

CRWMS/M&O

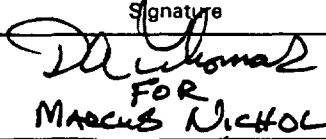

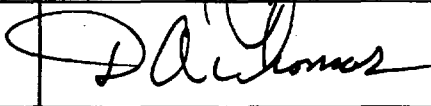
Design Analysis Cover Sheet

Complete only applicable items.

1.

QA: L

Page: 1 Of: 28

2. DESIGN ANALYSIS TITLE			
SAS2H Analysis of Radiochemical Assay Samples from Mihama PWR Reactor			
3. DOCUMENT IDENTIFIER (Including Rev. No.)			4. TOTAL PAGES
B00000000-01717-0200-00144 REV 00			28
5. TOTAL ATTACHMENTS		6. ATTACHMENT NUMBERS - NO. OF PAGES IN EACH	
2		I-13 pp.; II-39 pp.	
	Printed Name	Signature	Date
7. Originator	Marcus Nichol	 FOR MARCUS NICHOL	09/02/97
8. Checker	David Henderson		9-2-97
9. Lead Design Engineer	Dan Thomas		09/02/97
10. Department Manager	Hugh Benton	Hugh A. Benton	9/2/97
11. REMARKS			

Design Analysis Revision Record

Complete only applicable items.

1.

2. DESIGN ANALYSIS TITLE

SAS2H Analysis of Radiochemical Assay Samples from Mihama PWR Reactor

3. DOCUMENT IDENTIFIER (Including Rev. No.)

B00000000-01717-0200-00144 REV 00

4. Revision No.	5. Description of Revision
00	Initial Issuance

Table of Contents:

<u>Item</u>	<u>Page</u>
1. Purpose	4
2. Quality Assurance	4
3. Method	5
4. Design Inputs	6
4.1 Design Parameters	6
4.2 Criteria	14
4.3 Assumptions	14
4.4 Codes and Standards	14
5. References	15
6. Use of Computer Software	17
7. Design Analysis	18
7.1 SCALE Input Data Blocks 1, 2, and 3	18
7.2 SCALE Input Data Block 4	18
7.3 SCALE Input Data Blocks 5 Through 7	19
7.4 SCALE Input Data Block 8	20
7.5 SCALE Input Data Blocks 9 Through 16	23
7.6 Comparison of Calculated and Measured Concentrations	23
7.7 Results	24
8. Conclusions	27
9. Attachments	28

1. Purpose

The purpose of this design analysis is to determine the accuracy of the SAS2H module of SCALE 4.3 in predicting isotopic concentrations of spent fuel assemblies. The objective is to develop a methodology for modeling assemblies similar to those evaluated within this analysis and to establish the consistency of SAS2H predictions. The results of this analysis may then be applied to future depletion calculations using SAS2H in which no measurements are available.

2. Quality Assurance

The Quality Assurance (QA) program applies to this analysis. The work reported in this document is part of the Waste Package Design analysis that will eventually support the License Application Design phase. This activity, when appropriately confirmed, can impact the proper functioning of the Mined Geologic Disposal System (MGDS) waste package; the waste package has been identified as an MGDS Q-List item important to safety and waste isolation (pp. 4, 15, Reference 5.1). The waste package is on the Q-List by direct inclusion by the Department of Energy (DOE), without conducting a QAP-2-3 evaluation. The Waste Package Development Department (WPDD) responsible manager has evaluated this activity in accordance with QAP-2-0, *Conduct of Activities*. The *Perform Criticality, Thermal, Structural, and Shielding Analyses* (Reference 5.2) evaluation has determined the preparation and review of this design analysis is subject to *Quality Assurance Requirements and Description* (Reference 5.3) requirements. As specified in NLP-3-18, this activity is subject to QA controls.

The analysis described in this document supports development of the disposal criticality analysis methodology. No designs were analyzed in this document. This document will not directly support any construction, fabrication, or procurement activity and therefore is not required to be procedurally controlled as TBV (to be verified). The calculation design inputs or information used in this document come from data accepted by the Nuclear Regulatory Commission and by the scientific and engineering community as established fact. The specific references are listed in Section 5 and identified in Section 7. The information is therefore not treated as unqualified data.

3. Method

The analytical model employed for this analysis was the SAS2H module of the SCALE sequence. Based upon fuel design, power history, and operating data for specific assemblies in the Mihama pressurized water reactor (PWR), a computational model was developed for use with the SAS2H module of SCALE. The SAS2H module is used to perform a fuel depletion analysis to predict the isotopic concentrations in localized areas of assembly pins (pellet samples) subsequent to irradiation and cooling time. The isotopic concentrations predicted by the SAS2H module are then compared with measured concentrations of the same localized areas (axial locations) of the assembly pins to determine the accuracy of the developed model. The measured isotopic concentrations used for comparisons in the analysis are obtained from a separate report (Reference 5.5).

4. Design Inputs

The sources for the design parameters are References 5.4 through 5.9. Reference 5.4 provides information on molar masses; the assembly design, power history and operating parameters are obtained from References 5.5 and 5.6; the cladding composition from Reference 5.7; a list of trace elements in the fuel is derived from Reference 5.8; and light elements from Reference 5.9.

4.1 Design Parameters

The molar masses of selected elements are obtained from Reference 5.4 and are provided below within three significant figures. Precision beyond three significant figures is not necessary since the calculated isotopic concentrations from SCALE are only to three significant figures. Also, the weight per mole of enriched uranium is approximated by the weight per mole of natural uranium since the weight percent of enrichment is small.

Mole of natural uranium = 238 g,
 6.02×10^{23} atoms per mole. (Reference 5.4)

General spent fuel characteristics for each pellet sample are presented in Table 4-1 and include the initial ^{235}U enrichment, final burnup and the cooling time (Section 2.1.2, Reference 5.5). The initial enrichment ranges from 3.203 to 3.210 wt% ^{235}U and the burnup ranges from 6.92 to 34.32 GWd/MTU. Measurements of isotopic concentrations are back calculated to a reference cooling time of 1825 days for all samples.

Assembly design parameters are presented in Table 4-2 (Section 2.1.2, Reference 5.5). The samples come from a Westinghouse 15 x 15 assembly with one instrument tube and 20 guide tube positions, which were empty during operation. A cross section of a Westinghouse 15 x 15 assembly is presented in Figure 4-1 (Section 2.1.2, Reference 5.5). Initial enrichment of ^{234}U , ^{235}U and ^{236}U are given in Table 4-3 for the three different types of assemblies (Section 2.1.2, Reference 5.5).

One assembly was irradiated for one cycle, another for two cycles and the third for three cycles. The operating parameters in Table 4-4 include the uptime and downtime, cumulative burnups, specific powers, and average cycle boron concentrations (Section 2.1.2, Reference 5.5). The cycle boron concentrations were assumed to be to 450 ppm, since detailed information was not available. The average temperatures of the fuel, and moderator are presented in Table 4-5. The moderator temperature was determined by assuming a cosine fit based on axial height, and inlet and outlet temperatures. The moderator density is obtained from Appendix A of Reference 5.5. The fuel temperatures were not known, therefore, the temperature for Turkey Point Unit 3 assemblies are used, which is also a Westinghouse 15 x 15 design with similar specific powers (Table 3.8, Reference 5.6).

The composition of the cladding, Zircaloy-4, is presented in Table 4-6, and has a density of 6.56.

g/cm³ (Reference 5.7). A list of trace elements in the fuel used in updating cross sections during the depletion analysis is presented in Table 4-7 and developed with consideration of elements used in (Table 1, Reference 5.8). A generic set of light element weights for PWRs that is typically used in depletion analyses is included in Table 4-8 (Table 17, Reference 5.9). Variations in light element masses per unit fuel in different PWRs are small when compared to this generic set (p. 2-2, Reference 5.9). This data is provided in units of kg/MTUO₂ or kg/MTU depending on the units required in the analysis.

Measured isotopic concentrations are presented in Table 4-9 and are given in g/MTU (Section 2.1.2, Reference 5.5). The measurements were performed for nine samples from three assemblies at different axial heights, with varying degrees of exposure.

Table 4-1. Spent Fuel Characteristic Parameters for Samples from Mihama 3 PWR

Assembly	Enrichment, wt % ²³⁵U	Burnup, GWd/MTU	Cooling Time, days
86b02	3.208	8.30	1825
86b03	3.208	6.92	1825
86g03	3.203	21.29	1825
86g05	3.203	15.36	1825
86g07	3.203	14.66	1825
87c03	3.210	29.50	1825
87c04	3.210	32.20	1825
87c07	3.210	33.71	1825
87c08	3.210	34.32	1825

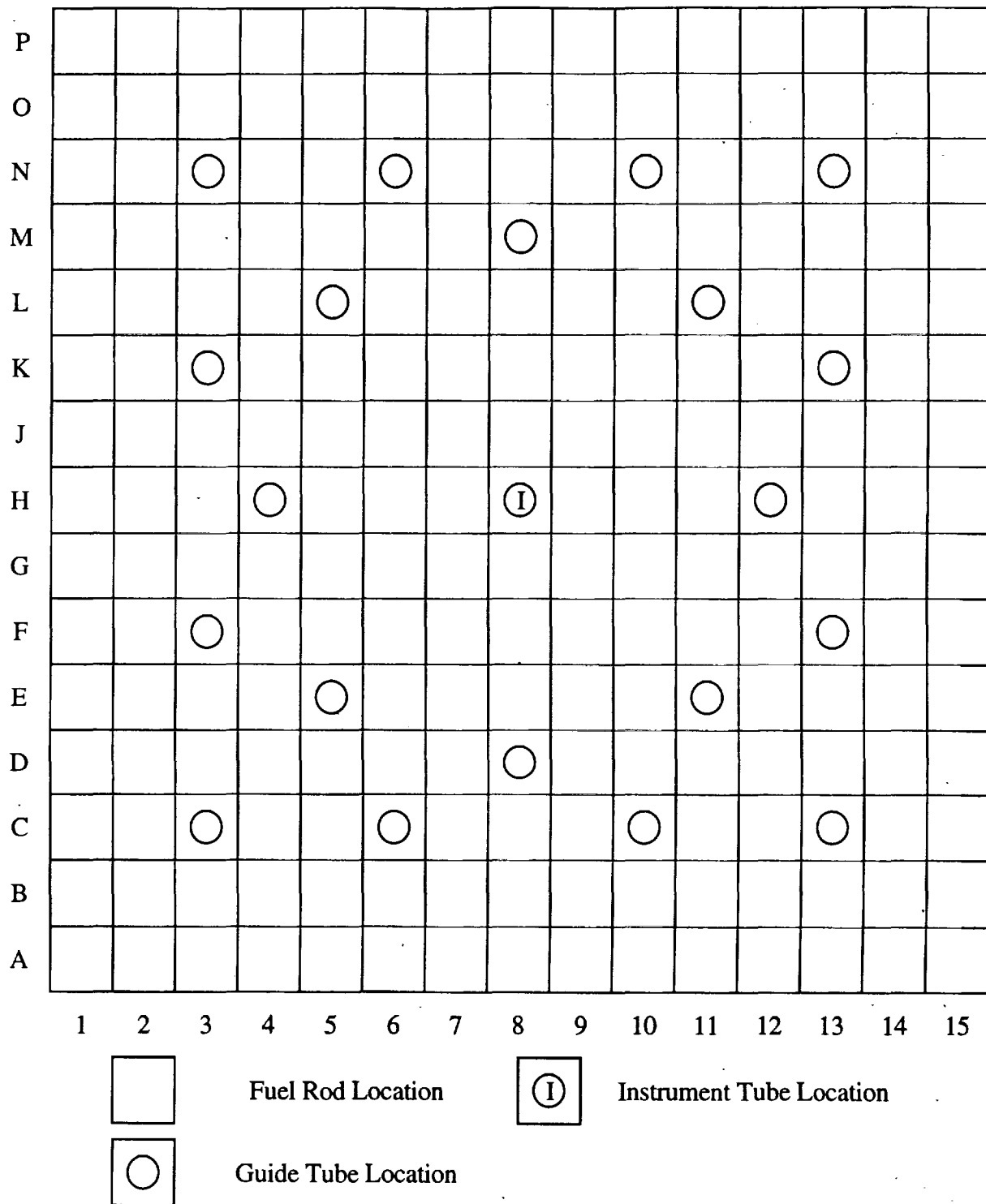
Reference 5.5

Table 4-2. Assembly Design Parameters for Mihama 3 PWR

Parameter	Data
Assembly General Data:	
Designer	Westinghouse
Lattice	15 x 15
Number of Fuel Rods	204
Number of Guide Tubes	20
Number of Instrument Tubes	1
Assembly Pitch, cm	21.50
Assembly Fuel, kg U	446
Fuel Rod Data:	
Pellet Density, g/cm ³	9.996
Rod Pitch, cm	1.430
Rod Outside Diameter (OD), cm	1.072
Rod Inside Diameter (ID), cm	0.948
Pellet Diameter, cm	0.929
Active Fuel Length, cm	365.76
Clad Material	Zircaloy-4
Guide Tube Data:	
Inner Diameter, cm	1.300
Outer Diameter, cm	1.387
Tube Material	Zircaloy-4

Reference 5.5

Figure 4-1. Cross Section of Mihama Assembly



Reference 5.5

Table 4-3. Fuel Composition by Assembly for Mihama 3 PWR

Assembly	86b	86g	87c
²³⁴ U wt %	0.0285	0.0285	0.0295
²³⁵ U wt %	3.208	3.203	3.210
²³⁶ U wt %	0.0208	0.0109	0.0327
²³⁸ U wt %	96.742	96.757	96.727

Reference 5.5

Table 4-4. Operating Data for Mihama 3 PWR

	Sample Identifier	Cycle II	Cycle III-1	Cycle III-2	Cycle IV-1	Cycle IV-2
Uptime, days		215	157	170	352	28
Downtime, days		388	9	176	0	1825
Cumulative Burnup, GWd/MTU	86b02	8.30	-	-	-	-
	86b03	6.92	-	-	-	-
	86g03	6.87	13.79	21.29	-	-
	86g05	4.94	9.95	15.36	-	-
	86g07	4.73	9.50	14.66	-	-
	87c03	5.29	10.77	16.71	28.73	29.50
	87c04	5.78	11.76	18.24	31.35	32.20
	87c07	6.05	12.31	19.10	32.82	33.71
	87c08	6.16	12.54	19.44	33.42	34.32
Specific Power, MW/MTU	86b02	38.61	-	-	-	-
	86b03	32.20	-	-	-	-
	86g03	31.95	44.10	44.10	-	-
	86g05	22.99	31.87	31.87	-	-
	86g07	22.00	30.37	30.37	-	-

Table 4-4. Operating Data for Mihama 3 PWR

	Sample Identifier	Cycle II	Cycle III-1	Cycle III-2	Cycle IV-1	Cycle IV-2
	87c03	24.61	34.92	34.92	34.15	27.47
	87c04	26.87	38.12	38.12	37.25	30.35
	87c07	28.13	39.91	39.91	38.99	31.77
	87c08	28.65	40.62	40.62	39.72	31.85
Boron Concentration, ppm	all	450	450	450	450	450

Reference 5.5

Table 4-5. Operating Temperatures for Mihama 3 PWR

Sample	Fuel, K	Cladding, K	Moderator, K	Moderator Density, g/cm ³
86b02	922	600	560	0.7518
86b03	922	634	594	0.6788
86g05	922	612	572	0.7298
86g03	922	625	585	0.6995
86g07	922	625	585	0.6995
87c03	922	600	560	0.7518
87c04	922	607	567	0.7390
87c07	922	601	561	0.7510
87c08	922	626	586	0.6984

References 5.5 and 5.6

Table 4-6. Composition of Zircaloy-4

Material	Weight Percent
O	0.12
Cr	0.10
Fe	0.20
Sn	1.40
Zr	98.18
Density = 6.56 g/cm ³	

