  end
pr-143 1 0 1-20 885  end
ce-144 1 0 1-20 885  end
nd-143 1 0 1-20 885  end
nd-145 1 0 1-20 885  end
nd-147 1 0 1-20 885  end
pm-147 1 0 1-20 885  end
pm-148 1 0 1-20 885  end
sm-147 1 0 1-20 885  end
sm-149 1 0 1-20 885  end
sm-150 1 0 1-20 885  end
sm-151 1 0 1-20 885  end
sm-152 1 0 1-20 885  end
eu-153 1 0 1-20 885  end
eu-154 1 0 1-20 885  end
eu-155 1 0 1-20 885  end
gd-155 1 0 1-20 885  end

arbm-ss348 8.03 11 0 0 0 6012 0.08 25055 2.0 15031 0.045
          16000 0.030 14000 0.75 24000 18.0 28000 11.0 41093 0.7
          73181 0.1 27059 0.2 26000 67.095 2 1 547  end

h2o  3 den=0.79733  1  532  end
arbm-bormod 0.79733 1 1 0 0 5000 100 3 1.0e-6 532  end
:
:  261 ppm boron (wt) in moderator for the Core IV
:
-----
:
:  fuel-pin-cell geometry:
:
squarepitch  1.072  0.747  1  3  0.864  2  0.757  0  end
:
:
:  assembly and cycle parameters:
:
mpin/assm=305 fuelngth=833.69 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numtotal=3  end
3 0.6048 500 10.5799 3 10 9791
power=33.13 burn=451.5 down=129  end
power=33.60 burn=333.1 down=370 tenkcy=889  end
power=27.02 burn=337 down=281.5 bfrac=261 tenkcy=847  end
o 135.0 cr 5.9 an 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

1  sssssssssss  aaaaaaaaaa  sssssssssss  2222222222  hh  hh
   sssssssssss  aaaaaaaaaa  sssssssssss  222222222222  hh  hh
ss  ss  aa  aa  ss  ss  22  22  hh  hh
ss  aa  aa  aa  ss  ss  22  22  hh  hh
ss  aa  aa  aa  ss  ss  22  22  hh  hh
ssssssssssss  aaaaaaaaaa  sssssssssss  22  hhhhhhhhhhhh
ssssssssssss  aaaaaaaaaa  sssssssssss  22  hhhhhhhhhhhh
   ss  aa  aa  ss  22  hh  hh
   ss  aa  aa  ss  22  hh  hh

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