Reference 5.7

Table 4-7. Nuclides Updated in SAS2H

⁸³ Kr	⁸⁵ Kr	⁸⁹ Y	⁹⁰ Sr	⁹⁵ Mo	⁹³ Zr
⁹⁴ Zr	⁹⁴ Nb	⁹⁵ Zr	⁹⁹ Tc	¹⁰¹ Ru	¹⁰³ Rh
¹⁰⁵ Rh	¹⁰⁶ Ru	¹⁰⁵ Pd	¹⁰⁸ Pd	¹⁰⁹ Ag	¹²⁴ Sb
¹³¹ Xe	¹³² Xe	¹³⁴ Cs	¹³⁵ Xe	¹³⁵ Cs	¹³⁶ Xe
¹³⁶ Ba	¹³⁷ Cs	¹³⁹ La	¹⁴¹ Pr	¹⁴³ Pr	¹⁴³ Nd
¹⁴⁴ Ce	¹⁴⁵ Nd	¹⁴⁷ Nd	¹⁴⁷ Pm	¹⁴⁷ Sm	¹⁴⁸ Pm
¹⁴⁹ Sm	¹⁵⁰ Sm	¹⁵¹ Sm	¹⁵² Sm	¹⁵³ Eu	¹⁵⁴ Eu
¹⁵⁵ Gd	¹⁵⁵ Eu				

Reference 5.8

Table 4-8. Light Element Mass per Unit of Fuel for a Typical PWR

Element	kg/MTU
O	135.0
Cr	5.9
Mn	0.33
Fe	13.0
Co	0.075
Ni	9.9
Zr	221.0
Nb	0.71
Sn	3.6

Reference 5.9

Table 4-9. Measured Isotopic Concentrations (g/MTU)

Sample	86b02	86b03	86g03	86g05	86g07	87c03	87c04	87c07	87c08
Burnup, GWd/MTU	8.30	6.92	21.29	15.36	14.66	29.50	32.20	33.71	34.32
²³⁴ U	267	-	-	-	-	-	174	174	-
²³⁵ U	23900	25200	14500	18500	18400	9790	9070	7890	8040
²³⁶ U	1650	1460	3270	2650	2660	3830	4000	4180	4200
²³⁸ U	962000	962000	952000	956000	957000	947000	944000	944000	942000
²³⁸ Pu	4.51	3.41	57.2	25.9	26.8	131	159	168	186
²³⁹ Pu	3020	2830	5080	4650	4740	5300	5470	4970	5320
²⁴⁰ Pu	422	344	1490	1030	1060	2100	2270	2320	2430
²⁴¹ Pu	109	82.8	651	408	425	955	1060	983	1080
²⁴² Pu	9.49	6.04	176	73.9	75.1	408	490	534	570

Reference 5.5

4.2 Criteria

The design of the waste package will depend on waste package configuration criticality analyses performed using an acceptable disposal criticality analysis methodology. Criteria that relate to the development and design of repository and engineered barrier components are derived from the applicable requirements and planning documents. The Engineered Barrier Design Requirements Document (EBDRD, Reference 5.12) provides requirements for engineered barrier segment design. The Repository Design Requirements Document (RDRD, Reference 5.13) provides requirements for repository design. The Controlled Design Assumptions Document (Reference 5.14) provides guidance for requirements listed in the EBDRD and RDRD which have unqualified or unconfirmed data associated with the requirement.

This analysis supports the disposal criticality analysis methodology by providing input, in the form of fuel depletion results, to benchmark calculations which address the prediction of both spent fuel isotopic compositions and their associated reactivity. These benchmark calculations will contribute to the determination of bias values in the method of critical multiplication factor calculation that is implemented by the analytic tools to be used in the disposal criticality methodology. The requirements for utilizing the bias in the method of calculation of the critical multiplication factor for disposal configurations containing spent nuclear fuel are located in Section 3.2.2.5 of the RDRD and Section 3.2.2.6 of the EBDRD. This analysis does not satisfy these requirements, but the results from this analysis will be used as input to subsequent analyses which will satisfy these requirements.

4.3 Assumptions

- 4.3.1 The fuel temperatures are assumed to be the same as for the Turkey Point Unit 3 temperatures from Table 3.8, Reference 5.6. This basis for this assumption is that the relationship between power and temperature in Turkey Point and Mihama are similar. The reason is that both reactors utilize the Westinghouse 15 x 15 assembly design and the samples for Mihama were irradiated at approximately the same specific power as those from Turkey Point Unit 3 (Reference 5.6, Table 3.8). This assumption is used in Section 7.2.
- 4.3.2 The cycle average boron concentrations are assumed to be 450 ppm. The basis for this assumption is that the value is an average of typical cycle average boron concentrations, and was obtained from Reference 5.5. This assumption is used in Section 7.2.

4.4 Codes and Standards

There are no applicable codes or standards for this design analysis.

5. References

- 5.1 *Yucca Mountain Site Characterization Project Q-List*, YMP/90-55Q REV 4, Yucca Mountain Site Characterization Project.
- 5.2 *QAP-2-0 Activity Evaluations: ID #WP-20, Perform Criticality, Thermal, Structural, and Shielding Analyses*, Civilian Radioactive Waste Management System (CRWMS) Management and Operating Contractor (M&O), August 3, 1997.
- 5.3 *Quality Assurance Requirements and Description*, DOE/RW-0333P REV 7, U.S. Department of Energy (DOE) Office of Civilian Radioactive Waste Management (OCRWM).
- 5.4 *Nuclides and Isotopes*, General Electric Company, 14ed., 1989.
- 5.5 *Isotopic and Criticality Validation for PWR Actinide-Only Burnup Credit*, DOE/RW-0497, DOE OCRWM.
- 5.6 *Fuel Inventory and Afterheat Power Studies of Uranium-Fueled Pressurized-Water-Reactors Fuel Assemblies Using the SAS2 and ORIGEN-S Modules of SCALE with an ENDF/B-V Updated Cross Section Library*, NUREG/CR-2397, November 1981.
- 5.7 *Material Compositions and Number Densities for Neutronics Calculations*, Document Identifier (DI) Number: BBA000000-01717-0200-00002 REV 00, CRWMS M&O.
- 5.8 *SCALE-4 Analysis of Pressurized Water Reactor Critical Configurations: Volume 2- Sequoyah Unit 2 Cycle 3*, ORNL/TM-12294/V2, March 1995.
- 5.9 *Validation of the Scale System for PWR Spent Fuel Isotopic Composition Analyses*, ORNL/TM-12667, Oak Ridge National Laboratory, March 1995.
- 5.10 *SCALE 4.3, A Modular Code System for Performing Standardized Computer Analyses for Licensing Evaluation for Workstations and Personal Computers*, NUREG/CR-0200 REV 5, ORNL/NUREG/CSD-2/R5, Volumes 1-3, Oak Ridge National Laboratory.
- 5.11 *Software Qualification Report for the SCALE Modular Code System*, DI Number: 30011-2002 REV 01, CRWMS M&O.
- 5.12 *Engineered Barrier Design Requirements Document*, YMP/CM-0024, REV 00, ICN 01, DOE OCRWM.

- 5.13 *Repository Design Requirements Document*, YMP/CM-0023, REV 00, ICN 01, DOE OCRWM.

- 5.14 *Controlled Design Assumptions Document*, DI#: B00000000-01717-4600-00032 REV 04, ICN 01, CRWMS M&O.

6. Use of Computer Software

- A. Reference 5.10 describes the SAS2H module of SCALE 4.3 that is used with the 44GROUPNDF5 cross section library to calculate the isotopic concentrations for the specified burnup and cooling time. The computer code's spatially independent point depletion model is appropriate for comparison with pellet sample measurements, and is used within the range of validation, as described in Reference 5.11, in accordance with the QAP-SI series procedures. SCALE is obtained from the Software Configuration Management in accordance with appropriate procedures. SCALE's CSCI number is 30011 V4.3 and is installed on the WPDD HP 9000, 700 Workstation with CRWMS M&O tag number 110433.

- B. *Lotus 1-2-3* Release 5 for Windows 95 is an Acquired Software spreadsheet program as defined in QAP-SI-0. User defined formulas and/or algorithms, inputs and results, are documented in the appropriate sections.

7. Design Analysis

The SAS2H module of SCALE 4.3 is used to perform one-dimensional (1-D) neutron transport and point depletion analyses on the Mihama samples using the preferred 44GROUPNDF5 cross-section library. To properly model the neutron flux spectrum and the nuclide composition changes, it is necessary to define the compositions, temperatures, and geometry of the fuel assembly. This is accomplished with the use of data blocks in which similar parameters are grouped together.

7.1 SCALE Input Data Blocks 1, 2, and 3

Data blocks 1 through 3 define the SCALE module to be used, the title of the input file, the cross section library to be used, and the lattice type to be modeled. The module used is SAS2H and the cross sectional library is 44GROUPNDF5, abbreviated as 44GROUP. The 44GROUP cross section library is recommended by Oak Ridge National Laboratory. Since SAS2H is only to be used for isotopic depletion/generation, the 'parm=skipshipdata' option is used so that a shipping cask shielding analysis is not performed. The title is arbitrary and should contain information that is sample specific, while the lattice type is "latticecell" to reflect the array characteristic of the assembly.

7.2 SCALE Input Data Block 4

Data block 4 defines the material compositions present in the assembly. A unique mixture number is assigned to each composition, and follows the form of mixture 1 for fuel, mixture 2 for cladding and mixture 3 for moderator.

The fuel mixture is specified as UO_2 using the isotopic weight percentages from Table 4-3 and the fuel temperature obtained from Table 4-5. The stack density is calculated from the fuel dimensions and the initial uranium fuel loading, with the following equation:

$$StackDensity = \frac{ULoad}{(NFR)\left(\frac{\pi}{4}\right)(PDia.)^2(FuelLength)} \left(\frac{1000gU}{1kgU}\right)\left(\frac{270gUO_2}{238gU}\right) \quad \text{Equation 7-1}$$

Where:

- StackDensity = Fuel Stack Density (gUO_2/cm^3)
- ULoad = Initial Uranium Fuel Loading per Assembly ($kgUO_2$)
- NFR = Number of Fuel Rods per Assembly
- PDia. = Fuel Pellet Diameter (cm)
- FuelLength = Active Fuel Length (cm)

The resulting stack density is $10.004 gUO_2/cm^3$, compared to the pellet density of $9.996 gUO_2/cm^3$. Therefore, it is concluded that the pellet density reported in Table 4-2 is the stack density, with the

difference being a result of rounding, and is used for mixture 1. Isotopes which are selected as needing their cross sections updated during the depletion analysis are included in the fuel mixture. A standard list of trace fuel elements is given in Table 4-7 and defined in the fuel mixture to have a concentration of 10^{-20} atoms/barn·cm.

The cladding material of Zircaloy-4 is not contained within the Standard Composition Library in SCALE 4.3 and must be defined as an arbitrary material. The cladding is defined with a density and isotopic weight percentages from Table 4-6 and temperature given in Table 4-5.

The moderator temperature, density and boron concentration are given in Tables 4-4 and 4-5, and is composed of H₂O and boron. The boron is defined as an arbitrary material with the moderator density and temperature, a volume fraction equal to the average boron concentration of cycle II, and a standard boron composition from the Standard Composition Library designated as 5000.

7.3 SCALE Input Data Blocks 5 Through 7

The unit fuel rod cell geometry is defined in data block 5. The 'squarepitch' designation for the type of lattice is appropriate since the fuel assembly consists of a square array of fuel rods. Fuel rod, cladding and pitch dimensions are given in Table 4-2 with the mixture number for each composition defined in Section 7.2. The gap mixture is defined as 0.

Data block 6 allows the user to specify such parameters as the spatial mesh, angular quadrature and the convergence criteria. It is determined that the default values are sufficient and such options are not used in this design model.

In data block 7 the user defines general assembly data and determines the level of detail in which the assembly is to be modeled. The number of fuel rods per assembly is given in Table 4-2 and the length is calculated so that an assembly contains 1 MTU, using the following equation:

$$Length = \frac{1}{\frac{\pi}{4}(POD)^2(PDen)(NFR)} * \frac{10^6 g UO_2}{1 MTU O_2} * \frac{270 MTU O_2}{238 MTU} \quad \text{Equation 7-2}$$

Where:

Length = Length Required for an Assembly to Contain 1 MTU (cm)

POD = Fuel Pellet Diameter (cm)

PDen = Pellet Stack Density (gUO₂/cm³)

NFR = Number of Fuel Rods

Since measured isotopic concentrations are presented in grams of isotope per Metric Ton of Uranium (MTU) and SCALE presents concentrations in grams of isotope per assembly, it is possible to alter the length so that the assembly contains 1 MTU. This is possible since the 1-D transport calculation is axially independent. Consequently, the length of the assembly does not impact the neutron flux spectrum nor the nuclide cross sections. The resulting length for the Mihama assembly is 820.74 cm.

One assembly was irradiated for a single cycle, another for two cycles and a third for three cycles. It is determined that approximately 80 days per cross section library is sufficient to accurately model the change in nuclide cross sections with increasing burnup, without over-burdening the SAS2H code. Therefore, the number of libraries per cycle are specified as five. To obtain the concentrations of all interested nuclides, a print level of 5 is chosen, while an input level of 2 is defined so that a Path B model may be utilized. The number of light elements is nine and is determined from Table 4-8, while the number of zones is five which is determined by the Path B model described in Section 7.4.

SAS2H calculates a linear boron concentration let down over each cycle when the number of libraries per cycle is specified as greater than one. The methodology calculates an initial boron concentration equal to 1.9 times the average boron concentration and a final boron concentration calculated as 0.1 times the average boron concentration. These two end points are used to determine a linear fit for the boron concentration let down, which is used to calculate the boron concentrations for each library in the cycle. However, a problem arises when the cycle specified is not a full cycle but rather an interval of a cycle. (It is sometimes necessary to specify an interval as a cycle in SAS2H so that either a period of downtime during the actual cycle or a power change during the actual cycle may be modeled.) In this case SAS2H would let down the boron concentration to 0.1 times the average boron concentration for the first interval and jump up to 1.9 times the average boron concentration for the beginning of the second cycle. In reality this jump does not exist and, therefore, the modeling of the boron concentration let down is inexact. A solution to this problem would be to split all cycles into approximately 80 day intervals and change the number of libraries per cycle to one. However, experience with the SAS2H code indicates that the error due to an inexact boron concentration let down function, such as described here, is usually less than 0.5%. Therefore, allowing the SAS2H code to calculate a boron concentration over an interval of a cycle is an acceptable approximation to the actual boron concentration let down.

7.4 SCALE Input Data Block 8

The Path B model for Mihama centralizes a guide tube with a surrounding homogenized fuel and moderator mixture and further surrounded by the moderator between assemblies. The equation below is used to determine the number of fuel unit cells that surround the guide tube unit cell by conserving the fuel to moderator volume ratio. All of the following equations used to calculate the

Path B model dimensions are derived. The results of the fuel-unit-cell calculations are presented in Table 7-1, and the resulting Path B model dimensions are presented in Table 7-2.

$$x = \frac{\left(\frac{F}{M}\right)(CUCMV)}{\left(FV\right) - \left(\frac{F}{M}\right)(MV)} \quad \text{Equation 7-3}$$

$$\frac{F}{M} = \frac{(NFR)\left(\frac{\pi}{4}\right)(POD)^2}{(NFR)\left[RP^2 - \left(\frac{\pi}{4}\right)(COD)^2\right] + (NGT)\left[RP^2 - \left(\frac{\pi}{4}\right)(GTOD)^2 + \left(\frac{\pi}{4}\right)(GTID)^2\right] + \left[RP^2 - \left(\frac{\pi}{4}\right)(ITOD)^2 + \left(\frac{\pi}{4}\right)(ITID)^2\right]} \quad \text{Equation 7-4}$$

$$CUCMV = RP^2 - \left(\frac{\pi}{4}\right)(GTOD)^2 + \left(\frac{\pi}{4}\right)(GTID)^2 \quad \text{Equation 7-5}$$

$$FV = \left(\frac{\pi}{4}\right)(POD)^2 \quad \text{Equation 7-6}$$

$$MV = RP^2 - \left(\frac{\pi}{4}\right)(COD)^2 \quad \text{Equation 7-7}$$

Where:

- x = Number of Unit Fuel Cells per Central Guide Tube
- F/M = Fuel to Moderator Volume Ratio
- NFR = Number of Fuel Rods
- POD = Fuel Pellet Outer Diameter
- RP = Rod Pitch
- COD = Cladding Outer Diameter
- NGT = Number of Guide Tubes
- GTOD = Guide Tube Outer Diameter
- GTID = Guide Tube Inner Diameter
- ITOD = Instrument Tube Outer Diameter
- ITID = Instrument Tube Inner Diameter
- CUCMV = Central Unit Cell Moderator Volume
- FV = Fuel Volume of One Fuel Unit Cell
- MV = Moderator Volume of One Fuel Unit Cell

Once the number of fuel cells per guide tube is determined the geometry of the Path B model is calculated. Since the guide tube unit cell is centralized, the dimensions of the first two zones are the same as the guide tube inner and outer radii.

The radius for the moderator surrounding the guide tube, but still within the guide tube cell, is calculated with the following equation:

$$R_3 = \sqrt{\left(\frac{1}{\pi}\right)RP^2} \quad \text{Equation 7-8}$$

Where:

R_3 = Radius of Moderator Surrounding Guide Tube

The area of an annular region is calculated by the difference between the outer circular area and the inner circular area. Equation 7-9 is the basis for the Equations 7-10 and 7-11 which determine the radii of the homogenized fuel zone and the outer moderator zone.

$$ARA = \pi(ORAR^2 - IRAR^2) \quad \text{Equation 7-9}$$

Where:

ARA = Annular Region Area

ORAR = Outer Radius of Annular Region

IRAR = Inner Radius of Annular Region

The area of the homogenized fuel zone surrounding the guide tube unit cell is equal to the number of fuel unit cells surrounding the guide tube multiplied by the area of a fuel unit cell. Consequently, the radius of the homogenized fuel zone is computed with the following equation:

$$R_4 = \sqrt{\left(\frac{x}{\pi}\right)RP^2 + R_3^2} \quad \text{Equation 7-10}$$

Where:

R_4 = Radius of Homogenized Fuel and Moderator Zone

The mixture number of the homogenized fuel and moderator mixture must be specified as 500. The code then determines the composition of the region based upon the dimensions and mixtures specified in the fuel unit cell data block 5.

The moderator in the channel between assemblies is determined by calculating the total moderator volume and multiplying by the fraction of unit cells in the larger unit cell of the Path B model. The total moderator volume between assemblies is determined by the assembly pitch and the fuel cell pitch multiplied by the number of unit cells. The radius of the moderator between assemblies is calculated from the following equation:

$$R_5 = \sqrt{\frac{(x+1)}{\pi * N_{Cell}} [AP^2 - (N_{Cell})(RP^2)] + R_4^2} \quad \text{Equation 7-11}$$

Where:

R_5 = Radius of Moderator Surrounding Assembly Zone

N_{Cell} = Number of Cells in Assembly

AP = Assembly Pitch

Table 7-1. Calculation of Fuel Unit Cell per Guide Tube Unit Cell

F/M	CUCMV, cm ²	FV, cm ²	MV, cm ²	x
0.5081	1.8613	0.6778	1.1423	9.7143

Table 7-2. Path B Model Dimensions

	R_1	R_2	R_3	R_4	R_5
Radius, cm	0.6500	0.6935	0.8068	2.6408	2.6470
Composition	Moderator	Cladding	Moderator	Fuel/Moderator	Moderator

7.5 SCALE Input Data Blocks 9 Through 16

Data block 9 is used to describe the power history of the reactor. The specific power, fuel irradiation period, the length of downtime, the fraction of boron and moderator density, and the temperature during the cycle may all be defined. The specific power is in units of MW/MTU, the irradiation period and length of downtime are both defined in days; with values presented in Table 4-4. The moderator density, boron concentration, and fuel temperature are assumed constant over the cycles irradiated and therefore, the options to specify cycle specific values are not used.

Light elements and their effective weight, in kg per assembly, are entered in data block 10. Table 4-8 provides a generic set of light elements and their weights, in kg per MTU. Since the fuel length is altered so that there is 1 MTU per assembly the use of light elements with weights of kg per MTU is appropriate.

Data blocks 11 through 15 describe the parameters used in radial shielding analysis of a shipping cask and are not necessary in performing the depletion analysis. Data block 16 denotes the end of the SCALE input.

7.6 Comparison of Calculated and Measured Concentrations

Comparisons of corresponding calculated and measured concentrations are performed on a percent difference basis. The difference between the measured and the calculated value is divided by the

measured value to determine the accuracy of the SAS2H calculation. A positive difference represents an over-prediction by the code, while a negative percent difference represents an under-prediction by the code. The measured concentrations are given in Table 4-9, calculated concentrations are presented in Table 7-3 and the percent differences are presented in Table 7-4.

In an attempt to determine the impact of the assumptions from Section 4.3 on the calculated isotopic concentrations, a sensitivity analysis is performed on the fuel temperature and boron concentration. Two samples representing low and high burnups, 86b02 and 87c07, are used to observe the changes in isotopic concentrations with both: 1) a 100 K decrease in fuel temperature, and 2) a 100 ppm increase in boron concentration. The results are reported in Tables 7-5 and 7-6.

7.7 Results

SAS2H predicted isotopic concentrations are presented in Table 7-3. The calculated concentrations are obtained through the methodology described in Sections 7.1 through 7.5, and with the input parameters defined in Section 4.1. Calculated concentrations are then compared with measured concentrations as described in Section 7.6 to determine the accuracy of the SAS2H module. Results of the comparison, in the form of percent differences, are presented in Table 7-4. Also, the results of the sensitivity analysis are reported in Tables 7-5 and 7-6.

Table 7-3. Calculated concentrations (g/MTU)

Sample	86b02	86b03	86g03	86g05	86g07	87c03	87c04	87c07	87c08
Burnup, GWd/MTU	8.30	6.92	21.29	15.36	14.66	29.50	32.20	33.71	34.32
²³⁴ U	2.53E2	-	-	-	-	-	1.82E2	1.78E2	-
²³⁵ U	2.34E4	2.48E4	1.39E4	1.77E4	1.83E4	9.40E3	8.31E3	7.63E3	7.77E3
²³⁶ U	1.75E3	1.53E3	3.25E3	2.63E3	2.54E3	4.08E3	4.23E3	4.31E3	4.32E3
²³⁸ U	9.62E5	9.63E5	9.52E5	9.57E5	9.57E5	9.46E5	9.44E5	9.43E5	9.42E5
²³⁸ Pu	4.54E0	3.30E0	5.01E1	2.18E1	2.03E1	1.15E2	1.41E2	1.54E2	1.69E2
²³⁹ Pu	3.05E3	2.81E3	4.98E3	4.30E3	4.29E3	5.11E3	5.21E3	5.19E3	5.45E3
²⁴⁰ Pu	4.30E2	3.47E2	1.51E3	1.01E3	9.69E2	2.05E3	2.23E3	2.30E3	2.39E3
²⁴¹ Pu	1.09E2	8.16E1	6.14E2	3.62E2	3.47E2	8.43E2	9.31E2	9.58E2	1.03E3
²⁴² Pu	1.02E1	6.26E0	1.76E2	7.04E1	6.33E1	3.81E2	4.69E2	5.19E2	5.45E2

Table 7-4. Percent Difference Between Measured and Calculated $[(C/M-1)*100]$

Sample	86b02	86b03	86g03	86g05	86g07	87c03	87c04	87c07	87c08
Burnup, GWd/MTU	8.30	6.92	21.29	15.36	14.66	29.50	32.20	33.71	34.32
²³⁴ U	-5.24	-	-	-	-	-	4.60	2.30	-
²³⁵ U	-2.09	-1.59	-4.14	-4.32	-0.54	-3.98	-8.38	-3.30	-3.36
²³⁶ U	6.06	4.79	-0.61	-0.75	-4.51	6.53	5.75	3.11	2.86
²³⁸ U	0.00	0.10	0.00	0.10	0.00	-0.11	0.00	-0.11	0.00
²³⁸ Pu	0.67	-3.23	-12.41	-15.83	-24.25	-12.21	-11.32	-8.33	-9.14
²³⁹ Pu	0.99	-0.71	-1.97	-7.53	-9.49	-3.58	-4.75	4.43	2.44
²⁴⁰ Pu	1.90	0.87	1.34	-1.94	-8.58	-2.38	-1.76	-0.86	-1.65
²⁴¹ Pu	0.00	-1.45	-5.68	-11.27	-18.35	-11.73	-12.17	-2.54	-4.63
²⁴² Pu	7.48	3.64	0.00	-4.74	-15.71	-6.62	-4.29	-2.81	-4.39

Table 7-5. Sensitivity Analyses for Sample 86b02

Case	Modeled Conditions	Fuel Temperature Decrease of 100 K		Boron Concentration Increase of 100 ppm	
		Calculated Concentration, g/MTU	% Change in Calculated	Calculated Concentration, g/MTU	% Change in Calculated
²³⁴ U	2.53E2	2.53E2	0.00	2.53E2	0.00
²³⁵ U	2.34E4	2.34E4	0.00	2.34E4	0.00
²³⁶ U	1.75E3	1.75E3	0.00	1.75E3	0.00
²³⁸ U	9.62E5	9.62E5	0.00	9.62E5	0.00
²³⁸ Pu	4.54E0	4.53E0	-0.22	4.60E0	1.32
²³⁹ Pu	3.05E3	3.02E3	-0.98	3.07E3	0.66
²⁴⁰ Pu	4.30E2	4.28E2	-0.47	4.33E2	0.70
²⁴¹ Pu	1.09E2	1.08E2	-0.92	1.10E2	0.92
²⁴² Pu	1.02E1	1.01E1	-0.98	1.03E1	0.98

Table 7-6. Sensitivity Analyses for Sample 87c07

Case	Modeled Conditions	Fuel Temperature Decrease of 100 K		Boron Concentration Increase of 100 ppm	
Isotope	Calculated Concentration, g/MTU	Calculated Concentration, g/MTU	% Change in Calculated Concentrations	Calculated Concentration, g/MTU	% Change in Calculated Concentrations
²³⁴ U	1.78E2	1.78E2	0.00	1.78E2	0.00
²³⁵ U	7.63E3	7.57E3	-0.79	7.70E3	0.92
²³⁶ U	4.31E3	4.32E3	0.23	4.30E3	-0.23
²³⁸ U	9.43E5	9.43E5	0.00	9.43E5	0.00
²³⁸ Pu	1.54E2	1.53E2	-0.65	1.55E2	0.65
²³⁹ Pu	5.19E3	5.12E3	-1.35	5.24E3	0.96
²⁴⁰ Pu	2.30E3	2.30E3	0.00	2.31E3	0.43
²⁴¹ Pu	9.58E2	9.47E2	-1.15	9.67E2	0.94
²⁴² Pu	5.19E2	5.17E2	-0.39	5.19E2	0.00

8. Conclusions

Inspection of the measured isotopic concentrations of sample 86g07 reveals that there is an inconsistency between the measured concentration of ^{235}U relative to other samples and the reported burnup. It is expected that for samples with the same enrichment, the concentration of ^{235}U will decrease with an increase in burnup. However, the concentration of ^{235}U for sample 86g07 is lower than the concentration for 86g05, while the indicated burnup for 86g05 is greater than that for 86g07. Therefore, it is believed that the reported burnup of sample 86g07 is lower than what would be expected by examining the relative isotopic concentrations. The results from sample 86g07 are not used as an indication of the accuracy of the SAS2H modules ability to predict isotopic concentrations.

The accuracy in which the SAS2H module is able to predict isotopic concentrations is indicated by the percent differences presented in Table 7-4. Inspection of such results reveals that the code consistently under-predicts the concentrations of ^{235}U , and ^{241}Pu . Percent differences from this analysis are compared with results from Reference 5.5, in which similar calculations were performed with a previous version of SCALE and the 27burnuplib cross section library. The concentrations calculated in Reference 5.5 for the most part agree with the concentrations calculated in this analysis; however, significant differences are seen for the plutonium isotopes. Since there are few differences between the model in Reference 5.5 and the model contained within, it is determined that the discrepancy between calculated concentrations for plutonium isotopes is caused by a change in the cross section library.

An analysis of the sensitivity of isotopic concentrations in relation to the fuel temperature reveals that for a 100 K decrease in the fuel temperature, most of the plutonium isotopic concentrations decrease by around 1.35% or less. For the sample at relatively low burnup, 86b02, the isotopes of ^{238}Pu , ^{239}Pu , ^{240}Pu , ^{241}Pu , and ^{242}Pu decrease by 1% or less; and the remaining isotopes are unchanged. For the sample at relatively high burnup, 87c07, the isotopes of ^{235}U , ^{238}Pu , and ^{242}Pu all decrease by less than 1% or less, isotopes ^{239}Pu and ^{241}Pu decrease by little more than 1%, ^{236}U increases by less than 1% and the remaining isotopes remain unchanged. Since the actual fuel temperature is not expected to deviate more than 200 K from the temperature assumed, the assumption of a fuel temperature of 922 K does not significantly effect the calculated isotopic concentrations.

An analysis of the sensitivity of isotopic concentrations in relation to the boron concentration reveals that for a 100 ppm increase in the boron concentration, the isotopic concentrations mostly increase. For the sample at relatively low burnup, 86b02, the isotopes of ^{238}Pu , ^{239}Pu , ^{240}Pu , ^{241}Pu and ^{242}Pu increase by around 1.32% or less, and the remaining isotopes are unchanged. For the sample at relatively high burnup, 87c07, the isotopes of ^{235}U , ^{238}Pu , ^{239}Pu , ^{240}Pu , and ^{241}Pu increase by less than 1%, the ^{236}U isotope decreases by less than 1%, and the remaining isotopes are unchanged. Since the average boron concentration is not expected to deviate more than 250 ppm from the assumed value, the assumption of an average boron concentration of 450 ppm does not significantly effect the calculated isotopic concentrations.

The SAS2H code normally predicts isotopic concentrations as a radial assembly average; however, measurements are performed on individual pellet samples. Therefore, local pellet conditions are modeled as closely as possible in this analysis so that a more realistic pellet composition can be determined. However, approximations made to obtain local pellet conditions will influence the calculated isotopic concentrations.

In general, the measured to calculated ratios reveal that the SAS2H module of SCALE is adequate in predicting isotopic concentrations for Mihama assemblies, using the modeling methodology presented. Although the assumptions for the fuel temperature and the average boron concentration do effect the resulting isotopic concentrations, the effects are not significant enough to account for all variation between the measured and calculated concentrations. More detailed operating data would be expected to improve the accuracy of the calculated concentrations in relation to the corresponding measurements. It is recommended that future analyses use more detailed data if possible.

9. Attachments

Attachment I includes thirteen pages and contains the input files used in the modeling of the Mihama samples. A description of the parameters contained within the input files is found in Sections 7.1 through 7.5.

Included in Attachment II is an extraction from each of the output files, containing the following information:

- echo of the SAS2H input deck,
- time/date stamp for when the SAS2H depletion calculation was performed,
- the output extraction of information pertinent to the Radiochemical Assay evaluations from the final ORIGEN calculation of the SAS2H depletion calculation.

mih86b02.input

=sas2h parm=skipshipdata

Mihama-3, 86b02 0, 8.3 GWd/MTU, 86b02, June 97

mixtures of fuel-pin-unitcell:

44group latticecell

uo2 1 den=9.996 1 922
92234 0.0285 92235 3.208 92236 0.0208 92238 96.742 end

kr-83 1 0 1-20 922 end

kr-85 1 0 1-20 922 end

y-89 1 0 1-20 922 end

sr-90 1 0 1-20 922 end

zr-93 1 0 1-20 922 end

zr-94 1 0 1-20 922 end

zr-95 1 0 1-20 922 end

nb-94 1 0 1-20 922 end

mo-95 1 0 1-20 922 end

tc-99 1 0 1-20 922 end

ru-101 1 0 1-20 922 end

ru-106 1 0 1-20 922 end

rh-103 1 0 1-20 922 end

rh-105 1 0 1-20 922 end

pd-105 1 0 1-20 922 end

pd-108 1 0 1-20 922 end

ag-109 1 0 1-20 922 end

sb-124 1 0 1-20 922 end

xe-131 1 0 1-20 922 end

xe-132 1 0 1-20 922 end

xe-135 1 0 1-20 922 end

xe-136 1 0 1-20 922 end

cs-134 1 0 1-20 922 end

cs-135 1 0 1-20 922 end

cs-137 1 0 1-20 922 end

ba-136 1 0 1-20 922 end

la-139 1 0 1-20 922 end

pr-141 1 0 1-20 922 end

pr-143 1 0 1-20 922 end

ce-144 1 0 1-20 922 end

nd-143 1 0 1-20 922 end

nd-145 1 0 1-20 922 end

nd-147 1 0 1-20 922 end

pm-147 1 0 1-20 922 end

pm-148 1 0 1-20 922 end

sm-147 1 0 1-20 922 end

sm-149 1 0 1-20 922 end

sm-150 1 0 1-20 922 end

sm-151 1 0 1-20 922 end

sm-152 1 0 1-20 922 end

eu-153 1 0 1-20 922 end

eu-154 1 0 1-20 922 end

eu-155 1 0 1-20 922 end

gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 600 end

h2o 3 den=0.7518 1 560 end

arbm-bormod 0.7518 1 1 0 0 5000 100 3 450.0e-6 560 end

450 ppm boron (wt) in moderator

end comp

fuel-pin-cell geometry:

squarepitch 1.4300 0.929 1 3 1.072 2 0.948 0 end

assembly and cycle parameters:

npin/assm=204 fuelnght=820.74 ncycles=1 nlib/cyc=5

printlevel=5 lightel=9 inplevel=2 numztotal=5 end

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

power=38.61 burn=215 down=1825 end

o 135.0 cr 5.9 mn 0.33

fe 13.0 co 0.075 ni 9.9

zr 221.0 nb 0.71 sn 3.6

end

mih86b03.input

=sas2h parm=skipshipdata

Mihama-3, 1, 6.92 GWd/MTU, 86b03, June 97

mixtures of fuel-pin-cell

44group latticecell

uo2 1 den=9.996 1 922

92234 0.0285 92235 3.208 92236 0.0208 92238 96.742 end

kr-83 1 0 1-20 922 end

kr-85 1 0 1-20 922 end

y-89 1 0 1-20 922 end

sr-90 1 0 1-20 922 end

zr-93 1 0 1-20 922 end

zr-94 1 0 1-20 922 end

zr-95 1 0 1-20 922 end

nb-94 1 0 1-20 922 end

mo-95 1 0 1-20 922 end

tc-99 1 0 1-20 922 end

ru-101 1 0 1-20 922 end

ru-106 1 0 1-20 922 end

rh-103 1 0 1-20 922 end

rh-105 1 0 1-20 922 end

pd-105 1 0 1-20 922 end

pd-108 1 0 1-20 922 end

ag-109 1 0 1-20 922 end

sb-124 1 0 1-20 922 end

xe-131 1 0 1-20 922 end

xe-132 1 0 1-20 922 end

xe-135 1 0 1-20 922 end

xe-136 1 0 1-20 922 end

cs-134 1 0 1-20 922 end

cs-135 1 0 1-20 922 end

cs-137 1 0 1-20 922 end

ba-136 1 0 1-20 922 end

la-139 1 0 1-20 922 end

pr-141 1 0 1-20 922 end

pr-143 1 0 1-20 922 end

ce-144 1 0 1-20 922 end

nd-143 1 0 1-20 922 end

nd-145 1 0 1-20 922 end

nd-147 1 0 1-20 922 end

pm-147 1 0 1-20 922 end

pm-148 1 0 1-20 922 end

sm-147 1 0 1-20 922 end

sm-149 1 0 1-20 922 end

sm-150 1 0 1-20 922 end

sm-151 1 0 1-20 922 end

sm-152 1 0 1-20 922 end

eu-153 1 0 1-20 922 end

eu-154 1 0 1-20 922 end

eu-155 1 0 1-20 922 end

gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40

40000 98.18 2 1.0 634 end

h2o 3 den=0.6788 1 594 end

arbm-bormod 0.6788 1 1 0 0 5000 100 3 450.0e-6 594 end

end comp

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

npin/assm=204 fuelnght=820.74 ncycles=1 nlib/cyc=5

printlevel=5 lightel=9 inplevel=2 numztotal=5 end

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

power=32.20 burn=215 down=1825 end

o 135.0 cr 5.9 mn 0.33

fe 13.0 co 0.075 ni 9.9

zr 221.0 nb 0.71 sn 3.6

end

mih86g03.input

=sas2h parm=skipshipdata

Mihama-3, 3, 21.29 GWd/MTU, 86g03, June 97

'mixtures of fuel-pin-cell
44group latticecell

```

uo2 1 den=9.996 1 933
92234 0.0285 92235 3.203 92236 0.0109 92238 96.757 end
kr-83 1 0 1-20 922 end
kr-85 1 0 1-20 922 end
y-89 1 0 1-20 922 end
sr-90 1 0 1-20 922 end
zr-93 1 0 1-20 922 end
zr-94 1 0 1-20 922 end
zr-95 1 0 1-20 922 end
nb-94 1 0 1-20 922 end
mo-95 1 0 1-20 922 end
tc-99 1 0 1-20 922 end
ru-101 1 0 1-20 922 end
ru-106 1 0 1-20 922 end
rh-103 1 0 1-20 922 end
rh-105 1 0 1-20 922 end
pd-105 1 0 1-20 922 end
pd-108 1 0 1-20 922 end
ag-109 1 0 1-20 922 end
sb-124 1 0 1-20 922 end
xe-131 1 0 1-20 922 end
xe-132 1 0 1-20 922 end
xe-135 1 0 1-20 922 end
xe-136 1 0 1-20 922 end
cs-134 1 0 1-20 922 end
cs-135 1 0 1-20 922 end
cs-137 1 0 1-20 922 end
ba-136 1 0 1-20 922 end
la-139 1 0 1-20 922 end
pr-141 1 0 1-20 922 end
pr-143 1 0 1-20 922 end
ce-144 1 0 1-20 922 end
nd-143 1 0 1-20 922 end
nd-145 1 0 1-20 922 end
nd-147 1 0 1-20 922 end
pm-147 1 0 1-20 922 end
pm-148 1 0 1-20 922 end
sm-147 1 0 1-20 922 end
sm-149 1 0 1-20 922 end
sm-150 1 0 1-20 922 end
sm-151 1 0 1-20 922 end
sm-152 1 0 1-20 922 end
eu-153 1 0 1-20 922 end
eu-154 1 0 1-20 922 end
eu-155 1 0 1-20 922 end
gd-155 1 0 1-20 922 end

```

```

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 625 end
h2o 3 den=0.6995 1 585 end
arbm-bormod 0.6995 1 1 0 0 5000 100 3 450.0e-6 585 end
end comp

```

```

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

```

```

npin/assm=204 fuelnght=820.74 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inlevel=2 numztotal=5 end

```

```

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

```

```

power=31.95 burn=215.0 down=388 end
power=44.10 burn=157.0 down=9.0 end
power=44.10 burn=170.0 down=1825 end

```

```

o 135.0 cr 5.9 mn 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

```

```

end

```

mih86g05.input

=sas2h parm=skipshpdata

Mihama-3, 2, 15.36 GWd/MTU, 86g05, June 97

mixtures of fuel-pin-cell
44group latticecell

```

uo2 1 den=9.996 1 922
  92234 0.0285 92235 3.203 92236 0.0109 92238 96.757 end
kr-83 1 0 1-20 922 end
kr-85 1 0 1-20 922 end
y-89 1 0 1-20 922 end
sr-90 1 0 1-20 922 end
zr-93 1 0 1-20 922 end
zr-94 1 0 1-20 922 end
zr-95 1 0 1-20 922 end
nb-94 1 0 1-20 922 end
mo-95 1 0 1-20 922 end
tc-99 1 0 1-20 922 end
ru-101 1 0 1-20 922 end
ru-106 1 0 1-20 922 end
rh-103 1 0 1-20 922 end
rh-105 1 0 1-20 922 end
pd-105 1 0 1-20 922 end
pd-108 1 0 1-20 922 end
ag-109 1 0 1-20 922 end
sb-124 1 0 1-20 922 end
xe-131 1 0 1-20 922 end
xe-132 1 0 1-20 922 end
xe-135 1 0 1-20 922 end
xe-136 1 0 1-20 922 end
cs-134 1 0 1-20 922 end
cs-135 1 0 1-20 922 end
cs-137 1 0 1-20 922 end
ba-136 1 0 1-20 922 end
la-139 1 0 1-20 922 end
pr-141 1 0 1-20 922 end
pr-143 1 0 1-20 922 end
ce-144 1 0 1-20 922 end
nd-143 1 0 1-20 922 end
nd-145 1 0 1-20 922 end
nd-147 1 0 1-20 922 end
pm-147 1 0 1-20 922 end
pm-148 1 0 1-20 922 end
sm-147 1 0 1-20 922 end
sm-149 1 0 1-20 922 end
sm-150 1 0 1-20 922 end
sm-151 1 0 1-20 922 end
sm-152 1 0 1-20 922 end
eu-153 1 0 1-20 922 end
eu-154 1 0 1-20 922 end
eu-155 1 0 1-20 922 end
gd-155 1 0 1-20 922 end

```

```

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 612 end

```

h2o 3 den=0.7298 1 572 end

```

arbm-bormod 0.7298 1 1 0 0 5000 100 3 450.0e-6 572 end
end comp

```

```

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

```

```

npin/assm=204 fuelght=820.74 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end

```

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

```

power=22.99 burn=215.0 down=388 end
power=31.87 burn=157.0 down=9.0 end
power=31.87 burn=170.0 down=1825 end

```

o 135.0 cr 5.9 mn 0.33

fe 13.0 co 0.075 ni 9.9

zr 221.0 nb 0.71 sn 3.6

end

mih86g07.input

=sas2h parm=skipshipdata

Mihama-3, 2, 14.66 GWd/MTU 86g07, June 97

'mixtures of fuel-pin-cell
44group latticecell

```

uo2 1 den=9.996 1 922
  92234 0.0285 92235 3.203 92236 0.0109 92238 96.757 end
kr-83 1 0 1-20 922 end
kr-85 1 0 1-20 922 end
y-89 1 0 1-20 922 end
sr-90 1 0 1-20 922 end
zr-93 1 0 1-20 922 end
zr-94 1 0 1-20 922 end
zr-95 1 0 1-20 922 end
nb-94 1 0 1-20 922 end
mo-95 1 0 1-20 922 end
tc-99 1 0 1-20 922 end
ru-101 1 0 1-20 922 end
ru-106 1 0 1-20 922 end
rh-103 1 0 1-20 922 end
rh-105 1 0 1-20 922 end
pd-105 1 0 1-20 922 end
pd-108 1 0 1-20 922 end
ag-109 1 0 1-20 922 end
sb-124 1 0 1-20 922 end
xe-131 1 0 1-20 922 end
xe-132 1 0 1-20 922 end
xe-135 1 0 1-20 922 end
xe-136 1 0 1-20 922 end
cs-134 1 0 1-20 922 end
cs-135 1 0 1-20 922 end
cs-137 1 0 1-20 922 end
ba-136 1 0 1-20 922 end
la-139 1 0 1-20 922 end
pr-141 1 0 1-20 922 end
pr-143 1 0 1-20 922 end
ce-144 1 0 1-20 922 end
nd-143 1 0 1-20 922 end
nd-145 1 0 1-20 922 end
nd-147 1 0 1-20 922 end
pm-147 1 0 1-20 922 end
pm-148 1 0 1-20 922 end
sm-147 1 0 1-20 922 end
sm-149 1 0 1-20 922 end
sm-150 1 0 1-20 922 end
sm-151 1 0 1-20 922 end
sm-152 1 0 1-20 922 end
eu-153 1 0 1-20 922 end
eu-154 1 0 1-20 922 end
eu-155 1 0 1-20 922 end
gd-155 1 0 1-20 922 end

```

```

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 625 end
h2o 3 den=0.6995 1 585 end
arbm-bormod 0.6995 1 1 0 0 5000 100 3 450.0e-6 585 end
end comp

```

```

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

```

```

npin/assm=204 fuelnght=820.74 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end

```

```

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

```

```

power=22.00 burn=215.0 down=388 end
power=30.37 burn=157.0 down=9.0 end
power=30.37 burn=170.0 down=1825 end

```

```

o 135.0 cr 5.9 mn 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

```

```

end

```

mih87c03.input

=sas2h parm=skipshipdata

Mihama-3, 5, 29.5 GWd/MTU 87c03, June 97

mixtures of fuel pin cell

44group latticecell

```

uo2 1 den=9.996 1 922
  92234 0.0295 92235 3.21 92236 0.0327 92238 96.727 end
kr-83 1 0 1-20 922 end
kr-85 1 0 1-20 922 end
y-89 1 0 1-20 922 end
sr-90 1 0 1-20 922 end
zr-93 1 0 1-20 922 end
zr-94 1 0 1-20 922 end
zr-95 1 0 1-20 922 end
nb-94 1 0 1-20 922 end
mo-95 1 0 1-20 922 end
tc-99 1 0 1-20 922 end
ru-101 1 0 1-20 922 end
ru-106 1 0 1-20 922 end
rh-103 1 0 1-20 922 end
rh-105 1 0 1-20 922 end
pd-105 1 0 1-20 922 end
pd-108 1 0 1-20 922 end
ag-109 1 0 1-20 922 end
sb-124 1 0 1-20 922 end
xe-131 1 0 1-20 922 end
xe-132 1 0 1-20 922 end
xe-135 1 0 1-20 922 end
xe-136 1 0 1-20 922 end
cs-134 1 0 1-20 922 end
cs-135 1 0 1-20 922 end
cs-137 1 0 1-20 922 end
ba-136 1 0 1-20 922 end
la-139 1 0 1-20 922 end
pr-141 1 0 1-20 922 end
pr-143 1 0 1-20 922 end
ce-144 1 0 1-20 922 end
nd-143 1 0 1-20 922 end
nd-145 1 0 1-20 922 end
nd-147 1 0 1-20 922 end
pm-147 1 0 1-20 922 end
pm-148 1 0 1-20 922 end
sm-147 1 0 1-20 922 end
sm-149 1 0 1-20 922 end
sm-150 1 0 1-20 922 end
sm-151 1 0 1-20 922 end
sm-152 1 0 1-20 922 end
eu-153 1 0 1-20 922 end
eu-154 1 0 1-20 922 end
eu-155 1 0 1-20 922 end
gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
  40000 98.18 2 1.0 600 end
h2o 3 den=0.7518 1 560 end
arbm-bormod 0.7518 1 1 0 0 5000 100 3 450.0e-6 560 end
end comp

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

```

```

npin/assm=204 fuelnght=820.74 ncycles=5 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end

```

```

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

```

```

power=24.61 burn=215.0 down=388 end
power=34.92 burn=157.0 down=9.0 end
power=34.92 burn=170.0 down=176 end
power=34.15 burn=352.0 down=0 end
power=27.47 burn=28.00 down=1825 end

```

```

o 135.0 cr 5.9 mn 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

```

end

mih87c04.input

=sas2h parm=skipshipdata

Mihama-3, 6, 32.2 GWd/MTU, 87c04, June 97

'mixtures of fuel-pin-cell

44group latticecell

uo2 1 den=9.996 1 922

92234 0.0295 92235 3.21 92236 0.0327 92238 96.727 end

kr-83 1 0 1-20 922 end

kr-85 1 0 1-20 922 end

y-89 1 0 1-20 922 end

sr-90 1 0 1-20 922 end

zr-93 1 0 1-20 922 end

zr-94 1 0 1-20 922 end

zr-95 1 0 1-20 922 end

nb-94 1 0 1-20 922 end

mo-95 1 0 1-20 922 end

tc-99 1 0 1-20 922 end

ru-101 1 0 1-20 922 end

ru-106 1 0 1-20 922 end

rh-103 1 0 1-20 922 end

rh-105 1 0 1-20 922 end

pd-105 1 0 1-20 922 end

pd-108 1 0 1-20 922 end

ag-109 1 0 1-20 922 end

sb-124 1 0 1-20 922 end

xe-131 1 0 1-20 922 end

xe-132 1 0 1-20 922 end

xe-135 1 0 1-20 922 end

xe-136 1 0 1-20 922 end

cs-134 1 0 1-20 922 end

cs-135 1 0 1-20 922 end

cs-137 1 0 1-20 922 end

ba-136 1 0 1-20 922 end

la-139 1 0 1-20 922 end

pr-141 1 0 1-20 922 end

pr-143 1 0 1-20 922 end

ce-144 1 0 1-20 922 end

nd-143 1 0 1-20 922 end

nd-145 1 0 1-20 922 end

nd-147 1 0 1-20 922 end

pm-147 1 0 1-20 922 end

pm-148 1 0 1-20 922 end

sm-147 1 0 1-20 922 end

sm-149 1 0 1-20 922 end

sm-150 1 0 1-20 922 end

sm-151 1 0 1-20 922 end

sm-152 1 0 1-20 922 end

eu-153 1 0 1-20 922 end

eu-154 1 0 1-20 922 end

eu-155 1 0 1-20 922 end

gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 607 end

h2o 3 den=0.7390 1 567 end

arbm-bormod 0.7390 1 1 0 0 5000 100 3 450.0e-6 567 end

end comp

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

npin/assm=204 fuelnght=820.74 ncycles=5 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

power=26.87 burn=215.0 down=388 end

power=38.12 burn=157.0 down=9.0 end

power=38.12 burn=170.0 down=176 end

power=37.25 burn=352.0 down=0 end

power=30.35 burn=28.00 down=1825 end

o 135.0 cr 5.9 mn 0.33

fe 13.0 co 0.075 ni 9.9

zr 221.0 nb 0.71 sn 3.6

end

mih87c07.input

=sas2h parm=skipshipdata

Mihama-3, 7, 33.7 GWd/MTU, 87c07, June 97

'mixtures of fuel-pin-cell

44group latticecell

uo2 1 den=9.996 1 922

92234 0.0295 92235 3.21 92236 0.0327 92238 96.727 end

kr-83 1 0 1-20 922 end

kr-85 1 0 1-20 922 end

y-89 1 0 1-20 922 end

sr-90 1 0 1-20 922 end

zr-93 1 0 1-20 922 end

zr-94 1 0 1-20 922 end

zr-95 1 0 1-20 922 end

nb-94 1 0 1-20 922 end

mo-95 1 0 1-20 922 end

tc-99 1 0 1-20 922 end

ru-101 1 0 1-20 922 end

ru-106 1 0 1-20 922 end

rh-103 1 0 1-20 922 end

rh-105 1 0 1-20 922 end

pd-105 1 0 1-20 922 end

pd-108 1 0 1-20 922 end

ag-109 1 0 1-20 922 end

sb-124 1 0 1-20 922 end

xe-131 1 0 1-20 922 end

xe-132 1 0 1-20 922 end

xe-135 1 0 1-20 922 end

xe-136 1 0 1-20 922 end

cs-134 1 0 1-20 922 end

cs-135 1 0 1-20 922 end

cs-137 1 0 1-20 922 end

ba-136 1 0 1-20 922 end

la-139 1 0 1-20 922 end

pr-141 1 0 1-20 922 end

pr-143 1 0 1-20 922 end

ce-144 1 0 1-20 922 end

nd-143 1 0 1-20 922 end

nd-145 1 0 1-20 922 end

nd-147 1 0 1-20 922 end

pm-147 1 0 1-20 922 end

pm-148 1 0 1-20 922 end

sm-147 1 0 1-20 922 end

sm-149 1 0 1-20 922 end

sm-150 1 0 1-20 922 end

sm-151 1 0 1-20 922 end

sm-152 1 0 1-20 922 end

eu-153 1 0 1-20 922 end

eu-154 1 0 1-20 922 end

eu-155 1 0 1-20 922 end

gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40

40000 98.18 2 1.0 601 end

h2o 3 den=0.7510 1 561 end

arbm-bormod 0.7510 1 1 0 0 5000 100 3 450.0e-6 561 end

end comp

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

npin/assm=204 fuelnght=820.74 ncycles=5 nlib/cyc=5

printlevel=5 lightel=9 inplevel=2 numztotal=5 end

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

power=28.13 burn=215.0 down=388 end

power=39.91 burn=157.0 down=9.0 end

power=39.91 burn=170.0 down=176 end

power=38.99 burn=352.0 down=0 end

power=31.77 burn=28.00 down=1825 end

o 135.0 cr 5.9 mn 0.33

fe 13.0 co 0.075 ni 9.9

zr 221.0 nb 0.71 sn 3.6

end

mih87c08.input

=sas2h parm=skipshipdata

Mihama-3, 8, 34.2 GWd/MTU, 87c08, June 97

'mixtures of fuel-pin-cell

44group latticecell

uo2 1 den=9.996 1 922

92234 0.0295 92235 3.21 92236 0.0327 92238 96.727 end

kr-83 1 0 1-20 922 end

kr-85 1 0 1-20 922 end

y-89 1 0 1-20 922 end

sr-90 1 0 1-20 922 end

zr-93 1 0 1-20 922 end

zr-94 1 0 1-20 922 end

zr-95 1 0 1-20 922 end

nb-94 1 0 1-20 922 end

mo-95 1 0 1-20 922 end

tc-99 1 0 1-20 922 end

ru-101 1 0 1-20 922 end

ru-106 1 0 1-20 922 end

rh-103 1 0 1-20 922 end

rh-105 1 0 1-20 922 end

pd-105 1 0 1-20 922 end

pd-108 1 0 1-20 922 end

ag-109 1 0 1-20 922 end

sb-124 1 0 1-20 922 end

xe-131 1 0 1-20 922 end

xe-132 1 0 1-20 922 end

xe-135 1 0 1-20 922 end

xe-136 1 0 1-20 922 end

cs-134 1 0 1-20 922 end

cs-135 1 0 1-20 922 end

cs-137 1 0 1-20 922 end

ba-136 1 0 1-20 922 end

la-139 1 0 1-20 922 end

pr-141 1 0 1-20 922 end

pr-143 1 0 1-20 922 end

ce-144 1 0 1-20 922 end

nd-143 1 0 1-20 922 end

nd-145 1 0 1-20 922 end

nd-147 1 0 1-20 922 end

pm-147 1 0 1-20 922 end

pm-148 1 0 1-20 922 end

sm-147 1 0 1-20 922 end

sm-149 1 0 1-20 922 end

sm-150 1 0 1-20 922 end

sm-151 1 0 1-20 922 end

sm-152 1 0 1-20 922 end

eu-153 1 0 1-20 922 end

eu-154 1 0 1-20 922 end

eu-155 1 0 1-20 922 end

gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40

40000 98.18 2 1.0 626 end

h2o 3 den=0.6984 1 586 end

arbm-bormod 0.6984 1 1 0 0 5000 100 3 450.0e-6 586 end

end comp

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

npin/assm=204 fuelnght=820.74 ncycles=5 nlib/cyc=5

printlevel=5 lightel=9 inlevel=2 numztotal=5 end

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

power=28.65 burn=215.0 down=388 end

power=40.62 burn=157.0 down=9.0 end

power=40.62 burn=170.0 down=176 end

power=39.72 burn=352.0 down=0 end

power=31.85 burn=28.00 down=1825 end

o 135.0 cr 5.9 mn 0.33

fc 13.0 co 0.075 ni 9.9

zr 221.0 nb 0.71 sn 3.6

end

mih86b02less100deg.input

=sas2h parm=skipshipdata

Mihama-3, 86b02 0, 8.3 GWd/MTU, 86b02, June 97

 mixtures of fuel-pin-unitcell:

44group latticecell

uo2 1 den=9.996 1 822

92234 0.0285 92235 3.208 92236 0.0208 92238 96.742 end

kr-83 1 0 1-20 822 end

kr-85 1 0 1-20 822 end

y-89 1 0 1-20 822 end

sr-90 1 0 1-20 822 end

zr-93 1 0 1-20 822 end

zr-94 1 0 1-20 822 end

zr-95 1 0 1-20 822 end

nb-94 1 0 1-20 822 end

mo-95 1 0 1-20 822 end

tc-99 1 0 1-20 822 end

ru-101 1 0 1-20 822 end

ru-106 1 0 1-20 822 end

rh-103 1 0 1-20 822 end

rh-105 1 0 1-20 822 end

pd-105 1 0 1-20 822 end

pd-108 1 0 1-20 822 end

ag-109 1 0 1-20 822 end

sb-124 1 0 1-20 822 end

xe-131 1 0 1-20 822 end

xe-132 1 0 1-20 822 end

xe-135 1 0 1-20 822 end

xe-136 1 0 1-20 822 end

cs-134 1 0 1-20 822 end

cs-135 1 0 1-20 822 end

cs-137 1 0 1-20 822 end

ba-136 1 0 1-20 822 end

la-139 1 0 1-20 822 end

pr-141 1 0 1-20 822 end

pr-143 1 0 1-20 822 end

ce-144 1 0 1-20 822 end

nd-143 1 0 1-20 822 end

nd-145 1 0 1-20 822 end

nd-147 1 0 1-20 822 end

pm-147 1 0 1-20 822 end

pm-148 1 0 1-20 822 end

sm-147 1 0 1-20 822 end

sm-149 1 0 1-20 822 end

sm-150 1 0 1-20 822 end

sm-151 1 0 1-20 822 end

sm-152 1 0 1-20 822 end

eu-153 1 0 1-20 822 end

eu-154 1 0 1-20 822 end

eu-155 1 0 1-20 822 end

gd-155 1 0 1-20 822 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40

40000 98.18 2 1.0 600 end

h2o 3 den=0.7518 1 560 end

arbm-bormod 0.7518 1 1 0 0 5000 100 3 450.0e-6 560 end

450 ppm boron (wt) in moderator

 end comp

fuel-pin-cell geometry:

squarepitch 1.4300 0.929 1 3 1.072 2 0.948 0 end

 assembly and cycle parameters:

npin/assm=204 fuelnght=820.74 ncycles=1 nlib/cyc=5

printlevel=5 lightel=9 inplevel=2 numztotal=5 end

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

power=38.61 burn=215 down=1825 end

o 135.0 cr 5.9 mn 0.33

fe 13.0 co 0.075 ni 9.9

zr 221.0 nb 0.71 sn 3.6

 end

mih86b02plus100boron.input

=sas2h parm=skipshipdata

Mihama-3, 86b02 0, 8.3 GWd/MTU, 86b02, June 97

mixtures of fuel-pin-unitcell:

44group latticecell

u02 1 den=9.996 1 922
 92234 0.0285 92235 3.208 92236 0.0208 92238 96.742 end
 kr-83 1 0 1-20 922 end
 kr-85 1 0 1-20 922 end
 y-89 1 0 1-20 922 end
 sr-90 1 0 1-20 922 end
 zr-93 1 0 1-20 922 end
 zr-94 1 0 1-20 922 end
 zr-95 1 0 1-20 922 end
 nb-94 1 0 1-20 922 end
 mo-95 1 0 1-20 922 end
 tc-99 1 0 1-20 922 end
 ru-101 1 0 1-20 922 end
 ru-106 1 0 1-20 922 end
 rh-103 1 0 1-20 922 end
 rh-105 1 0 1-20 922 end
 pd-105 1 0 1-20 922 end
 pd-108 1 0 1-20 922 end
 ag-109 1 0 1-20 922 end
 sb-124 1 0 1-20 922 end
 xe-131 1 0 1-20 922 end
 xe-132 1 0 1-20 922 end
 xe-135 1 0 1-20 922 end
 xe-136 1 0 1-20 922 end
 cs-134 1 0 1-20 922 end
 cs-135 1 0 1-20 922 end
 cs-137 1 0 1-20 922 end
 ba-136 1 0 1-20 922 end
 la-139 1 0 1-20 922 end
 pr-141 1 0 1-20 922 end
 pr-143 1 0 1-20 922 end
 ce-144 1 0 1-20 922 end
 nd-143 1 0 1-20 922 end
 nd-145 1 0 1-20 922 end
 nd-147 1 0 1-20 922 end
 pm-147 1 0 1-20 922 end
 pm-148 1 0 1-20 922 end
 sm-147 1 0 1-20 922 end
 sm-149 1 0 1-20 922 end
 sm-150 1 0 1-20 922 end
 sm-151 1 0 1-20 922 end
 sm-152 1 0 1-20 922 end
 eu-153 1 0 1-20 922 end
 eu-154 1 0 1-20 922 end
 eu-155 1 0 1-20 922 end
 gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
 40000 98.18 2 1.0 600 end
 h2o 3 den=0.7518 1 560 end
 arbm-bormod 0.7518 1 1 0 5000 100 3 550.0e-6 560 end

450 ppm boron (wt) in moderator

end comp

fuel-pin-cell geometry:

squarepitch 1.4300 0.929 1 3 1.072 2 0.948 0 end

assembly and cycle parameters:

npin/assm=204 fuelnght=820.74 ncycles=1 nlib/cyc=5
 printlevel=5 lightel=9 inplevel=2 numztotal=5 end
 3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470
 power=38.61 burn=215 down=1825 end
 o 135.0 cr 5.9 mn 0.33
 fe 13.0 co 0.075 ni 9.9
 zr 221.0 nb 0.71 sn 3.6

end

mih87c07less100deg.input

=sas2h parm=skipshipdata

Mihama-3, 7, 33.7 GWd/MTU, 87c07, June 97

'mixtures of fuel-pin-cell

44group latticecell

uo2 1 den=9.996 1 822

92234 0.0295 92235 3.21 92236 0.0327 92238 96.727 end

kr-83 1 0 1-20 822 end

kr-85 1 0 1-20 822 end

y-89 1 0 1-20 822 end

sr-90 1 0 1-20 822 end

zr-93 1 0 1-20 822 end

zr-94 1 0 1-20 822 end

zr-95 1 0 1-20 822 end

nb-94 1 0 1-20 822 end

mo-95 1 0 1-20 822 end

tc-99 1 0 1-20 822 end

ru-101 1 0 1-20 822 end

ru-106 1 0 1-20 822 end

rh-103 1 0 1-20 822 end

rh-105 1 0 1-20 822 end

pd-105 1 0 1-20 822 end

pd-108 1 0 1-20 822 end

ag-109 1 0 1-20 822 end

sb-124 1 0 1-20 822 end

xe-131 1 0 1-20 822 end

xe-132 1 0 1-20 822 end

xe-135 1 0 1-20 822 end

xe-136 1 0 1-20 822 end

cs-134 1 0 1-20 822 end

cs-135 1 0 1-20 822 end

cs-137 1 0 1-20 822 end

ba-136 1 0 1-20 822 end

la-139 1 0 1-20 822 end

pr-141 1 0 1-20 822 end

pr-143 1 0 1-20 822 end

ce-144 1 0 1-20 822 end

nd-143 1 0 1-20 822 end

nd-145 1 0 1-20 822 end

nd-147 1 0 1-20 822 end

pm-147 1 0 1-20 822 end

pm-148 1 0 1-20 822 end

sm-147 1 0 1-20 822 end

sm-149 1 0 1-20 822 end

sm-150 1 0 1-20 822 end

sm-151 1 0 1-20 822 end

sm-152 1 0 1-20 822 end

eu-153 1 0 1-20 822 end

eu-154 1 0 1-20 822 end

eu-155 1 0 1-20 822 end

gd-155 1 0 1-20 822 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40

40000 98.18 2 1.0 601 end

h2o 3 den=0.7510 1 561 end

arbm-bormod 0.7510 1 1 0 0 5000 100 3 450.0e-6 561 end

end comp

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

npin/assm=204 fuelnght=820.74 ncycles=5 nlib/cyc=5

printlevel=5 lightel=9 inlevel=2 numztotal=5 end

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

power=28.13 burn=215.0 down=388 end

power=39.91 burn=157.0 down=9.0 end

power=39.91 burn=170.0 down=176 end

power=38.99 burn=352.0 down=0 end

power=31.77 burn=28.00 down=1825 end

o 135.0 cr 5.9 mn 0.33

fe 13.0 co 0.075 ni 9.9

zr 221.0 nb 0.71 sn 3.6

end

mih87c07plus100boron.input

=sas2h parm=skipshipdata

Mihama-3, 7, 33.7 GWd/MTU, 87c07, June 97

'mixtures of fuel-pin-cell

44group latticecell

uo2 1 den=9.996 1 922

92234 0.0295 92235 3.21 92236 0.0327 92238 96.727 end

kr-83 1 0 1-20 922 end

kr-85 1 0 1-20 922 end

y-89 1 0 1-20 922 end

sr-90 1 0 1-20 922 end

zr-93 1 0 1-20 922 end

zr-94 1 0 1-20 922 end

zr-95 1 0 1-20 922 end

nb-94 1 0 1-20 922 end

mo-95 1 0 1-20 922 end

tc-99 1 0 1-20 922 end

ru-101 1 0 1-20 922 end

ru-106 1 0 1-20 922 end

rh-103 1 0 1-20 922 end

rh-105 1 0 1-20 922 end

pd-105 1 0 1-20 922 end

pd-108 1 0 1-20 922 end

ag-109 1 0 1-20 922 end

sb-124 1 0 1-20 922 end

xe-131 1 0 1-20 922 end

xe-132 1 0 1-20 922 end

xe-135 1 0 1-20 922 end

xe-136 1 0 1-20 922 end

cs-134 1 0 1-20 922 end

cs-135 1 0 1-20 922 end

cs-137 1 0 1-20 922 end

ba-136 1 0 1-20 922 end

la-139 1 0 1-20 922 end

pr-141 1 0 1-20 922 end

pr-143 1 0 1-20 922 end

ce-144 1 0 1-20 922 end

nd-143 1 0 1-20 922 end

nd-145 1 0 1-20 922 end

nd-147 1 0 1-20 922 end

pm-147 1 0 1-20 922 end

pm-148 1 0 1-20 922 end

sm-147 1 0 1-20 922 end

sm-149 1 0 1-20 922 end

sm-150 1 0 1-20 922 end

sm-151 1 0 1-20 922 end

sm-152 1 0 1-20 922 end

eu-153 1 0 1-20 922 end

eu-154 1 0 1-20 922 end

eu-155 1 0 1-20 922 end

gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40

40000 98.18 2 1.0 601 end

h2o 3 den=0.7510 1 561 end

arbm-bormod 0.7510 1 1 0 0 5000 100 3 550.0e-6 561 end

end comp

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

npin/assm=204 fuelnght=820.74 ncycles=5 nlib/cyc=5

printlevel=5 lightel=9 inplevel=2 numztotal=5 end

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

power=28.13 burn=215.0 down=388 end

power=39.91 burn=157.0 down=9.0 end

power=39.91 burn=170.0 down=176 end

power=38.99 burn=352.0 down=0 end

power=31.77 burn=28.00 down=1825 end

o 135.0 cr 5.9 mn 0.33

fe 13.0 co 0.075 ni 9.9

zr 221.0 nb 0.71 sn 3.6

end

mih86b02.sum

```

0.....
:
:          SCALE4.3  Bulletin  Board
:          -----
:
:          Welcome to SCALE-4.3.
:
:.....
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  Mihama-3, 86b02 0, 8.3 Gwd/MTU, 86b02, June 97

```

mixtures of fuel-pin-unitcell:

44group latticecell

```

uo2 1 den=9.996 1 922
92234 0.0285 92235 3.208 92236 0.0208 92238 96.742 end
kr-83 1 0 1-20 922 end
kr-85 1 0 1-20 922 end
y-89 1 0 1-20 922 end
sr-90 1 0 1-20 922 end
zr-93 1 0 1-20 922 end
zr-94 1 0 1-20 922 end
zr-95 1 0 1-20 922 end
nb-94 1 0 1-20 922 end
mo-95 1 0 1-20 922 end
tc-99 1 0 1-20 922 end
ru-101 1 0 1-20 922 end
ru-106 1 0 1-20 922 end
rh-103 1 0 1-20 922 end
rh-105 1 0 1-20 922 end
pd-105 1 0 1-20 922 end
pd-108 1 0 1-20 922 end
ag-109 1 0 1-20 922 end
sb-124 1 0 1-20 922 end
xe-131 1 0 1-20 922 end
xe-132 1 0 1-20 922 end
xe-135 1 0 1-20 922 end
xe-136 1 0 1-20 922 end
cs-134 1 0 1-20 922 end
cs-135 1 0 1-20 922 end
cs-137 1 0 1-20 922 end
ba-136 1 0 1-20 922 end
la-139 1 0 1-20 922 end
pr-141 1 0 1-20 922 end
pr-143 1 0 1-20 922 end
ce-144 1 0 1-20 922 end
nd-143 1 0 1-20 922 end
nd-145 1 0 1-20 922 end
nd-147 1 0 1-20 922 end
pm-147 1 0 1-20 922 end
pm-148 1 0 1-20 922 end
sm-147 1 0 1-20 922 end
sm-149 1 0 1-20 922 end
sm-150 1 0 1-20 922 end
sm-151 1 0 1-20 922 end
sm-152 1 0 1-20 922 end
eu-153 1 0 1-20 922 end
eu-154 1 0 1-20 922 end
eu-155 1 0 1-20 922 end
qd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 600 end
h2o 3 den=0.7518 1 560 end
arbm-bormod 0.7518 1 1 0 0 5000 100 3 450.0e-6 560 end

```

450 ppm boron (wt) in moderator
end comp

fuel-pin-cell geometry:

squarepitch 1.4300 0.929 1 3 1.072 2 0.948 0 end

assembly and cycle parameters:

```

npin/assm=204 fuelnght=820.74 ncycles=1 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numxtotal=5 end
3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470
power=38.61 burn=215 down=1825 end
o 135.0 cr 5.9 sm 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

```

```

1  SSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  2222222222  hh  hh
SSSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  222222222222  hh  hh
SS  SS  AA  AA  SS  SS  22  22  hh  hh
SS  SS  AA  AA  SS  SS  22  22  hh  hh
SS  SS  AA  AA  SS  SS  22  22  hh  hh
SSSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  22  hhhhhhhhhhhh
SSSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  22  hhhhhhhhhhhh
SS  SS  AA  AA  SS  SS  22  hh  hh
SS  SS  AA  AA  SS  SS  22  hh  hh
SS  SS  AA  AA  SS  SS  22  hh  hh

```


mih86g03.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  Mihama-3, 3, 21.29 GWD/MTU, 86g03, June 97

'mixtures of fuel-pin-cell
44group latticecell

uo2 1 den=9.996 1 933
92234 0.0285 92235 3.203 92236 0.0109 92238 96.757 end
kr-83 1 0 1-20 922 end
kr-85 1 0 1-20 922 end
y-89 1 0 1-20 922 end
sr-90 1 0 1-20 922 end
zr-93 1 0 1-20 922 end
zr-94 1 0 1-20 922 end
zr-95 1 0 1-20 922 end
nb-94 1 0 1-20 922 end
mo-95 1 0 1-20 922 end
tc-99 1 0 1-20 922 end
ru-101 1 0 1-20 922 end
ru-106 1 0 1-20 922 end
rh-103 1 0 1-20 922 end
rh-105 1 0 1-20 922 end
pd-105 1 0 1-20 922 end
pd-108 1 0 1-20 922 end
ag-109 1 0 1-20 922 end
sb-124 1 0 1-20 922 end
xe-131 1 0 1-20 922 end
xe-132 1 0 1-20 922 end
xe-135 1 0 1-20 922 end
xe-136 1 0 1-20 922 end
cs-134 1 0 1-20 922 end
cs-135 1 0 1-20 922 end
cs-137 1 0 1-20 922 end
ba-136 1 0 1-20 922 end
la-139 1 0 1-20 922 end
pr-141 1 0 1-20 922 end
pr-143 1 0 1-20 922 end
ce-144 1 0 1-20 922 end
nd-143 1 0 1-20 922 end
nd-145 1 0 1-20 922 end
nd-147 1 0 1-20 922 end
pm-147 1 0 1-20 922 end
pm-148 1 0 1-20 922 end
sm-147 1 0 1-20 922 end
sm-149 1 0 1-20 922 end
sm-150 1 0 1-20 922 end
sm-151 1 0 1-20 922 end
sm-152 1 0 1-20 922 end
eu-153 1 0 1-20 922 end
eu-154 1 0 1-20 922 end
eu-155 1 0 1-20 922 end
gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 625 end
h2o 3 den=0.6995 1 585 end
arbm-bormod 0.6995 1 1 0 0 5000 100 3 450.0e-6 585 end
end comp

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

npin/assm=204 fuelnght=820.74 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

power=31.95 burn=215.0 down=388 end
power=44.10 burn=157.0 down=9.0 end
power=44.10 burn=170.0 down=1825 end

o 135.0 cr 5.9 mn 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

1 ssssssssss aaaaaaaaaa ssssssssss 2222222222 hh hh
  ssssssssss aaaaaaaaaa ssssssssss 2222222222 hh hh
  ss aa aa ss ss 22 22 hh hh
  ss aa aa ss ss 22 22 hh hh
  ss aa aa ss ss 22 22 hh hh
  ssssssssss aaaaaaaaaa ssssssssss 22 hhhhhhhhhhhh
  ssssssssss aaaaaaaaaa ssssssssss 22 hhhhhhhhhhhh
  ss aa aa ss ss 22 hh hh
  ss aa aa ss ss 22 hh hh
  ss aa aa ss ss 22 hh hh
  ssssssssss aa aa ssssssssss 2222222222 hh hh
  ssssssssss aa aa ssssssssss 2222222222 hh hh

0 nn nn iiiiiiiiii cccccccccc hh hh oooooooooooo 11
  nnn nn iiiiiiiiii cccccccccc hh hh oooooooooooo 11
  nnnn nn ii cccccccccc hh hh oo oo 11

```


mih86g05.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
Mihama-3, 2, 15.36 GWD/MTU, 86g05, June 97

'mixtures of fuel-pin-cell
44group latticecell

uo2 1 den=9.996 1 922
92234 0.0285 92235 3.203 92236 0.0109 92238 96.757 end
kr-83 1 0 1-20 922 end
kr-85 1 0 1-20 922 end
y-89 1 0 1-20 922 end
sr-90 1 0 1-20 922 end
zr-93 1 0 1-20 922 end
zr-94 1 0 1-20 922 end
zr-95 1 0 1-20 922 end
nb-94 1 0 1-20 922 end
mo-95 1 0 1-20 922 end
tc-99 1 0 1-20 922 end
ru-101 1 0 1-20 922 end
ru-106 1 0 1-20 922 end
rh-103 1 0 1-20 922 end
rh-105 1 0 1-20 922 end
pd-105 1 0 1-20 922 end
pd-108 1 0 1-20 922 end
ag-109 1 0 1-20 922 end
sb-124 1 0 1-20 922 end
xe-131 1 0 1-20 922 end
xe-132 1 0 1-20 922 end
xe-135 1 0 1-20 922 end
xe-136 1 0 1-20 922 end
cs-134 1 0 1-20 922 end
cs-135 1 0 1-20 922 end
cs-137 1 0 1-20 922 end
ba-136 1 0 1-20 922 end
la-139 1 0 1-20 922 end
pr-141 1 0 1-20 922 end
pr-143 1 0 1-20 922 end
ce-144 1 0 1-20 922 end
nd-143 1 0 1-20 922 end
nd-145 1 0 1-20 922 end
nd-147 1 0 1-20 922 end
pm-147 1 0 1-20 922 end
pm-148 1 0 1-20 922 end
sm-147 1 0 1-20 922 end
sm-149 1 0 1-20 922 end
sm-150 1 0 1-20 922 end
sm-151 1 0 1-20 922 end
sm-152 1 0 1-20 922 end
eu-153 1 0 1-20 922 end
eu-154 1 0 1-20 922 end
eu-155 1 0 1-20 922 end
qd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 612 end
h2o 3 den=0.7298 1 572 end
arbm-bormod 0.7298 1 1 0 0 5000 100 3 450.0e-6 .572 end
end comp

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

npin/assm=204 fuelnght=820.74 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

power=22.99 burn=215.0 down=388 end
power=31.87 burn=157.0 down=9.0 end
power=31.87 burn=170.0 down=1825 end

o 135.0 cr 5.9 mn 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

1 sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
ssssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
ss ss aa aa ss ss 22 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
ssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ssssssssssss aa aa sssssssssss 2222222222 hh hh
ssssssssssss aa aa sssssssssss 2222222222 hh hh

0 nn nn iiiiiiiiii cccccccccc hh hh oooooooooo 11
nnn nn iiiiiiiiii cccccccccc hh hh oooooooooo 11

```


mih86g07.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....
1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
Mihama-3, 2, 14.66 Gwd/MTU 86g07, June 97

'mixtures of fuel-pin-cell
44group latticecell

uo2 1 den=9.996 1 922
92234 0.0285 92235 3.203 92236 0.0109 92238 96.757 end
kr-83 1 0 1-20 922 end
kr-85 1 0 1-20 922 end
y-89 1 0 1-20 922 end
sr-90 1 0 1-20 922 end
zr-93 1 0 1-20 922 end
zr-94 1 0 1-20 922 end
zr-95 1 0 1-20 922 end
nb-94 1 0 1-20 922 end
mo-95 1 0 1-20 922 end
tc-99 1 0 1-20 922 end
ru-101 1 0 1-20 922 end
ru-106 1 0 1-20 922 end
rh-103 1 0 1-20 922 end
rh-105 1 0 1-20 922 end
pd-105 1 0 1-20 922 end
pd-108 1 0 1-20 922 end
ag-109 1 0 1-20 922 end
sb-124 1 0 1-20 922 end
xe-131 1 0 1-20 922 end
xe-132 1 0 1-20 922 end
xe-135 1 0 1-20 922 end
xe-136 1 0 1-20 922 end
cs-134 1 0 1-20 922 end
cs-135 1 0 1-20 922 end
cs-137 1 0 1-20 922 end
ba-136 1 0 1-20 922 end
la-139 1 0 1-20 922 end
pr-141 1 0 1-20 922 end
pr-143 1 0 1-20 922 end
ce-144 1 0 1-20 922 end
nd-143 1 0 1-20 922 end
nd-145 1 0 1-20 922 end
nd-147 1 0 1-20 922 end
pm-147 1 0 1-20 922 end
pm-148 1 0 1-20 922 end
sm-147 1 0 1-20 922 end
sm-149 1 0 1-20 922 end
sm-150 1 0 1-20 922 end
sm-151 1 0 1-20 922 end
sm-152 1 0 1-20 922 end
eu-153 1 0 1-20 922 end
eu-154 1 0 1-20 922 end
eu-155 1 0 1-20 922 end
gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 625 end
h2o 3 den=0.6995 1 585 end
arbm-bormod 0.6995 1 1 0 0 5000 100 3 450.0e-6 585 end
end comp

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

npin/assm=204 fuelnght=820.74 ncycles=3 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end

3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

power=22.00 burn=215.0 down=388 end
power=30.37 burn=157.0 down=9.0 end
power=30.37 burn=170.0 down=1825 end

o 135.0 cr 5.9 mn 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

1 *****
*****
ss ss aa aa ss ss 22 hh hh
ss ss aa aa ss ss 22 hh hh
ss ss aa aa ss ss 22 hh hh
ss ss aa aa ss ss 22 hh hh
*****
*****
ss aa aa ss 22 hh hh
ss aa aa ss 22 hh hh
ss ss aa aa ss ss 22 hh hh
*****
*****
*****
nn nn iiiiiiiiii cccccccccc hh hh oooooooooo 11
nnn nn iiiiiiiiii cccccccccc hh hh oooooooooo 11

```


mih87c03.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....

```

```

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
Mihama-3, 5, 29.5 GWD/MTU 87c03, June 97

```

```

mixtures of fuel pin cell
44group latticecell

```

```

uo2 1 den=9.996 1 922
92234 0.0295 92235 3.21 92236 0.0327 92238 96.727 end
kr-83 1 0 1-20 922 end
kr-85 1 0 1-20 922 end
y-89 1 0 1-20 922 end
sr-90 1 0 1-20 922 end
zr-93 1 0 1-20 922 end
zr-94 1 0 1-20 922 end
zr-95 1 0 1-20 922 end
nb-94 1 0 1-20 922 end
mo-95 1 0 1-20 922 end
tc-99 1 0 1-20 922 end
ru-101 1 0 1-20 922 end
ru-106 1 0 1-20 922 end
rh-103 1 0 1-20 922 end
rh-105 1 0 1-20 922 end
pd-105 1 0 1-20 922 end
pd-108 1 0 1-20 922 end
ag-109 1 0 1-20 922 end
sb-124 1 0 1-20 922 end
xe-131 1 0 1-20 922 end
xe-132 1 0 1-20 922 end
xe-135 1 0 1-20 922 end
xe-136 1 0 1-20 922 end
cs-134 1 0 1-20 922 end
cs-135 1 0 1-20 922 end
cs-137 1 0 1-20 922 end
ba-136 1 0 1-20 922 end
la-139 1 0 1-20 922 end
pr-141 1 0 1-20 922 end
pr-143 1 0 1-20 922 end
ce-144 1 0 1-20 922 end
nd-143 1 0 1-20 922 end
nd-145 1 0 1-20 922 end
nd-147 1 0 1-20 922 end
pm-147 1 0 1-20 922 end
pm-148 1 0 1-20 922 end
sm-147 1 0 1-20 922 end
sm-149 1 0 1-20 922 end
sm-150 1 0 1-20 922 end
sm-151 1 0 1-20 922 end
sm-152 1 0 1-20 922 end
eu-153 1 0 1-20 922 end
eu-154 1 0 1-20 922 end
eu-155 1 0 1-20 922 end
gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 600 end
h2o 3 den=0.7518 1 560 end
arbm-borrm0d 0.7518 1 1 0 0 5000 100 3 450.0e-6 560 end
end comp

```

```

squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

```

```

npin/assm=204 fuelnght=820.74 ncycles=5 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

```

```

power=24.61 burn=215.0 down=388 end
power=34.92 burn=157.0 down=9.0 end
power=34.92 burn=170.0 down=176 end
power=34.15 burn=352.0 down=0 end
power=27.47 burn=28.00 down=1825 end

```

```

o 135.0 cr 5.9 mn 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

```

```

1 sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 222222222222 hh hh
  ss ss aa aa ss ss 22 22 hh hh
  ss aa aa aa ss ss 22 hh hh
  ss aa aa aa ss ss 22 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
  ss aa aa aa ss ss 22 hh hh
  ss ss aa aa ss ss 22 hh hh
  sssssssssss aa aa sssssssssss 222222222222 hh hh
  sssssssssss aa aa sssssssssss 222222222222 hh hh

```


		basis =single reactor assembly			
		912.5 d	1216.7 d	1520.8 d	1825.0 d
o 16	initial	304.2 d	608.3 d	912.5 d	1216.7 d
	1.35E+05	1.35E+05	1.35E+05	1.35E+05	1.35E+05
	nuclide concentrations, grams				
	basis =single reactor assembly				
	912.5 d 1216.7 d 1520.8 d 1825.0 d				
mo 95	initial	304.2 d	608.3 d	912.5 d	1216.7 d
	1.25E+01	1.51E+01	1.52E+01	1.52E+01	1.52E+01
tc 99	3.31E-05	3.35E-05	3.35E-05	3.35E-05	3.35E-05
total	3.90E+05	3.90E+05	3.90E+05	3.90E+05	3.90E+05
	nuclide concentrations, grams				
	basis =single reactor assembly				
	912.5 d 1216.7 d 1520.8 d 1825.0 d				
u233	initial	304.2 d	608.3 d	912.5 d	1216.7 d
	1.79E-03	1.90E-03	2.02E-03	2.13E-03	2.24E-03
u234	1.86E+02	1.86E+02	1.87E+02	1.88E+02	1.89E+02
u235	9.40E+03	9.40E+03	9.40E+03	9.40E+03	9.40E+03
u236	4.08E+03	4.08E+03	4.08E+03	4.08E+03	4.08E+03
u238	9.46E+05	9.46E+05	9.46E+05	9.46E+05	9.46E+05
np237	3.71E-02	3.78E-02	3.78E-02	3.79E-02	3.79E-02
pu236	4.87E-04	4.01E-04	3.29E-04	2.69E-04	2.21E-04
pu238	1.08E-02	1.16E-02	1.17E-02	1.17E-02	1.16E-02
pu239	5.04E+03	5.11E+03	5.11E+03	5.11E+03	5.11E+03
pu240	2.05E+03	2.05E+03	2.05E+03	2.05E+03	2.05E+03
pu241	1.07E-03	1.03E-03	9.90E-04	9.51E-04	9.14E-04
pu242	3.81E-02	3.81E-02	3.81E-02	3.81E-02	3.81E-02
am241	3.36E+01	7.59E+01	1.16E+02	1.55E+02	1.93E+02
am242m	6.35E-01	6.33E-01	6.30E-01	6.27E-01	6.25E-01
am243	6.57E+01	6.58E+01	6.58E+01	6.57E+01	6.57E+01
total	9.69E+05	9.69E+05	9.69E+05	9.69E+05	9.69E+05
	element concentrations, grams				
	nuclide concentrations, grams				
	basis =single reactor assembly				
	912.5 d 1216.7 d 1520.8 d 1825.0 d				
mo 95	initial	304.2 d	608.3 d	912.5 d	1216.7 d
	5.91E+02	6.89E+02	6.95E+02	6.95E+02	6.95E+02
	nuclide concentrations, grams				
	basis =single reactor assembly				
	912.5 d 1216.7 d 1520.8 d 1825.0 d				
tc 99	initial	304.2 d	608.3 d	912.5 d	1216.7 d
	7.26E+02	7.29E+02	7.29E+02	7.29E+02	7.29E+02
ru101	6.88E+02	6.88E+02	6.88E+02	6.88E+02	6.88E+02
rh103	3.97E+02	4.39E+02	4.39E+02	4.39E+02	4.39E+02
ag109	7.46E+01	7.47E+01	7.47E+01	7.47E+01	7.47E+01
	nuclide concentrations, grams				
	basis =single reactor assembly				
	912.5 d 1216.7 d 1520.8 d 1825.0 d				
nd143	initial	304.2 d	608.3 d	912.5 d	1216.7 d
	7.33E+02	7.52E+02	7.52E+02	7.52E+02	7.52E+02
nd145	6.19E+02	6.19E+02	6.19E+02	6.19E+02	6.19E+02
sm147	8.03E+01	1.15E+02	1.43E+02	1.66E+02	1.84E+02
sm149	2.06E+00	3.12E+00	3.12E+00	3.12E+00	3.12E+00
sm150	2.56E+02	2.56E+02	2.56E+02	2.56E+02	2.56E+02
sm151	1.27E+01	1.28E+01	1.27E+01	1.26E+01	1.25E+01
sm152	1.45E-02	9.70E-02	1.79E-01	2.60E-01	3.41E-01
	1.20E+02	1.20E+02	1.20E+02	1.20E+02	1.20E+02
	nuclide concentrations, grams				
	basis =single reactor assembly				
	912.5 d 1216.7 d 1520.8 d 1825.0 d				
eu153	initial	304.2 d	608.3 d	912.5 d	1216.7 d
	9.78E+01	9.85E+01	9.85E+01	9.85E+01	9.85E+01
gd155	3.50E-02	5.54E-01	1.01E+00	1.42E+00	1.78E+00
total	3.03E+04	3.03E+04	3.03E+04	3.03E+04	3.03E+04

mih87c04.sum

```

0.....
:
:                SCALE4.3  Bulletin  Board
:                -----
:                Welcome to SCALE-4.3.
:.....
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
  Mihama-3, 6, 32.2 GWD/MTU, 87c04, June 97
  mixtures of fuel-pin-cell
  44group latticecell
  .
  uo2 1 den=9.996 1 922
    92234 0.0295 92235 3.21 92236 0.0327 92238 96.727 end
  kr-83 1 0 1-20 922 end
  kr-85 1 0 1-20 922 end
  y-89 1 0 1-20 922 end
  sr-90 1 0 1-20 922 end
  zr-93 1 0 1-20 922 end
  zr-94 1 0 1-20 922 end
  zr-95 1 0 1-20 922 end
  nb-94 1 0 1-20 922 end
  mo-95 1 0 1-20 922 end
  tc-99 1 0 1-20 922 end
  ru-101 1 0 1-20 922 end
  ru-106 1 0 1-20 922 end
  rh-103 1 0 1-20 922 end
  rh-105 1 0 1-20 922 end
  pd-105 1 0 1-20 922 end
  pd-108 1 0 1-20 922 end
  ag-109 1 0 1-20 922 end
  sb-124 1 0 1-20 922 end
  xe-131 1 0 1-20 922 end
  xe-132 1 0 1-20 922 end
  xe-135 1 0 1-20 922 end
  xe-136 1 0 1-20 922 end
  ca-134 1 0 1-20 922 end
  cs-135 1 0 1-20 922 end
  cs-137 1 0 1-20 922 end
  ba-136 1 0 1-20 922 end
  la-139 1 0 1-20 922 end
  pr-141 1 0 1-20 922 end
  pr-143 1 0 1-20 922 end
  ce-144 1 0 1-20 922 end
  nd-143 1 0 1-20 922 end
  nd-145 1 0 1-20 922 end
  nd-147 1 0 1-20 922 end
  pm-147 1 0 1-20 922 end
  pm-148 1 0 1-20 922 end
  sm-147 1 0 1-20 922 end
  sm-149 1 0 1-20 922 end
  sm-150 1 0 1-20 922 end
  sm-151 1 0 1-20 922 end
  sm-152 1 0 1-20 922 end
  eu-153 1 0 1-20 922 end
  eu-154 1 0 1-20 922 end
  eu-155 1 0 1-20 922 end
  gd-155 1 0 1-20 922 end

  arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
    40000 98.18 2 1.0 607 end
  h2o 3 den=0.7390 1 567 end
  arbm-bormod 0.7390 1 1 0 0 5000 100 3 450.0e-6 567 end
  end comp
  .
  squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end
  .
  npin/assm=204 fuelnght=820.74 ncycles=5 nlib/cyc=5
  printlevel=5 lightel=9 inplevel=2 numztotal=5 end
  .
  3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470
  .
  power=26.87 burn=215.0 down=388 end
  power=38.12 burn=157.0 down=9.0 end
  power=38.12 burn=170.0 down=176 end
  power=37.25 burn=352.0 down=0 end
  power=30.35 burn=28.00 down=1825 end

  o 135.0 cr 5.9 mn 0.33
  fe 13.0 co 0.075 ni 9.9
  zr 221.0 nb 0.71 sn 3.6

1  sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
  ss aa aa ss 22 22 hh hh
  ss aa aa ss 22 22 hh hh
  ss aa aa ss 22 22 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  sssssssssss aa aa sssssssssss 2222222222 hh hh
  sssssssssss aa aa sssssssssss 2222222222 hh hh

0
nn nn iiiiiiiiii ccccccccc hh hh oooooooooo 11

```


mih87c07.sum

```

0.....
:
:          SCALE4.3  Bulletin  Board
:          -----
:
:          Welcome to SCALE-4.3.
:
:.....
1      primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h      will be called
  Mihama-3, 7, 33.7 Gwd/MTU, 87c07, June 97
  'mixtures of fuel-pin-cell
  44group latticecell
  :
  uo2 1 den=9.996 1 922
      92234 0.0295 92235 3.21 92236 0.0327 92238 96.727 end
kr-83 1 0 1-20 922 end
kr-85 1 0 1-20 922 end
y-89 1 0 1-20 922 end
sr-90 1 0 1-20 922 end
zr-93 1 0 1-20 922 end
zr-94 1 0 1-20 922 end
zr-95 1 0 1-20 922 end
nb-94 1 0 1-20 922 end
mo-95 1 0 1-20 922 end
tc-99 1 0 1-20 922 end
ru-101 1 0 1-20 922 end
ru-106 1 0 1-20 922 end
rh-103 1 0 1-20 922 end
rh-105 1 0 1-20 922 end
pd-105 1 0 1-20 922 end
pd-108 1 0 1-20 922 end
ag-109 1 0 1-20 922 end
sb-124 1 0 1-20 922 end
xe-131 1 0 1-20 922 end
xe-132 1 0 1-20 922 end
xe-135 1 0 1-20 922 end
xe-136 1 0 1-20 922 end
cs-134 1 0 1-20 922 end
cs-135 1 0 1-20 922 end
cs-137 1 0 1-20 922 end
ba-136 1 0 1-20 922 end
la-139 1 0 1-20 922 end
pr-141 1 0 1-20 922 end
pr-143 1 0 1-20 922 end
ce-144 1 0 1-20 922 end
nd-143 1 0 1-20 922 end
nd-145 1 0 1-20 922 end
nd-147 1 0 1-20 922 end
pm-147 1 0 1-20 922 end
pm-148 1 0 1-20 922 end
sm-147 1 0 1-20 922 end
sm-149 1 0 1-20 922 end
sm-150 1 0 1-20 922 end
sm-151 1 0 1-20 922 end
sm-152 1 0 1-20 922 end
eu-153 1 0 1-20 922 end
eu-154 1 0 1-20 922 end
eu-155 1 0 1-20 922 end
gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
            40000 98.18 2 1.0 601 end
h2o 3 den=0.7510 1 561 end
arbm-bormod 0.7510 1 1 0 0 5000 100 3 450.0e-6 561 end
end comp
:
squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end
:
:
npin/assm=204 fuelnght=820.74 ncycles=5 nlib/cyc=5
printlevel=5 lightel=9 inplevel=2 numztotal=5 end
:
3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470
:
power=28.13 burn=215.0 down=388 end
power=39.91 burn=157.0 down=9.0 end
power=39.91 burn=170.0 down=176 end
power=38.99 burn=352.0 down=0 end
power=31.77 burn=28.00 down=1825 end
:
o 135.0 cr 5.9 mn 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

1  sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 2222222222 hh hh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
  sssssssssss aaaaaaaaaa sssssssssss 22 hhhhhhhhhhhh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  ss aa aa ss 22 hh hh
  sssssssssss aa aa sssssssssss 222222222222 hh hh
  sssssssssss aa aa sssssssssss 222222222222 hh hh

0
nn nn iiiiiiiiii cccccccccc hh hh oooooooooo 11

```


mih87c08.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....

1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
- module sas2h will be called
  Mihama-3, 8, 34.2 Gwd/MTU, 87c08, June 97

  mixtures of fuel-pin-cell
  44group latticecell

  uo2 1 den=9.996 1 922
    92234 0.0295 92235 3.21 92236 0.0327 92238 96.727 end
  kr-83 1 0 1-20 922 end
  kr-85 1 0 1-20 922 end
  y-89 1 0 1-20 922 end
  sr-90 1 0 1-20 922 end
  zr-93 1 0 1-20 922 end
  zr-94 1 0 1-20 922 end
  zr-95 1 0 1-20 922 end
  nb-94 1 0 1-20 922 end
  mo-95 1 0 1-20 922 end
  tc-99 1 0 1-20 922 end
  ru-101 1 0 1-20 922 end
  ru-106 1 0 1-20 922 end
  rh-103 1 0 1-20 922 end
  rh-105 1 0 1-20 922 end
  pd-105 1 0 1-20 922 end
  pd-108 1 0 1-20 922 end
  ag-109 1 0 1-20 922 end
  sb-124 1 0 1-20 922 end
  xe-131 1 0 1-20 922 end
  xe-132 1 0 1-20 922 end
  xe-135 1 0 1-20 922 end
  xe-136 1 0 1-20 922 end
  cs-134 1 0 1-20 922 end
  cs-135 1 0 1-20 922 end
  cs-137 1 0 1-20 922 end
  ba-136 1 0 1-20 922 end
  la-139 1 0 1-20 922 end
  pr-141 1 0 1-20 922 end
  pr-143 1 0 1-20 922 end
  ce-144 1 0 1-20 922 end
  nd-143 1 0 1-20 922 end
  nd-145 1 0 1-20 922 end
  nd-147 1 0 1-20 922 end
  pm-147 1 0 1-20 922 end
  pm-148 1 0 1-20 922 end
  sm-147 1 0 1-20 922 end
  sm-149 1 0 1-20 922 end
  sm-150 1 0 1-20 922 end
  sm-151 1 0 1-20 922 end
  sm-152 1 0 1-20 922 end
  eu-153 1 0 1-20 922 end
  eu-154 1 0 1-20 922 end
  eu-155 1 0 1-20 922 end
  gd-155 1 0 1-20 922 end

  arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
    40000 98.18 2 1.0 626 end
  h2o 3 den=0.6984 1 586 end
  arbm-bormod 0.6984 1 1 0 0 5000 100 3 450.0e-6 586 end
  end comp

  squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

  mpin/assm=204 fuelnght=820.74 ncycles=5 nlib/cyc=5
  printlevel=5 lightel=9 inplevel=2 numztotal=5 end

  3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

  power=28.65 burn=215.0 down=388 end
  power=40.62 burn=157.0 down=9.0 end
  power=40.62 burn=170.0 down=176 end
  power=39.72 burn=352.0 down=0 end
  power=31.85 burn=28.00 down=1825 end

  o 135.0 cr 5.9 mn 0.33
  fe 13.0 co 0.075 ni 9.9
  zr 221.0 nb 0.71 sn 3.6

1  SSSSSSSSSS aaaaaaaaaa SSSSSSSSSS 2222222222 hh hh
  SSSSSSSSSS aaaaaaaaaa SSSSSSSSSS 2222222222 hh hh
  SS aa aa aa SS 22 22 hh hh
  SS aa aa aa SS 22 22 hh hh
  SS aa aa aa SS 22 22 hh hh
  SSSSSSSSSS aaaaaaaaaa SSSSSSSSSS 22 hhhhhhhhhhhh
  SSSSSSSSSS aaaaaaaaaa SSSSSSSSSS 22 hhhhhhhhhhhh
  SS aa aa aa SS 22 hh hh
  SS aa aa aa SS 22 hh hh
  SS aa aa aa SS 22 hh hh
  SSSSSSSSSS aa aa SSSSSSSSSS 2222222222 hh hh
  SSSSSSSSSS aa aa SSSSSSSSSS 2222222222 hh hh

0

nn nn iiiiiiiiii ccccccccc hh hh oooooooooo 11

```


mih86b02less100deg.sum

```

.....
SCALE4.3 Bulletin Board
-----
Welcome to SCALE-4.3.
.....
1 primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
  module sas2h will be called
  Mihama-3, 86b02 0, 8.3 GWD/MTU, 86b02, June 97

```

```

-----
mixtures of fuel-pin-unitcell:
44group latticecell
uo2 1 den=9.996 1 822
92234 0.0285 92235 3.208 92236 0.0208 92238 96.742 end
kr-83 1 0 1-20 822 end
kr-85 1 0 1-20 822 end
y-89 1 0 1-20 822 end
sr-90 1 0 1-20 822 end
zr-93 1 0 1-20 822 end
zr-94 1 0 1-20 822 end
zr-95 1 0 1-20 822 end
nb-94 1 0 1-20 822 end
mo-95 1 0 1-20 822 end
tc-99 1 0 1-20 822 end
ru-101 1 0 1-20 822 end
ru-106 1 0 1-20 822 end
rh-103 1 0 1-20 822 end
rh-105 1 0 1-20 822 end
pd-105 1 0 1-20 822 end
pd-108 1 0 1-20 822 end
ag-109 1 0 1-20 822 end
sb-124 1 0 1-20 822 end
xe-131 1 0 1-20 822 end
xe-132 1 0 1-20 822 end
xe-135 1 0 1-20 822 end
xe-136 1 0 1-20 822 end
cs-134 1 0 1-20 822 end
cs-135 1 0 1-20 822 end
cs-137 1 0 1-20 822 end
ba-136 1 0 1-20 822 end
la-139 1 0 1-20 822 end
pr-141 1 0 1-20 822 end
pr-143 1 0 1-20 822 end
ce-144 1 0 1-20 822 end
nd-143 1 0 1-20 822 end
nd-145 1 0 1-20 822 end
nd-147 1 0 1-20 822 end
pm-147 1 0 1-20 822 end
pm-148 1 0 1-20 822 end
sm-147 1 0 1-20 822 end
sm-149 1 0 1-20 822 end
sm-150 1 0 1-20 822 end
sm-151 1 0 1-20 822 end
sm-152 1 0 1-20 822 end
eu-153 1 0 1-20 822 end
eu-154 1 0 1-20 822 end
eu-155 1 0 1-20 822 end
qd-155 1 0 1-20 822 end

```

```

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 600 end
h2o 3 den=0.7518 1 560 end
arbm-bormod 0.7518 1 1 0 0 5000 100 3 450.0e-6 560 end

```

```

450 ppm boron (wt) in moderator
-----
end comp

```

```

fuel-pin-cell geometry:
squarepitch 1.4300 0.929 1 3 1.072 2 0.948 0 end

```

```

-----
assembly and cycle parameters:
npin/assm=204 fuelnght=820.74 ncycles=1 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numztotal=5 end
3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470
power=38.61 burn=215 down=1825 end
o 135.0 cr 5.9 mn 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 sn 3.6

```

```

1  SSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  2222222222  hh  hh
SSSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  2222222222  hh  hh
SS  SS  aa  aa  aa  SS  SS  22  22  hh  hh
SS  SS  aa  aa  aa  SS  SS  22  22  hh  hh
SS  SS  aa  aa  aa  SS  SS  22  22  hh  hh
SSSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  22  hhhhhhhhhhhh
SSSSSSSSSSSS  AAAAAAAAAA  SSSSSSSSSS  22  hhhhhhhhhhhh
SS  SS  aa  aa  aa  SS  SS  22  hh  hh
SS  SS  aa  aa  aa  SS  SS  22  hh  hh
SS  SS  aa  aa  aa  SS  SS  22  hh  hh

```


mih86b02plus100boron.sum

```

.....
*
*          SCALE4.3  Bulletin  Board
*          -----
*
*          Welcome to SCALE-4.3.
*
*
.....
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
  Mihama-3, 86b02 0, 8.3 Gwd/MTU, 86b02, June 97

```

```

-----
mixtures of fuel-pin-unitcell:
44group      latticecell

uo2 1 den=9.996 1 922
92234 0.0285 92235 3.208 92236 0.0208 92238 96.742 end
kr-83 1 0 1-20 922 end
kr-85 1 0 1-20 922 end
y-89 1 0 1-20 922 end
sr-90 1 0 1-20 922 end
zr-93 1 0 1-20 922 end
zr-94 1 0 1-20 922 end
zr-95 1 0 1-20 922 end
nb-94 1 0 1-20 922 end
mo-95 1 0 1-20 922 end
tc-99 1 0 1-20 922 end
ru-101 1 0 1-20 922 end
ru-106 1 0 1-20 922 end
rh-103 1 0 1-20 922 end
rh-105 1 0 1-20 922 end
pd-105 1 0 1-20 922 end
pd-108 1 0 1-20 922 end
ag-109 1 0 1-20 922 end
sb-124 1 0 1-20 922 end
xe-131 1 0 1-20 922 end
xe-132 1 0 1-20 922 end
xe-135 1 0 1-20 922 end
xe-136 1 0 1-20 922 end
cs-134 1 0 1-20 922 end
cs-135 1 0 1-20 922 end
cs-137 1 0 1-20 922 end
ba-136 1 0 1-20 922 end
la-139 1 0 1-20 922 end
pr-141 1 0 1-20 922 end
pr-143 1 0 1-20 922 end
ce-144 1 0 1-20 922 end
nd-143 1 0 1-20 922 end
nd-145 1 0 1-20 922 end
nd-147 1 0 1-20 922 end
pm-147 1 0 1-20 922 end
pm-148 1 0 1-20 922 end
sm-147 1 0 1-20 922 end
sm-149 1 0 1-20 922 end
sm-150 1 0 1-20 922 end
sm-151 1 0 1-20 922 end
sm-152 1 0 1-20 922 end
eu-153 1 0 1-20 922 end
eu-154 1 0 1-20 922 end
eu-155 1 0 1-20 922 end
gd-155 1 0 1-20 922 end

arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
40000 98.18 2 1.0 600 end
h2o 3 den=0.7518 1 560 end
arbm-bormod 0.7518 1 1 0 0 5000 100 3 550.0e-6 560 end

```

```

450 ppm boron (wt) in moderator
-----
end comp

```

```

fuel-pin-cell geometry:
squarepitch 1.4300 0.929 1 3 1.072 2 0.948 0 end

```

```

-----
assembly and cycle parameters:
npin/assm=204 fuelnght=820.74 ncycles=1 nlib/cyc=5
printlevel=5 lightel=9 implevel=2 numstotal=5 end
3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470
power=38.61 burn=215 down=1825 end
o 135.0 ck 5.9 mm 0.33
fe 13.0 co 0.075 ni 9.9
zr 221.0 nb 0.71 an 3.6

```

```

.....
1  #####          #####          #####          222222222222  hh          hh
#####          #####          #####          222222222222  hh          hh
ss          ss          aa          aa          ss          ss          22          22          hh          hh
ss          ss          aa          aa          ss          ss          22          22          hh          hh
ss          ss          aa          aa          ss          ss          22          22          hh          hh
#####          #####          #####          22          hh          hh          hh          hh
#####          #####          #####          22          hh          hh          hh          hh
ss          ss          aa          aa          ss          ss          22          22          hh          hh
ss          ss          aa          aa          ss          ss          22          22          hh          hh
ss          ss          aa          aa          ss          ss          22          22          hh          hh

```


mih87c07less100deg.sum

```

0.....
:
:          SCALE4.3  Bulletin  Board
:          -----
:
:          Welcome to SCALE-4.3.
:
:.....
1  primary module access and input record ( scale driver - 95/03/29 - 09:06:37 )
-  module sas2h will be called
  Mihama-3, 7, 33.7 GWD/MTU, 87c07, June 97
  'mixtures of fuel-pin-cell
  44group latticecell
  .
  uo2 1 den=9.996 1 822
    92234 0.0295 92235 3.21 92236 0.0327 92238 96.727 end
  kr-83 1 0 1-20 822 end
  kr-85 1 0 1-20 822 end
  y-89 1 0 1-20 822 end
  sr-90 1 0 1-20 822 end
  zr-93 1 0 1-20 822 end
  zr-94 1 0 1-20 822 end
  zr-95 1 0 1-20 822 end
  nb-94 1 0 1-20 822 end
  mo-95 1 0 1-20 822 end
  tc-99 1 0 1-20 822 end
  ru-101 1 0 1-20 822 end
  ru-106 1 0 1-20 822 end
  rh-103 1 0 1-20 822 end
  rh-105 1 0 1-20 822 end
  pd-105 1 0 1-20 822 end
  pd-108 1 0 1-20 822 end
  ag-109 1 0 1-20 822 end
  sb-124 1 0 1-20 822 end
  xe-131 1 0 1-20 822 end
  xe-132 1 0 1-20 822 end
  xe-135 1 0 1-20 822 end
  xe-136 1 0 1-20 822 end
  cs-134 1 0 1-20 822 end
  cs-135 1 0 1-20 822 end
  cs-137 1 0 1-20 822 end
  ba-136 1 0 1-20 822 end
  la-139 1 0 1-20 822 end
  pr-141 1 0 1-20 822 end
  pr-143 1 0 1-20 822 end
  ce-144 1 0 1-20 822 end
  nd-143 1 0 1-20 822 end
  nd-145 1 0 1-20 822 end
  nd-147 1 0 1-20 822 end
  pm-147 1 0 1-20 822 end
  pm-148 1 0 1-20 822 end
  sm-147 1 0 1-20 822 end
  sm-149 1 0 1-20 822 end
  sm-150 1 0 1-20 822 end
  sm-151 1 0 1-20 822 end
  sm-152 1 0 1-20 822 end
  eu-153 1 0 1-20 822 end
  eu-154 1 0 1-20 822 end
  eu-155 1 0 1-20 822 end
  gd-155 1 0 1-20 822 end

  arbm-zirc4 6.56 5 0 0 0 8016 0.12 24000 0.10 26000 0.20 50000 1.40
    40000 98.18 2 1.0 601 end
  h2o 3 den=0.7510 1 561 end
  arbm-boromod 0.7510 1 1 0 0 5000 100 3 450.0e-6 561 end
  end comp

  squarepitch 1.430 0.929 1 3 1.072 2 0.948 0 end

  .
  npin/assm=204 fuelnght=820.74 ncycles=5 nlib/cyc=5
  printlevel=5 lightel=9 inplevel=2 numztotal=5 end

  3 0.6500 2 0.6935 3 0.8068 500 2.6408 3 2.6470

  .
  power=28.13 burn=215.0 down=388 end
  power=39.91 burn=157.0 down=9.0 end
  power=39.91 burn=170.0 down=176 end
  power=38.99 burn=352.0 down=0 end
  power=31.77 burn=28.00 down=1825 end

  .
  o 135.0 cr 5.9 mn 0.33
  fe 13.0 co 0.075 ni 9.9
  zr 221.0 nb 0.71 sn 3.6

1  #####          aaaaaaaaaa          #####          2222222222          hh          hh
#####          aaaaaaaaaa          #####          2222222222          hh          hh
ss          ss          aa          aa          ss          ss          22          22          hh          hh
ss          ss          aa          aa          ss          ss          22          22          hh          hh
ss          ss          aa          aa          ss          ss          22          22          hh          hh
#####          aaaaaaaaaa          #####          22          hh          hh
#####          aaaaaaaaaa          #####          22          hh          hh
ss          ss          aa          aa          ss          ss          22          hh          hh
ss          ss          aa          aa          ss          ss          22          hh          hh
ss          ss          aa          aa          ss          ss          22          hh          hh
#####          aa          aa          #####          2222222222          hh          hh
#####          aa          aa          #####          2222222222          hh          hh

0

nn          nn          iiiiiiiiii          ccccccccc          hh          hh          oooooooooo          11

```